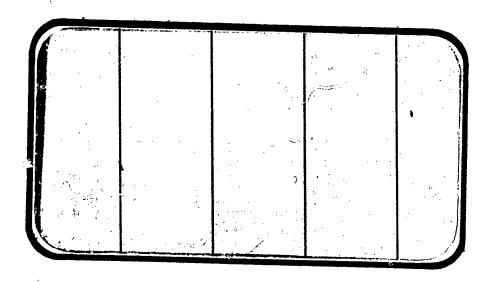
# NATIONAL AERONAUTICS AND SPACE ADMINISTRATION



ASA-CR-144620) TERMINAL AREA ENERGY NAGEMENT REGIME INVESTIGATIONS UTILIZING C.230-SCALE MODEL (47-0) OF THE SPACE . TELE VEHICLE ORBITER CONFIGURATION 1401/B/C/R IN THE AMES RESEARCH CENTER 11 x G3/02 49184.

N76-29163 HC\$16.25

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SPACE SHUTTLE

AEROTHERMODYNAMIC DATA REPORT



JOHNSON SPACE CENTER

HOUSTON, TEXAS

DATA MANagement services





DMS-DR-2254 NASA CR-144,620 VOLUME 2 OF 13

TERMINAL AREA ENERGY MANAGEMENT
REGIME INVESTIGATIONS UTILIZING AN 0.030-SCALE
MODEL (47-0) OF THE SPACE SHUTTLE VEHICLE
ORBITER CONFIGURATION 140A/B/C/R IN THE
AMES RESEARCH CENTER 11 X 11 FOOT
TRANSONIC WIND TUNNEL (0A148)

by

P. J. Hawthorne Rockwell International Space Division

Prepared under NASA Contract Number NAS9-13247

by

Data Management Services Chrysler Corporation Space Division New Orleans, La. 70189

for

**Engineering Analysis Division** 

Johnson Space Center National Aeronautics and Space Administration Houston, Texas

### WIND TUNNEL TEST SPECIFICS:

Test Number:

ARC 11-073

NASA Series Number:

0A148

Model Number:

47-0

Test Dates:

May 5 through May 17, 1975

Occupancy Hours:

220

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TERMINAL AREA ENERGY MANAGEMENT

REGIME INVESTIGATIONS UTILIZING AN 0.030-SCALE

MODEL (47-0) OF THE SPACE SHUTTLE VEHICLE

ORBITER CONFIGURATION 140A/B/C/R IN THE

AMES RESEARCH CENTER 11 x 11 FOOT

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by

P. J. Hawthorne, Rockwell International Space Division

#### **ABSTRACT**

This report documents data obtained in wind tunnel test OA148. The objectives of the test series were to:

- 1) obtain pressure distributions, forces and moments over the vehicle 5 Orbiter in the terminal area energy management (TAEM) and approach phases of flight.
- 2) obtain elevon and rudder hinge moments in the TAET and approach phases of flight.
- 3) obtain body flap and elevon loads for verification of loads balancing with integrated pressure distributions.
- 4) obtain pressure distributions near the short OMS pods in the high subsonic, transonic and low supersonic Mach number regimes.

Testing was conducted over a Mach number range from 0.6 to 1.4 with Reynolds number variations from 4.57 x  $10^6$  to 2.74 x  $10^6$  per foot. Model angle-of-attack was varied from -4 to 16 degrees and angles of side slip ranged from -8 to 8 degrees.

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PLOTTED COEFFICIENTS SCHEDULE:

- CY, CYN and CBL versus BETA
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- CHEO, CHEI, CHETOT and CHBF versus ALPHA
- CP versus X/LB
- CP versus X/CW
- CP versus X/CV

### NOMENCLATURE.

| Symbol             | Plot<br>Symbol | Definition  |
|--------------------|----------------|---|
| Ab                 | AB             | total Orbiter base area, ft <sup>2</sup>  |
| A <sub>1</sub>     | Af             | area over which P <sub>i</sub> acts, ft <sup>2</sup>                                |
| A <sub>sb</sub>    | ASB            | speed brake base area, ft <sup>2</sup>  |
| b                  | BREF, BW       | Orbiter wing span, in   |
| b <sub>V</sub>     | в٧             | vertical tail reference span, in  |
| c <sub>Au</sub>    | CAU            | Orbiter uncorrected axial force coefficient   |
| c <sub>A</sub>     | CA             | Orbiter axial force coefficient with sting cavity adjusted to average base pressure |
| CAF                | CAF            | Orbiter forebody axial force coefficient.   |
| CAsc               | CASC           | Orbiter sting cavity axial force coefficient.                                       |
| cou                | CDU            | Orbiter uncorrected drag coefficient  |
| c <sub>hbf</sub>   | CHBF           | body flap hinge moment coefficient, about hinge line $X_0 = 3532.0$                 |
| C <sub>hei</sub>   | CHEI           | inner elevon hinge moment coefficient, about hinge line $X_0 = 1387.0$              |
| C <sub>h</sub> eo  | CHEO           | outer elevon hinge moment coefficient, about hinge line $X_0 = 1387.0$              |
| C <sub>HeTOT</sub> | CHETOT         | total right elevon hinge moment coefficient   |
| cLU                | CLU            | Orbiter uncorrected lift coefficient  |
| C <sub>R</sub>     | CBL            | Orbiter rolling moment coefficient, body axis system                                |

## NOMENCLATURE (Continued)

| Symbol                | Plot<br><u>Symbol</u>   | <u>Definition</u>  |
|-----------------------|-------------------------|--|
| C <sub>m</sub>        | CLM                     | Orbiter pitching moment coefficient with sting cavity adjusted to average base pressure, referenced to Orbiter MRC.  |
| c <sub>mu</sub>       | CLMU                    | Orbiter uncorrected pitching moment coefficient  |
| c <sub>mF</sub>       | CLMF                    | Orbiter forebody pitching moment coefficient referenced to orbiter MRC.  |
| C <sub>msc</sub>      | CLMSC                   | Orbiter sting cavity pitching moment coefficient, referenced to Orbiter MRC  |
| c <sub>Nu</sub>       | CNU                     | Orbiter uncorrected normal force coefficient   |
| C <sub>N</sub>        | CN                      | Orbiter normal force coefficient with sting cavity adjusted to average base pressure   |
| c <sub>NF</sub>       | CNF                     | Orbiter forebody normal force coefficient  |
| C <sub>Nsc</sub>      | CNSC                    | Orbiter sting cavity normal force coefficient  |
| c <sub>n</sub>        | CYN                     | Orbiter yawing moment coefficient, body axis system  |
| c <sub>pi</sub>       | CPi                     | surface tap pressure coefficient, port i, $(P_1 - P_{\infty})/q$   |
| CY                    | CY                      | Orbiter side force coefficient   |
| c[x][v]               | c[x][Y]                 | base area force and moment coefficients. The first subscript (post fix) designates the type of coefficient, the second the pressure tap and it's associated area. The symbolic |
| [x]                   | <u>]</u> =              | vectors [X] and [Y] are defined below.   |
| A<br>N<br>Y<br>m<br>n | A<br>N<br>Y<br>LM<br>YN | axial force normal force side force pitching moment yawing moment  |
| L                     | BL                      | rolling moment   |

## NOMENCLATURE (Continued)

| Symbol                         | Plot<br>Symbol             | Definition   |
|--------------------------------|----------------------------|--|
| <u>[Y</u>                      | ]•                         |  |
| 1,2,3<br>4,5,6<br>sc<br>bf     | 1,2,3<br>4,5,6<br>SC<br>BF | areas associated with pressure taps 1 through 6 see figure 2b sting cavity area upper body flap area |
| 1 <sub>b</sub>                 | LB                         | Orbiter reference body length, IML nose to $X_0 = 1528.3$ , in.                                      |
| <sup>2</sup> REF               | LREF                       | longitudinal reference length, Orbiter mean aerodynamic chord, in                                    |
|                                | LU/DU                      | uncorrected lift to drag ratio, CLU/CDU  |
| M                              | MACH                       | freestream Mach number   |
| •                              | PHI                        | angular cylindrical coordinate position around Orbiter body - deg.                                   |
| Pi                             | Pi                         | pressure at surface tap i, PSF   |
| P <sub>co</sub>                | P                          | freestream static pressure, PSF  |
| Pt                             | PT                         | freestream total pressure, PSF   |
| 9                              | Q                          | freestream dynamic pressure, PSF   |
|                                | RN/L                       | unit_Reynolds_number, million-per foot   |
| S                              | SREF                       | wing reference area, ft <sup>2</sup>   |
| īt                             | TTR                        | freestream total temperature, °R   |
| X <sub>cp</sub>                | XCP/L                      | center of pressure location referred to 1b   |
| X <sub>o</sub> /L <sub>o</sub> | X/LB                       | longitudinal location of body surface, fraction of body length                                       |

## NOMENCLATURE (Concluded)

| Symbol .         | Plot<br>Symbol    | Definition   |
|------------------|-------------------|--|
| X/C              | X/CW              | chordwise location on wing surface, fraction of local chord                          |
| X/Cy             | X/CV              | chordwise location on vertical tail, fraction of local chord                         |
| nv               | Z/BV              | spanwise location on vertical tail, fraction of vertical tail span                   |
| η                | 2Y/BW             | spanwise location on wing, fraction of semi span                                     |
| X <sub>mrp</sub> | XMRP              | longitudinal location of moment reference point                                      |
| хт               | XT                | longitudinal moment transfer distance from Orbiter balance center to Orbiter MRC, in |
| Ymrp             | YMRP              | lateral location of moment reference point   |
| Z <sub>T</sub>   | <b>ZT</b> .       | vertical moment transfer distance from Orbiter balance center to Orbiter MRG, in     |
| α                | ALPHA             | angle of attack, degraes   |
| ß                | BETA              | angle of sideslip, degrees   |
| <sup>6</sup> bf  | BDFLAP            | body flap deflection, degrees  |
| <sup>6</sup> eL  | ELVN-L,<br>L-ELVN | left elevon deflection, degrees  |
| <sup>δ</sup> eR  | ELVN-R,<br>R-ELVN | right elevon deflection, degrees   |
| 6 <sub>r</sub>   | RUDDER            | rudder deflection, degrees   |
| δ <sub>sb</sub>  | SPDBRK            | speed brake deflection, degrees  |
| Z <sub>mrp</sub> | ZMRP              | vertical location of moment reference point  |
|                  | \$\$ /            | mask character used to indicate all possible values for this test 01 through 85      |

#### REMARKS

During the course of the test it was necessary to replumb the scanivalves. The resultant time loss necessitated deleting the priority 4 runs which incorporated the use of the metric vertical tail.

Data obtained from pressure taps 184, 296 and 347 are suspect due to slow leaks noticed while leak checking individual model pressure taps.

Body flap hinge moment data for datasets RE8001 through the have a -15% drift while datasets RE8006 and RE8007 to 0% drift due to data recording system errors. System checks withing the remainder of the test indicate a system error of less than 4% for body flap hinge moment data.

Rolling moment data has an approximate -.003 bias in the coafficient. The reason for this was not determined, but possible sources are fabrication tolerances and/or differential stiffness of the left and right elevon panels.

Distortion of the instrumented elevon shaft appears to have occurred around run 310 due to model assembly difficulties and the maximum loads encountered at these test conditions. A comparison of measured elevon deflection before and after the test with the nominal setting is presented below:

| Elevon Panel   | Nominal Nominal   | <u>Pre-Test</u>                                     | Post-Test   |
|----------------|---|---|---|
| Inboard right  | $ \begin{cases} -10 \\ -4 \\ 0 \\ 4 \\ 10 \end{cases} $ | -9° 36'<br>-3° 34'<br>+0° 10'<br>+4° 26'<br>+10°32' | -8° 55'<br>-2° 55'<br>+1° 02'<br>+4° 28'<br>+10°39' |
| Outboard right | $\begin{cases} -10 \\ -4 \\ 0 \\ 4 \\ 10 \end{cases}$   | -9° 36'<br>-3' 34'<br>+0° 10'<br>+4° 26'<br>+10°32' | -8° 15'<br>-2° 20'<br>+1° 05'<br>+3° 59'<br>+10°18' |

\* Inboard only was measured but was the same as outboard panel(see Ref 2)

## CONFIGURATION INVESTIGATED

The Rockwell International model 47-0 Space Shuttle Orbiter Vehicle was utilized in this test series. The model was originially constructed to -140A/B lines, but was modified prior to this test with the addition of the -140C OMS pods, six inch bevelled interpanel elevon gaps and uncovered RCS forward thrustor parts. To denote these additions, the additional designations "C" (for -140C OMS pods) and "R" (for RCS thrustors) were added, and the slashes deleted for convenience on Table II(designated "-140 ABCR").

In data sets RE8069 to 085 the RCS thrustor ports in the nose were filled reverting the configuration to -140A/B/C modified with body  $^{\rm B}26$ .

The following nomenclature denotes the model components:

| Component             | Description   |
|-----------------------|---|
| B <sub>26</sub>       | 140A/B fuselage (VL70-000140A, VL70000140B)   |
| B <sub>70</sub>       | 140A/B fuselage (VL70-000140A, VL70-000145, VL70-000140B, VL70-000143A, VL70-000139) with RCS thrustor parts (VL70-08501, VL70-08502, VL70-08296) |
| c <sub>9</sub>        | 140A/B basic canopy (VL70-000140A, VL70-000143A)  |
| E <sub>44</sub>       | 140A/B elevons (VL70-000200, VL70-006089, VL70-006092) with six inch bevelled interpanel gaps, no flipper door                                    |
| F <sub>9</sub>        | 140A/B body flap (VL70-000140B, VL70-000200)  |
| <sup>M</sup> 16       | OMS-RCS pods for 140C Orbiter   |
| N <sub>28</sub>       | OMS basic nozzles   |
| R <sub>5</sub>        | basic Orbiter rudder (VL70-000146A, VL70-000095)  |
| <b>v</b> <sub>8</sub> | basic Orbiter vertical tail (VL70-00014CA, VL70-000146A)  |
| W <sub>116</sub>      | basic 140A/B wing (VL70-000140B, VL70-000200)   |

## CONFIGURATIONS INVESTIGATED (Concluded)

Designated configurations are:

-140ABCR =  $B_{70}$   $C_{9}$   $E_{44}$   $F_{9}$   $M_{16}$   $N_{28}$   $R_{5}$   $V_{8}$   $W_{116}$ 

-140 ABC =  $B_{26}$   $C_{9}$   $E_{44}$   $F_{9}$   $M_{16}$   $N_{28}$   $R_{5}$   $V_{8}$   $W_{116}$ 

(1)

#### TEST FACILITY DESCRIPTION

The Ames Research Center Unitary Plan 11- by 11-Foot Transonic Wind Tunnel is a closed-circuit, air-medium, variable-density facility capable of attaining Mach numbers from 0.6 to 1.4 at Reynolds numbers from 1.7 x  $10^6/\text{ft}$  to 9.4 x  $10^6/\text{ft}$ . The test section is 22 feet long, and models are installed on internal strain-gauge balances mounted  $\frac{1}{2}$  sting-type support systems.

Shadowgraph and Schlieren photographic equipment is available, and pressure transducer instrumentation is provided.

Tunnel operating temperature is 580°R. Extended high Reynolds number runs are restricted by power availability.

#### DATA REDUCTION

Standard NASA/Ames data reduction equations were used to reduce forces, moments, and pressures to coefficient form. Orbiter main balance force and moment coefficients were computed using the following equations:

| Symbol .   | Orbiter main balance measurement  |
|--|---|
| NF<br>AF<br>PM<br>YM<br>SF<br>RM                                 | Normal Force Axial Force Pitching Moment Yawing Moment Side Force Rolling Moment  |
| C <sub>Au</sub> = AF / (q S)<br>C <sub>Nii</sub> = NF / (q S)    | C <sub>Lu</sub> = C <sub>Nu</sub> cos a -C <sub>Au</sub> sin a<br>C <sub>Du</sub> = C <sub>Nu</sub> sin a + C <sub>Au</sub> cos a |
| C <sub>γ</sub> = SF / (q S)                                      | Du Shu Sin a Shu cos a  |
| $c_{m_u} = \frac{PM}{qS_c} + \frac{c_A \cdot z_T}{c} .$          | C <sub>N</sub> · X <sub>T</sub>   |
| $C_{\ell} = \frac{R M}{qS_b} + \frac{C_{\gamma} \cdot Z_{T}}{b}$ | Moment Transfer Distances $X_T = 0.572 \text{ in.}$   |
| $c_n = \frac{\gamma_M}{qS_b} - \frac{c\gamma + \chi_T}{b}$       | $Y_{T} = 0$ $Z_{T} = 0.450 in.$   |

The Moment Reference Center about which the data was reduced is located at

Balance coefficients were grouped into datasets RE80\$\$.

Hinge moments and hinge moment coefficients were computed using the following equations:

Elevon hinge moments (inboard and outboard).

 $HM_{e_1} = (HM1-HM2) (M1/D1) + HM1$ 

 $HM_{eo} = (HM3-HM4) (M3/D3) + HM3$ 

where

HMi = measured moment on strain gage i

D1 = distance between gages 1 and 2, .49335 in.

D3 = distance between gages 3 and 4, .45800 in.

M1 = moment transfer distance for inboard elevon, .93825 in.

M3 = moment transfer distance for outboard elevon, .92250 in.

Elevon hinge moment coefficients

Inboard,  $C_{H_{e_I}} = H_{M_{e_I}} / (4 S_e c_e)$ 

Outboard,  $C_{\text{Heo}} = \frac{H_{\text{Me}_0}}{I} / (q S_e c_e)$ 

Total,  $C_{H_{e_{TOT}}} = C_{H_{e_{I}}} + C_{H_{e_{o}}}$ 

Se = elevon reference area, 0.189 ft.<sup>2</sup>

ce = elevon reference MAC, 2.721 in.

Body flap hinge moment coefficient

 $C_{H_{bf}} = HM_{bf} / (q S_{bf} c_{bf})$ 

HMbf = measured body flap hinge moment

 $S_{hf}$  = body flap reference area, 0.12834 ft.<sup>2</sup>

cbf = body flap reference MAC, 2.541 in.

Hinge moment coefficients are part of datasets RE8X\$\$.

Pressure coefficients for all model orifice pressure measurements were computed using this equation:

$$C_{P_i} = (P_i - P_{\infty})/q$$

 $( \downarrow )$ 

where  $P_i$  = pressure at model orifice i

P = tunnel static pressure

q = tunnel dynamic pressure

Other data reduction constants include:

S = wing reference area, 2.4210 ft.<sup>2</sup>

c = wing reference chord, 14.2443 in.

b = wing reference span, 28.1004 in.

After the data had been reduced to coefficient form by NASA/AMES,DMS interpolated it to nominal  $\alpha$ 's and  $\beta$ 's. Then 2 types of base and sting cavity area coefficients were calculated. When they are applied 3 types of balance coefficient data exists. These can be distinguished by the last subscript (symbolic name) or postfix (mnemonic name). The key is given below

- U ~ uncorrected coefficients.
  - coefficients with sting cavity pressure corrected to base pressure (without a suffix).
- F ~ forebody coefficients with the base area pressure corrected to freestream pressure.

Only the correction coefficients associated with base pressure tapes 1 through 4 were applied to the longitudinal orbiter coefficients.

tap. Alphabetic characters bf and sc designate body flap and sting cavity areas, respectively. Base area coefficient names have a numeric character which designates the pressure tap number. Base coefficients for vertical tail areas 5 and 6 were calculated but not applied to the total orbiter coefficients. Base area coefficient values are tabulated in the appendix. A detailed derivation of these coefficients follows. It is concluded by a matrix of base area geometric properties.

The orbiter sting cavity force and moment coefficients were computed as:

$$C_{A_{SC}} = \frac{(C_{p2} - C_{p1})}{S} A_{1}$$

$$C_{N_{SC}} = \frac{(C_{p2} - C_{p1})}{S} A_{1} \tan 12.55^{\circ}$$

$$C_{M_{SC}} = C_{A_{SC}} \frac{Z_{t}}{C} - C_{N_{SC}} \frac{X_{SC}}{C}$$

The orbiter force and moment coefficients corrected for the difference between balance cavity pressure and orbiter base pressure:

$$C_{A} = C_{A_{u}} - C_{A_{SC}}$$

$$C_{N} = C_{N_{u}} - C_{N_{SC}}$$

$$C_{m} = C_{m_{u}} - C_{m_{SC}}$$

These orbiter coefficients are part of datasets KE80\$\$.

Orbiter base force and moment coefficients were calculated as follows:

Upper base area

)

$$C_{N2u} = -(C_{p2} A_{2u} \tan 16^{\circ})/S$$

$$C_{A2u} = -(C_{p2} A_{2u})/S$$

$$C_{m2u} = \frac{C_{A2u} Z_{2u}}{C} - \frac{C_{N2u} X_{2u}}{C}$$

Lower base area

$$C_{N2_g} = -(C_{p2} A_{2_g} \tan 10^\circ)/S$$

$$C_{A2_{\ell}} = -(C_{p2} A_{2_{\ell}})/S$$

$$C_{m2_{\ell}} = C_{A2_{\ell}} \frac{Z_{2\ell}}{c} - C_{N2_{\ell}} \frac{X_{2\ell}}{c}$$

Total base area, A<sub>2</sub>

$$C_{N2} = C_{N2u} + C_{N2g}$$

$$C_{m2} = C_{m2_u} + C_{m2_{\frac{1}{2}}}$$

OMS pod base area, A3

(This assumes the surface is perpendicular to the orbiter X-axis)

$$C_{A3} = -(C_{p3} A_3)/S$$

$$C_{m3} = C_{A3} \frac{Z_3}{C}$$

OMS pod base area, A4

(This assumes the surface is perpendicular to the orbiter X-axis)

$$C_{A4} = -(C_{p4} A_4)/S$$

$$c_{m4} = c_{A4} \frac{Z_4}{c}$$

Coefficients for the above areas are grouped into datasets EE8D\$\$.

Upper surface of body flap

$$C_{A_{bf}} = \frac{-C_{p_{bf}} A_{bf}}{S} \sin (\delta_{bf} + 6.88^{\circ})$$

$$C_{Nbf} = \frac{-C_{pbf} A_{bf}}{S} \cos (\delta_{bf} + 6.88^{\circ})$$

$$c_{mbf} = \frac{c_{Abf} z_{bf}}{c} - \frac{c_{Nbf} x_{bf}}{c}$$

where:

$$C_{pbf} = \frac{C_{p200} + C_{p201} + C_{p204} + C_{p205}}{4}$$

The orbiter force and moment coefficients adjusted to free stream pressure (forebody coefficients).

$$C_{A_{F}} = C_{A_{U}} - \left(\frac{-C_{p1} A_{1}}{S} + \sum_{i=2}^{4} C_{A_{i}} + C_{Abf}\right)$$

$$C_{N_{F}} = C_{N_{U}} - \left(C_{N_{2}} + C_{N_{bf}}\right)$$

$$C_{m_{F}} = C_{m_{U}} - \left(\sum_{i=2}^{4} C_{m_{i}} + C_{m_{bf}}\right)$$

These orbiter coefficients are part of datasets KE80\$\$.

Vertical tail "undercarriage" area, A5

Top Segment:

$$C_{N5t} = (C_{p5} A_{5t} tan 63.75^{\circ})/S$$

$$C_{A5t} = - (C_{p5} A_{5t})/S$$

$$C_{m5t} = C_{A5t} \frac{Z_{5t}}{C} - C_{N5t} \frac{X_{5t}}{C}$$

### Middle Segment:

$$C_{N5m} = (C_{p5} A_{5m} \tan 26.1426^{\circ})/S$$

$$C_{A5m} = - (C_{p5} A_{5m})/S$$

$$c_{m5m} = c_{A5m} \frac{z_{5m}}{c} - c_{N5m} \frac{x_{5m}}{c}$$

### **Bottom Segment:**

$$C_{N5b} = (C_{p5} A_{5b} tan 21.94^{\circ})/S$$

$$C_{A5b} = - (C_{p5} A_{5b})/S$$

$$C_{m5b} = C_{A5b} \frac{Z_{5b}}{c} - C_{N5b} \frac{X_{5b}}{c}$$

## Total area, A5:

$$C_{N5} = C_{N5t} + C_{N5m} + C_{N5b}$$

### Vertical Tail base area, A6:

### Segment above rudder

$$C_{N6u} = (C_{p6} A_{6u} tan 63.75^{\circ})/S$$

$$C_{A6u} = (C_{p6} A_{6u})/S$$

### Rudder/Speed brake base:

$$C_{A6_{\ell}} = C_{P6} A_{6_{\ell}} [sin (e-55.1667^{\circ}) \cos 55.1667^{\circ} + \cos (e-55.1667^{\circ}) \sin 55.1667^{\circ} \cos (4r)]/s$$

$$C_{N6_{\ell}} = C_{p6} A_{6_{\ell}} [sin (e-55.1667^{\circ}) \sin 55.1667^{\circ} - \cos (e-55.1667^{\circ}) \cos 55.1667^{\circ} \cos (4r)]/s$$

$$C_{Y6_{\ell}} = C_{p6} A_{6_{\ell}} \cos (e-55.1667^{\circ}) \sin 4r/s$$

$$C_{M6_{\ell}} = [C_{A6_{\ell}} (Z_{6_{\ell}}) - C_{N6} (X_{6_{\ell}})]/c$$

$$C_{L6_{\ell}} = [C_{Y6_{\ell}} (Z_{6_{\ell}})]/b$$

$$C_{N6_{\ell}} = -[C_{Y6} (X_{6_{\ell}})]/b$$

$$C_{N6_{\ell}} = -[C_{Y6} (X_{6_{\ell}})]/b$$

$$A_{6_{\ell}} = A_{6_{\ell}}/\sin e$$

## Total area, A<sub>6</sub>:

$$C_{A6} = C_{A6u} + C_{A6e}$$
 $C_{N6} = C_{N6u} + C_{N6e}$ 
 $C_{Y6} = C_{Y6e}$ 
 $C_{m6} = C_{m6u} + C_{m6e}$ 
 $C_{e6} = C_{e6e}$ 
 $C_{n6} = C_{n6e}$ 

Vertical tail area coefficient data are grouped into datasets GE8D\$\$.

BASE GEOMETRIC PROPERTIES MATRIX

|                                      |                |                   | Distance between                   | Distance between Centroid and MRC |
|--------------------------------------|----------------|-------------------|------------------------------------|-----------------------------------|
|                                      | Sub-<br>script | Area<br>A - ft. 2 | vertical<br>Z - in.                | longitudinal<br>X - in.           |
| escription                           | , S            | 0.076699          | 0.45                               | 12.199                            |
| ting cavity                          | 4              | 0,128             | - 2.64                             | 13.659                            |
| ody flap upper surface               | } 「            | 0 076699          | 0.45                               | 12.199                            |
|                                      | - ,            | 0.07000           | - 1.32                             | 12.617                            |
| Jrbiter base orifice 2 lower         | 3              | 0.130             | 20 6                               | 12, 384                           |
| Orbiter base orifice 2 upper         | 2n             | 0.0818055         | /0.7                               | 2                                 |
| Lower OMS pod                        | က              | 0.030472          | 2.68                               | <b>E</b> :                        |
| lbper OHS pod                        | •              | 0.074166          | 3.63                               | <b>5</b>                          |
| Wertical tail "undercarriage" bottom | 25             | 0.003565          | 4.612                              | 12.395                            |
| Vertical tail "undercarriage" middle | \$             | 0.002610          | 5.336                              | 14.079                            |
| Vertical tail "undercarriage" top    | 3              | 0.000341          | 5.97                               | 15.185                            |
| Vertical tail above rudder           | 3              | 0.000798          | 12.656                             | 18.482                            |
| Base area of speed brake             | 79             | Varies with       | Varies with speed brake deflection | tion                              |

IES: Sting cavity and Orbiter balance cavity are synonymous.

\ - not applicable.

| δ <u>sb</u>               | A6 <sub>p</sub> ft <sup>2</sup>                               |
|---------------------------|---|
| 0<br>25<br>35<br>55<br>85 | 0.0066036<br>0.0456000<br>0.0621000<br>0.0950800<br>0.1551400 |
| x <sub>62</sub> =         | 15.045 + 1.442277 [1-cos (6sb/2)]                             |
| Z <sub>62</sub> =         | 9.755 + 0.501827 [1-cos (6sb/2)]                              |

Standard DMS loads cycle test procedures were used to process the OAl48 pressure data. First numerous pressure distribution plots were released. Analysis of these produced bad pressure data list. This list is reproduced below:

OA148 Bad Pressure Data

| Component            | Dataset<br>No.                      | Tap<br>No.   | £                                   | •                                       |
|----------------------|-------------------------------------|--|-------------------------------------|---|
| Fuselage<br>(B)      | 1<br>1<br>1<br>1<br>1<br>1          | 143<br>148<br>150<br>152<br>186<br>187<br>189<br>191               | 4<br>4<br>4<br>4<br>4<br>4          | -4<br>-4<br>-4<br>-4<br>-4<br>-4        |
| Lower Wing<br>(L)    | 1 + 7<br>1 + 85<br>1<br>1<br>1<br>1 | 231<br>290<br>316<br>317<br>337<br>338<br>358<br>378<br>379<br>398 | ALL<br>ALL<br>4<br>4<br>4<br>4<br>4 | ALL<br>-4<br>-4<br>-4<br>-4<br>-4<br>-4 |
| Upper Wing           | 1 <b>+ 7</b>                        | 247<br>357   | ALL 4                               | ALL                                     |
| Body Flap (F)        | 24                                  | 205  | -4                                  | 12                                      |
| Speed Brake (K)      | 1 + 85                              | 822  | ALL                                 | Al.L                                    |
| Vertical Tail<br>(V) | 8<br>ALL<br>79<br>79                | 443<br>1444<br>1453<br>1454  | ALL<br>ALL<br>-4<br>-4              | ALL<br>ALL<br>-4<br>-4                  |

Note: Wind tunnel pressure data tabulated in the appendix have the original bad data values.

These points were eliminated from further processing. The remaining data were interpolated to nominal alpha and beta values. Processing was completed with the release of a magnetic tape containing the final interpolated pressure coefficients.

This report contains plots and tabular listings for both force and pressure data. Plotted force data illustrates lateral-directional, longitudinal and hinge moment characteristics of the configuration tested. Plotted pressure data illustrates the effect of several control deflections and attitude changes on local pressure distributions. The multiple volume appendix contains a tabulated listing of the basic force and pressure data. Listing of the interpolated base area coefficients is also included. The plotted and tabulated data are arranged in the following \_\_\_\_\_\_\_\_manner:

| VOLUME<br>NO. | CONTENTS   |
|---------------|--|
| 1             | Force data plots showing lateral-directional     |
|               | longitudinal and hinge moment characteristics.   |
| 2             | Plots illustrating the effect of control surface |
|               | deflections on fuselage, wing and vertical tail  |
|               | pressure distributions.                          |

## DATA REDUCTION (Concluded)

| VOLUME<br>NO. |                      | CONTENTS   |
|---------------|----------------------|--|
| 3             | Tabulated            | Force Data   |
|               | <u>Dataset</u>       | Data type  |
|               | RE80\$\$             | source balance coefficients  |
|               | RE8X\$\$             | source hinge moment coefficients   |
|               | RE8Y\$\$             | source base pressure coefficients  |
|               | KE80\$\$             | interpolated balance coefficients adjusted for cavity pressure and forebody coefficients |
|               | EE8D\$\$<br>FE8D\$\$ | interpolated base and cavity area coefficients   |
|               | GE8D\$\$             | interpolated vertical tail base area coefficients  |

### Tabulated Pressure Data

|          | Component                          | Fourth<br>Character* | Page .       |
|----------|------------------------------------|----------------------|--------------|
| 4, 5     | orbiter fuselage                   | <b>B</b> _           | 1            |
| 6,7,8    | lower wing                         | L                    | 1271         |
| 9,10,11  | upper wing                         | U                    | 3147         |
| 12<br>12 | upper body flap<br>lower body flap | F<br>G               | 5405<br>5774 |
| 13<br>13 | speed brake<br>vertical tail       | ,<br>K<br>V          | 6143<br>6547 |

<sup>\*</sup> The fourth character in each dataset identifier (i.e., XE8BXX, B for Fuselage) represents the individual component.

### RÉFERÈNCES

- 1. SD75-SH-0106, "Pretest Information for OA148 of the 0.03-Scale 47-0 Pressure Loads Space Shuttle Model in the 11 x 11 Foot Leg of the NASA/ARC Unitary Plan Wind Tunnel," April 18, 1975.
- 2. MG-75-07-11, Rockwell International Corporation Internal Letter: "Model design Dimensional Varification Task 36: Elevon Deflection Angle Check of the 0.03-Scale SSV Model 47-0 (140A/B Configuration)". SAS/WTO/ ,-283, July 29, 1975.

| TEST \$ OA148     |                                 |                                       | DATE & May 1975                             |
|-------------------|---------------------------------|---------------------------------------|---|
|                   | TEST CON                        | IDITIONS                              |   |
|                   |                                 |                                       |   |
| MACH NÚMBER       | REYNOLDS NUMBER<br>(per foot)   | DYNAMIC PRESSURE<br>(pounds/sq. inch) | STAGNATION TEMPERATURE (degrees Fahrenheit) |
| 0,60              | 4.57 x 10 <sup>6</sup>          | 4.166                                 | 120   |
| 0.90              | $3.41 \times 10^6$              | 4.166                                 | 120   |
| 1.10              | 3.05 x 10 <sup>6</sup>          | 4.166                                 | 120   |
| 1.25              | 2.86 x 10 <sup>6</sup>          | 4.166                                 | 120   |
| 1.40              | 2.74 x 10 <sup>6</sup>          | 4.166                                 | 120   |
|                   |                                 |                                       |   |
|                   | <u> </u>                        |                                       |   |
|                   |                                 | •                                     |   |
|                   |                                 |                                       |   |
|                   |                                 |                                       |   |
| <u> </u>          |                                 |                                       |   |
|                   |                                 |                                       |   |
|                   |                                 |                                       |   |
|                   |                                 |                                       |   |
|                   | ·                               | ·                                     |   |
|                   |                                 |                                       |   |
|                   |                                 | . *                                   |   |
| BALANCE UTILIZED: | ARC Task MK XX                  | Α                                     |   |
|                   | CAPACITY:                       | ACCURACY:                             | COEFFICIENT                                 |
|                   |                                 |                                       | TOLERANCE:                                  |
| NF                | 3000 lbf/gage                   | •                                     |   |
| SF                | 1500 lbf/gage                   |                                       |   |
| AF                | _600_1bf                        |                                       |   |
| PM                | 27.000 in-1bf<br>4000 in-1bf    |                                       |   |
| RM                | <del></del>                     |                                       |   |
| YM                | 10,500 in-1bf                   | · <del></del>                         |   |
|                   | um normal and side fo<br>cation | orce dependent upo                    | on point of                                 |
|                   | 27                              |                                       |   |
| i                 | 27                              |                                       |   |

ARC 11-073

TABLE II.

|                                       |              |               |        |      |                |     |          | TE       | 57 (      | RUN  | <br>NUN  | IBE II |      |          |     |     |   |   |   |          | 3,76 |     | >            |            | ١             |
|---------------------------------------|--------------|---------------|--------|------|----------------|-----|----------|----------|-----------|------|----------|--------|------|----------|-----|-----|---|---|---|----------|------|-----|--------------|------------|---------------|
|                                       |              |               |        |      |                |     |          |          |           |      |          |        |      |          |     |     |   | , |   |          | ř    |     | NON          |            | NASA-MSFC-MAF |
|                                       | s            | Н             | Н      | •    |                |     |          |          |           |      |          |        |      |          | 1.1 |     |   |   |   |          |      | 3   | IDVAR (2)    |            | -HSF          |
| TEST                                  | MACH NUMBERS |               |        |      |                |     |          |          |           |      |          |        |      |          |     |     |   |   |   |          | 67   | 4   | 1DV          |            | XXX.          |
|                                       | N<br>H<br>U  |               | 1.4    | 1.25 | 1.1            | 6.0 | 0.6      |          | 9.0       | 6.9  |          | 4      | 1.25 | 1        | 6.0 | 9.0 |   |   | Ť |          |      | 1   | 3            |            |               |
| 7887                                  | ₹            | H             | 1      |      | 1              | 0   | 0        |          | 0         | 9    |          |        |      | <u>-</u> | ٥   | 0   |   |   |   |          |      | 4   | DVAR (1)     |            |               |
|                                       |              |               |        |      |                |     |          |          |           |      |          |        |      |          |     |     |   |   |   |          | 6.1  | 1   | ō            | i l        |               |
| DATE                                  |              | 9             | S      |      |                |     |          |          |           |      |          | 76     |      |          |     |     |   |   |   |          |      | 1   |              |            |               |
|                                       |              | 721           | 88     | 4%   | 47             | 52  | 57       |          | 64        | ٥٢   |          | 75     | 18   | 38       | 16  | 96  |   |   |   |          | 55   | •   |              |            |               |
|                                       |              |               |        | •    |                | 8   |          | -        | _         |      | <u> </u> |        |      |          |     |     | - |   |   | -        |      |     |              |            |               |
| AARY                                  |              | 80            | 38     | 4    | 46             | \$  | 26       |          | 63        | 63   |          | 74     | 88   | 88       | 8   | 56  |   |   |   |          |      | •   |              |            |               |
| SUMA                                  | Y            | 4             | \$     | \$   | 13             | 50  | SS       |          | 62        | 67   |          | 73     | 96   | 84       | 68  | 34  |   |   |   |          | 49   | 1   |              |            |               |
| NO                                    |              |               |        |      |                | _   | -        | $\vdash$ |           |      | _        | 2      | _    |          |     | _   | - |   |   |          |      | 4   |              | , ,        |               |
| LAT                                   |              | 0             | 33     | 39   | 44             | 45  | 8        | _        | ق         |      |          | ۲      | 94   | 83       | 86  |     |   |   |   |          | 43   | 1   |              |            |               |
| DATA SET/RUN NUMBER COLLATION SUMMARY |              | 4             | 32     | 38   | 43             | 48  | 53       |          | 9         | 65   |          | ٦      | רר   | 82       | 83  | 92  |   |   |   |          |      | •   |              | 1 1        | İ             |
| BER                                   |              | 800           | 0      |      |                |     |          |          | 0         |      |          | 0      |      |          |     |     |   |   |   |          | 37   | 4   | ENTS         |            |               |
| NON                                   |              | Ser           | 0      |      |                |     |          |          | 0         |      |          | 0      |      |          |     |     |   |   |   |          |      | ,   | COEFFICIENTS | 9          |               |
| S                                     |              | Sec 8         | 16.3   |      |                |     |          | -        | 225       |      | -        | 223    |      |          |     |     |   |   |   |          |      | 4   | - 1          | 121        | œ             |
| 1/13                                  | H            | S 828         |        |      |                |     |          |          |           |      | _        |        |      |          |     |     |   |   |   |          | 31   | 111 | -            | <b>-</b> 1 | 4             |
| TA S                                  |              |               | 55     |      |                |     |          |          | 55        |      |          | 85     |      |          |     |     |   |   |   |          |      | •   | Ø            | L          | ٦             |
| A<br>A                                |              | s 6 a         |        |      |                |     |          |          | 0         |      |          | 0      |      |          |     |     |   |   |   |          | 25   | •   | 1            | 1 '1       | `ھـ ا         |
|                                       |              | 8/8           | 8      | 0 4  | 0              | 9   | <b>U</b> |          | ١٥        |      |          | 0      | A    | (        | 6   | 2   |   | _ |   |          |      |     | 0            | o          | Y             |
| Ы                                     | ۲            | ۲             |        | 4    |                | 4   | ٨        |          | ٧         | ٧    |          | 3      | 4    | V        | 4   |     |   |   |   |          |      |     | 4            | 4          | 00            |
|                                       | ١,           | 2             | N      |      |                |     |          |          | .1        |      |          | 8      |      |          |     |     |   |   |   |          | 91   | 4   |              |            |               |
| ~                                     |              | NOI: YEROLAND | ABCR   |      |                |     |          |          | 20        |      |          | ABCE   |      |          |     |     |   |   |   |          |      | 3   | 278          | 32=        | 3             |
| 148                                   |              | 3             | 4      |      |                |     |          |          | 43        |      |          | 4      |      |          |     |     |   |   |   |          | 13   | 1   | 4            | 161        | ľ             |
| 2                                     |              |               | Ç      |      |                |     |          |          | -140 ABCR |      |          | -1440  |      |          |     |     |   |   |   |          |      | 3   |              |            |               |
| 40                                    | L            |               | -140   |      |                |     |          |          | -14       |      |          | 1      |      |          |     |     |   |   |   |          |      | 3   | a            | LES        |               |
| 0                                     | SET          | FIER          | Ď      | 200  | <del>003</del> | 400 | Sac      |          | 000       | ١٥٥٦ |          | 800    | 600  | 010      | 011 | 210 |   |   |   |          | ,    | 7   | 0            | SCHEDULES  | '             |
| TEST:                                 | DATA SET     | IDENTIFIER    | 2€8001 | U    | 0              | Q   | Q        |          | O         | 0    |          | 0      | Q    | 0        | 0   | 0   |   |   |   |          |      | 1   | 1            | Š          |               |
| E                                     | Ľ            | ō             | Ń      | ]    |                |     |          |          |           |      |          |        |      |          |     |     | L |   | L | <u> </u> | Ŀ    |     |              |            |               |

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TABLE II - Continued.

|                              | П            | _             |            |        |     |             |          |     | TE       | ST F  | א אט | UMI | 9C /1    | .,  |             |     |        |             |     |              | I       | 36. 2.     | -        | NO.          |      | AF.           |
|------------------------------|--------------|---------------|------------|--------|-----|-------------|----------|-----|----------|-------|------|-----|----------|-----|-------------|-----|--------|-------------|-----|--------------|---------|------------|----------|--------------|------|---------------|
| TEST                         | S            |               |            |        |     |             |          |     |          |       |      |     |          |     |             |     |        |             |     |              |         |            |          | ICVAR (2)    |      | NASA-MSFC-MAF |
| '                            | MACH NUMBERS |               | 4          | ,      |     | 1           | 6        |     |          |       | 12   | _   |          |     | <del></del> |     | 10     |             | , r |              | _       | 6.7        |          |              |      | ž             |
| 205                          | MAC          | -             | <b>*</b>   | +      | 3   | -           | 6.0      | 0.6 |          | サー    | \$21 | 3   | 6:0      | 0.6 |             | 1.4 | 1.25   | 1           | 9.0 | 9            |         |            |          | 10VAR (1)    |      |               |
| DATE:                        | ig           | 9             | 02         | +      | +   |             |          |     |          | 821   | -    |     |          |     |             | 154 |        |             |     |              |         | 13         |          |              |      |               |
| ۵                            |              | 7             | H          | +      | त्र | 2           | Li       | 221 | <u> </u> | , 121 | 133  | 138 | 143      | 30  |             | (S) | 154    | 491         | 164 | 17           |         | sn<br>ui   | -        |              |      |               |
| ARY                          |              | a             | 3          |        | 39  | =           | 9:       | 121 |          | 727   | 132  | 137 | 201      | 147 |             | 152 | 158    | 163         | +   | 517          |         |            |          |              |      |               |
| RUN NUMBER COLLATION SUMMARY | R            | 4             | 1_         | _      | S   | 110         | 151      | 3   |          | 521   | 150  | 136 | 141      |     |             | 151 | LSI    | 762         | 5.  | 74           |         | ٦          | -        |              | ļ    |               |
| ATION                        |              | 9             | 000        | 9      | 104 | १०५         | 411      | 611 |          | 124   | 621  | 135 | L        |     |             | Š   |        | <u> </u>    |     | i            |         | ] ;        |          |              |      |               |
| COLL                         |              | 1             | g          |        | 103 | 801         | 13       | 311 |          | 123   | 151  | 134 | 35       | 4   |             | 9   | S      | 3           | 3   | 5            |         |            |          | 4            | İ    |               |
| MBER                         | r            | V             |            | 0      |     |             |          |     |          | 0     |      |     |          |     |             | C   |        | _           | _   | L            | _       | ;          | ·  .     | COEFFICIENTS |      |               |
| N N                          |              | 4             |            | 이      |     |             | _        |     | 1        | 0     | _    | _   | L        | -   | -           | 0   | ╁      | _           | 1   | <del> </del> | -       | -          |          | 18           |      |               |
|                              |              | Y             | ٧.         | 기<br>사 |     |             | _        | -   | +        | 1     | _    | _   | $\vdash$ | -   | $\dotplus$  |     | ┿      | +           | ╀   | _            | ╀       | <b>∤</b> ′ | ; <br> - | 7            |      |               |
| TA SET                       |              | 2             | 4          |        |     |             | L        | 1   | +        | 0     | _    | -   | ╀        | -   | +           | ┿   |        | +           | +   | +            | +       | 1          |          | ]            |      |               |
| AQ                           |              | _             | -          | 0      | ρ   | P           | 1        | ) c | 十        | P     | A    | P   | 0        | +,  | ונ          | E   | +-     | TE          | IA  | U            | 土       | 1          |          | }            |      |               |
|                              | ,            | Ŀ             |            | 9      | 4   | 4           | _        | _   | _        | 0     | _    |     | _        | 1   | 1           | 8   | 2      | 4           | 2 4 | 1            | +       | 4          |          | }            |      |               |
|                              |              | Z             |            | V      |     |             |          |     |          | C     |      |     |          |     |             |     | y      |             |     |              |         |            | 2        | 4            |      |               |
| 100                          |              | CONFIGURATION | į          | ABC R  |     |             |          |     |          | 2000  |      |     |          |     |             |     | A COCK |             |     |              |         |            | :        | ]            |      |               |
|                              |              | CONFIC        |            | -140   |     |             |          |     |          | 047   |      |     |          |     |             |     | -140   |             |     |              |         |            |          | 1            |      |               |
| 0                            | $\  \ $      |               |            |        |     | \<br>\<br>\ | <u> </u> | 3   | +        |       |      | 1   | 5        | - 1 | 7           |     |        | <u>a, l</u> | 3   | 411          | +       | 4          | ,        | 4            | 9 50 | SCHECULES     |
|                              |              | DATA SET      | IDENTIFIER | RE8013 | 4.0 | 3           |          |     | 5        | 0     |      | 220 | 3        | 70  | 70          |     | 8      | \$70        | शु  | 100          | 170     |            |          | ملامين       | 50   | SCHE          |
| TEST                         |              | ŏ             | 106        | RE     |     |             |          |     |          |       |      |     | 1        |     |             |     |        |             |     |              | $\perp$ |            | -        | 1            |      |               |

TABLE II. - Continued.

| TEXT           | 841 40        |   | 3    | ;        |           |          |              |             | 9.5                              |        | 2    |      | DATE | : Jost | 1            | 1.519         |          |
|----------------|---------------|---|------|----------|-----------|----------|--------------|-------------|----------------------------------|--------|------|------|------|--------|--------------|---------------|----------|
|                |               |   | 2    | 4        | בי<br>ציי | 2        | UMB          | בא כען      | SEI KUN NUMBER LULLATIUN SUMMANI | N SOMN | AKI  | -    |      |        |              |               |          |
| DATA SET       |               |   |      |          | _         |          |              |             |                                  | ሄ      |      |      |      | 2      | MACH NUMBERS | MBERS         |          |
| IDENTIFIER     | CONFIGURATION | X | 65,  | - 5sb    | 300 0     |          | 26 28        | <b>6-</b> 4 | 0                                | 4      | 8    | 72   | 16   |        |              |               |          |
| <b>८८८०८</b> ८ | 140 ABER      | 2 | - Q  | 35 0     | 5 163     | 3 10     |              | צריו        | 2116                             | רכי    | 178  | 179  | 180  |        | 7.           |               | T        |
| 520            |               | 4 | A    |          |           |          |              | 181         | 1 82                             | 183    | 184  | 188  |      |        | 1.25         |               |          |
| 030            |               | 4 | A    | $\vdash$ |           |          |              | 186         | 187                              | 881    | હ્યા | 190  |      |        | -            |               |          |
| 031            |               | 4 | A    | -        |           | _        | -            | (6)         | 76)                              | (6)    | 401  | (05  | 1    | U      | 0.0          |               |          |
| 250            |               | - | J    | -        |           | _        | _            | 3           |                                  |        |      | 200  |      |        | 9.0          |               | 1        |
|                |               |   | -    | -        |           | <u> </u> | _            |             | _                                |        |      |      |      |        |              |               |          |
| 033            | 140 ABCR      | 3 | P    | +10 35   | 5 16.3    | 30       | 0            | 102 0       | 202 1                            | 203    | 202  | 205  | 206  |        | 1.4          |               | ST F     |
| 250            |               | 4 | ۵    | _        |           | _        | -            | 102         | _                                |        | 200  | 112  |      |        | 1.25         |               |          |
| 250            |               | 4 | A    | -        | _         |          |              | 212         | 513                              | 412    | 512  | 712  |      |        | -            |               |          |
| 936            |               | ۵ | 0    | -        | _         |          |              | L'2         |                                  | 512    | 220  | 122  |      |        | 60           |               |          |
| C50            |               | 4 | J    | _        |           |          |              | 222         |                                  | 224    | 225  | 226  |      | 7      | 0.5          |               |          |
|                |               |   | }-   |          |           | _        | _            |             |                                  |        |      |      |      |        |              |               |          |
| 980            | 140 ABCIZ     | 8 | 9 HO | 0 85     | 5.4.3     | 3 10     | o            | 127         | 7 228                            | 522    | 230  | 1231 | 232  |        | 4.1          |               |          |
| 030            |               | 4 | P    |          |           |          |              | 233         | 22.8                             | 235    | 762  | 752  |      | -      | 1.25         |               |          |
| 8              |               | 4 | A    |          |           |          |              | 238         | B 23%                            | 240    | 241  | 242  |      |        | -            |               |          |
| 8              |               | _ | A    |          |           |          |              | 243         | \$ 244                           |        | 74   | 147  |      | Ĭ      | e.<br>e.     |               |          |
| 280            |               | d | つ    |          |           |          |              | 248         | G 249                            | 282    | 152  | 222  |      |        | 9,0          |               | T        |
|                |               |   |      |          |           |          |              |             |                                  |        |      |      |      |        |              | 1             | $\dashv$ |
|                | 13 19         |   | 75   |          | ē         |          | 37           |             | 5                                | \$     |      | 55   |      | 5      | ۱            | 5             | \$ 1     |
| to a tack      |               | 1 | 7    | 1        | 7         | 1        | }            | 4           | 4                                | 4      | 1    | 4    | 1    | 4      | 1            | 444           | 48       |
| •              |               |   |      |          |           | . Oğ     | COEFFICIENTS | 15          |                                  |        |      |      |      | HAVO!  |              | מעאמי         |          |
| SCHEDULES      | 1168          |   |      |          |           |          |              |             |                                  |        |      |      |      |        |              |               |          |
|                |               |   |      |          |           |          |              |             |                                  |        |      |      |      |        |              | NASA-MSFC-MAF | FC-MAP   |

• }

TABLE II. - Continued.

|                                  |             |            |          |       |         |         | 76 | ST      | RUN     | NUN     | BEI     |            |          |              |       |       |        |          | £ 75 | 1       | 20 2         |           |
|----------------------------------|-------------|------------|----------|-------|---------|---------|----|---------|---------|---------|---------|------------|----------|--------------|-------|-------|--------|----------|------|---------|--------------|-----------|
| 76.57                            | UMBERS      |            |          |       |         |         |    |         |         |         |         |            |          |              |       | ;     |        |          | 67   | Lassa   | IDVAR (2)    |           |
| 150                              | MACHNUMBERS |            | 60       | 20    | 0.9     | 0.0     |    | 17.7    | 125     | 1.1     | 6.0     | 06         | 1.4      | 125          | 1.1   | 5.6   | 9.0    |          |      |         | DVAR (1)     |           |
| DATE                             |             | 16         |          |       |         | ·       |    | 278     |         |         |         |            | 304      |              |       |       |        | _        | 3    | 1       | 2            |           |
| اقا                              |             | 12         | LS2      | 792   | 267     | 272     |    | 21 7    | 283     | 887     | 862     | 862        | 303      | ઉજ્          | 314   | 319   | 324    | 1        | 55   | 1       |              |           |
| MARY                             |             | 8          | 256      | 26.1  | 266     | 172     |    | 272     | 282     | ر28     | 292     | <b>297</b> | 302      | 308          | 313   | 3/8   | 323    |          |      | 444     |              |           |
| ON SUM                           | 8           | 4          | 4 255    | 092 ا | 4 26S   | 1 270   | -  | 262     | 281     | 1286    | 1620    |            | <br>301  | <b>6</b> 307 | 312   | F 817 | 325    |          | \$   | 444     |              |           |
| SET RUN NUMBER COLLATION SUMMARY |             | 4 0        | 233 254  | 52852 | 263 264 | 268 269 |    | 273 274 | 279 280 | 284 285 | 289 290 | 294 29     | 19 300   | 805 306      | 0 311 | 5 316 | 128 0  |          | 43   | 1       |              |           |
| ABER C                           | -           | Sed -      | 10 2:    | 7.    | 4 20    | 77      |    | 4 2     | .2      | 32      | 28      | 25         | P4 299   | 8            | 010   | 315   | 320    | $\dashv$ | 37   | 4       | ENTS         |           |
| UN NU                            |             | Serie      | 5 10     |       | 5 4     |         |    | 3 4     |         |         |         |            | 3 A      |              |       |       |        |          | l    | 4       | COEFFICIENTS |           |
| SET R                            |             | 888        | 55225    |       | SS 22.5 |         |    | 85 163  | _       |         |         |            | 55 6     |              |       |       |        | $\dashv$ | 5    | 444     |              |           |
| DATA                             |             | 8 8R       | 0        | U     | 00      | J       |    | D-10    | ρ       | 0       | P       | C          | D -10    | Α            | Q.    | ^     | ر<br>د |          | 23   | 444     |              |           |
| H                                | μ           | (X         | <b>₹</b> | 4     | *       | ٧       |    | 8       |         |         | V       | ) <b>V</b> | 18       | 1            | A     | C V   | V      |          |      | 4       |              |           |
|                                  | 20.140      |            | इटर      |       | ABCC    |         |    | ABCR    |         |         |         |            | BeR      |              |       |       |        |          | 5    | 4111    |              |           |
| 841                              |             |            | 140 ABCR |       | 140 A   |         |    | 40 A    |         |         |         |            | 140 ABER |              |       |       |        |          | 13   | 4444    | 1            | 5         |
| EST: O                           | DATA SET    | IDENTIFIER | REBOAS 1 | 044   | 045     | 046     |    | ראס     | 048     | 049     | 8:0     | 150        | 250      | 550          | 054   | ठठ    | 9290   |          | ,    | معلنمما | 9 uo 8       | SCHEDULES |

TABLE II. - Continued.

|      | Π                                   |              |               |           |      |     |          |      | Ť€       | 5T F  | UN    | MUM    | BEN      | :<br>- |   |        |     |          | -     |         |          | ¥,  | Ž<br>Ž |  |          |
|------|-------------------------------------|--------------|---------------|-----------|------|-----|----------|------|----------|-------|-------|--------|----------|--------|---|--------|-----|----------|-------|---------|----------|-----|--------|--|----------|
|      |                                     |              |               | -         |      |     |          |      |          |       |       |        |          |        |   |        |     |          |       |         |          |     | 3      |  |          |
| 1    |                                     | MERS         |               |           |      |     |          |      |          |       |       |        |          |        |   |        |     |          |       |         |          | 23  | 4      |  |          |
|      | 1                                   | MACH NUMBERS |               | 7         | 1.27 |     | 6        | ٩    |          | 7     | 1.25  | 1.1    | 0.0      | 9      |   | 6      | و   |          | 6     | 90      |          |     | 7:     | :                                      |          |
| 7    |                                     | M            | H             | -         | -=   |     | 0        | 0    |          |       | نر    | _      | 0        | 0      |   | O,     | Ó   |          | 0     | 9       | -1       |     | 1      | אייייייייייייייייייייייייייייייייייייי |          |
| Ν.   | .                                   |              |               |           | arvo | ,   |          |      |          |       |       |        |          |        |   |        |     |          |       | -       | _        | 5   | 4      |  |          |
| DATE |                                     |              | 7             | 530       |      |     |          |      |          | 356   |       |        |          |        |   |        |     |          |       |         |          |     | 1      |  |          |
|      |                                     |              | 12            | 329       | 335  | 340 | 345      | ळह   |          | 325   | 178   | 9%     | 371      | 376    |   | 38     | 386 |          | 391   | 316     | 1        | \$5 | 4      |  |          |
|      | .χ                                  |              | 8             | 328       | 334  | 339 | 344      | 343  |          | 354   | 360   |        | 370      | 375    | · | 380    |     |          | 390   | 395     |          |     | 1      |  |          |
|      | MMM                                 | 8            | +             | 327 3     |      |     | 343 3    | 3482 | _        | 353 3 | 359 3 | 3/4365 | 369 3    | 374    | - | 3793   |     |          | 389 3 |         | $\dashv$ | \$  | 4      |  |          |
|      | 3<br>3<br>3<br>3                    |              | 4             |           |      |     | かっ       |      |          |       |       |        | <u> </u> |        |   |        |     |          | 8 35  | 393 394 | _        |     | }      | •                                      |          |
|      | ATI(                                |              | 0             | 728       | 332  | 337 |          | 4    |          | 352   | 358   | 263    | 37.8     | _      | _ | 378    | -   |          | 3%8   |         |          | 43  | 4      |  |          |
|      | TA SET/RUN NUMBER COLLATION SUMMARY |              | 1             | 328       | 331  | 336 | 340      | 2    |          | 351   | 357   | 367    | 26.7     | 372    |   | 3      | 382 |          | 387   | 342     | 100      |     | 1      | _                                      |          |
| 3    | BER                                 |              | 55.6          | 1         |      |     |          |      | Γ        | 4     | ·     |        |          |        |   | 4      |     |          | 01-   |         |          | 37  | 4      | COEFFICIENTS                           |          |
| 5    | <b>N</b>                            | İ            | Sol           | 4         |      |     |          |      |          | 4     |       |        |          |        |   | 4      |     |          | 10    |         |          |     | 1      | DEFFIC                                 |          |
| -    | Z.                                  |              | 585           | 16.3      |      |     |          |      |          | 16.3  |       |        |          |        |   | 225    |     |          | 22.5  |         |          | Ę.  | 4      | ŭ                                      |          |
|      | SET                                 |              | 525           | 28        |      |     |          |      |          | 55    |       |        |          |        |   | 55     |     |          | 25    |         |          |     | 1      | ·                                      |          |
| l    | DATA                                |              | 58            | 01        |      |     |          |      |          | 5,4   |       |        |          |        |   | ٥      | T   |          | 0     |         |          | 25  | 3      |  |          |
|      | _                                   |              | 9             | _         | _    | P   | P        | J    |          | ٥     | P     | 0      | P        | _      | _ | 0      | -   | _        | 0     | J       |          |     | 3      |  |          |
| H    | 7                                   | -            | 1             | 9         | 4    | X   | 4        | 4    |          | 6     | 4     | 4      | 2        | 4      | - | 1      | 4   | $\vdash$ | 4     | 4       |          | 6   | 1      |  |          |
|      |                                     |              | Z             | N         |      |     |          |      |          | له    |       |        |          |        |   |        | ,   |          |       |         |          | 19  | 4      |  |          |
| 1    | W T                                 |              | CONFIGURATION | 7         |      |     |          |      |          | ABC   |       |        |          |        |   |        |     |          | ABC   |         |          |     | 4      |  |          |
| ľ    | -                                   |              | NFIG          | 4         |      |     |          |      |          | 404   |       |        |          |        |   | 40     |     |          |       |         |          | 13  |        |  | ı        |
|      | 4                                   |              | S             | -140 ABCP |      |     |          |      |          | 4     |       |        |          |        |   | MOARCE |     |          | 140   |         |          |     |        | •                                      | <b>.</b> |
| ľ    | V                                   | 1            | . E.          | ₩         | +    | 550 | 3        | 198  | +        | 670   |       | 470    | 7        |        | 8 | 2      |     | 1        | 630   | סרס     |          | ^   |        | 6                                      |          |
| 1    | rest:                               |              | DENTIFIER     | PE8057    | 0    | 0   | O        | ď    |          |       |       | ) (    |          | ) (    | ) | 1      | ٥   |          | 0     | 0       |          |     | 1      | (                                      | •        |
| L    |                                     | Ľ            | , <u>ē</u>    | 9         |      |     | <u>L</u> |      | <u> </u> |       |       |        |          |        |   |        | 1   | L        | L     |         |          | Ŀ   |        |  |          |

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TABLE II. - Concluded.

|          | П                                    |              |               |             |             |          |         |              | 7 6 | <b>5</b> T ( | NUF           | NUM  | BÉR     | is .          |          |       |         |         |      |            |   | ,,<br>K  | 1                 | > \<br>2     |          |   |
|----------|--------------------------------------|--------------|---------------|-------------|-------------|----------|---------|--------------|-----|--------------|---------------|------|---------|---------------|----------|-------|---------|---------|------|------------|---|----------|-------------------|--------------|----------|---|
| 1        |                                      |              |               |             |             |          |         |              |     |              |               |      |         |               |          |       |         |         |      |            |   | 1        | 4                 |              |          |   |
| TEST     |                                      | ERS          |               |             |             |          |         |              |     |              |               |      |         |               |          |       |         |         | 1    | $\dashv$   | - |          | 3                 | IDVAR IZ     |          |   |
| 1        |                                      | MACH NUMBERS | Н             |             |             |          |         | _            |     |              | <b>\</b>      |      |         |               |          |       |         | _       | _    | _          |   | 3        | 4                 | 00           | Ą        |   |
| 7505     |                                      | MACH         |               | 7.          | 1.25        | -        | ० १     | 9            |     | 4.           | 52.1          | 1:1  | 6.5     | 2.0           |          | 4     | 1.25    | =       | 0.9  | 0.0        |   |          | 4                 | PAAR III     | X<br>"   |   |
|          |                                      |              |               |             |             |          |         |              |     |              |               |      |         |               |          |       |         |         |      |            |   | 6.1      | 4                 | ğŦ           | G        |   |
| DATE:    |                                      |              | 9             | 402         |             |          |         |              |     | 828          |               |      |         |               |          | 454   |         |         |      |            |   | ۳        | 1                 | )!<br>X      |          |   |
| ă        | J                                    |              | 1             |             |             | - 1      | 1       |              | _   | <u>₹</u>     |               | 00   | 3       | 8             | _        | 34    | 5       | 4       |      | -          |   |          | 3                 | 000 00       | -404     | ł |
|          |                                      |              | 21            | 401         | <b>4</b> 07 | 412      | 417     | 422          |     | 427          | 433           | 438  | 43      | 446 AUT) C498 |          | 453   | 452     | 454     | 469  | <b>474</b> |   | 55       | and a a a a a d a | 0            | 4        |   |
| à        | ואו                                  |              | 0             | 400         | 406         | = 7      | 416     | 124          |     | 226          | 432           | 187  | 441 442 | 4             |          | 452   | 458     | 163     | 002  | 471 472 AZ |   |          | 4                 | 7            |          |   |
|          | MM                                   | γ            | 4             | _           | 405         |          |         |              |     |              |               | _    | 4       | 2             | $\vdash$ |       |         | 2       | 216  | 72/        |   | \$       | 1                 | 11           | 1        |   |
| 3        | Z                                    |              | 1             | 3399        | 4           | 1410     | Ā       | 420          | _   | 425          | 431           | 43.  |         | 4             | _        | ASI   | 456 4C) | 462     | 1467 | 4          |   |          |                   |              |          | 1 |
|          | AIR                                  |              | 0             | 398         | 404         | 409      | 4       | 4 5          |     | 4217         | 430           | 435  | \$      | 445           |          | 450   | 151     | 2       | 46   | 4          |   | 43       | •                 |              |          |   |
| į        | NIA SELZKUN NUMBER CULLATION SUMMANT |              | V             | 397         | 403         | 408      | 413 414 | 4.8          |     | 224          | 424           | 43.4 | 439     |               |          | 449   | 455     | 460 461 | 465  | 410        |   |          | •                 |              | 1        | ١ |
|          | און<br>און                           | H            | Sed-          |             | A           | 4        | 7       | Y            |     | 0            | 4             |      | 4       | _Y_           |          | 410   | 4       | 7       | 4    | d          |   | 37       |                   | STA          | 2        |   |
|          |                                      |              | ود او         | -101-       |             |          |         | <del> </del> |     |              |               |      |         | $\vdash$      | -        | -10   |         |         |      |            |   |          |                   | COEFFICIENTS |          | H |
|          | 2<br>2<br>2                          |              |               | 16.3        |             |          |         |              |     | 01+ (-11-    |               |      | -       | _             | -        | 1-11- |         |         |      |            |   |          | •                 |              | . Pa.    |   |
|          |                                      | H            | <b>309</b> 9  |             |             |          |         |              | _   |              | <del> -</del> | -    | _       |               | -        |       |         |         |      |            |   | 31       | 111               | 4            | <b>.</b> |   |
|          | ⊼<br><b>&lt;</b> _                   |              | . See         | 5 55        |             |          |         | _            | _   | 0            | _             | _    | _       |               | <u> </u> | 0     |         |         |      |            |   |          | •                 | 4            | 0        | н |
|          | 2                                    |              | 56            | 7           |             |          |         | <u> </u>     |     | 3            | _             | _    | _       | _             | _        | ò     |         |         |      |            |   | 25       |                   | 11 7         | 4        |   |
|          |                                      |              | 8 70          | व्यश्व      | A           | A        | B A     | V            | _   | 8 8          | P             | P    | A       | C             |          | 图     | A       | AE      | AF   | A 6        | - |          |                   |              | 1        |   |
| <b> </b> | 7                                    | -            | દ             | 122         | 7           | <i>'</i> |         |              |     | 100          | F             | F    | -       |               |          |       | 7       |         | _    | 7          | - | 5        |                   | 0            | A        |   |
|          |                                      |              | 2 0           |             |             |          |         |              |     | ١,           |               |      |         |               |          |       |         |         |      |            |   |          | 6 .               | 1            |          |   |
| 1        | Ì                                    |              | CONFIGURATION | ABC         |             |          |         |              |     | 138 C        |               |      |         |               |          | ABC   |         |         |      |            |   |          |                   | 11           | }        |   |
| 4        |                                      |              | אבופר         |             |             |          |         |              |     |              |               |      |         |               |          |       |         |         |      |            |   | 13       | -                 |              | 1        | 1 |
|          | ,                                    |              | Ď             | -140        |             |          |         |              | ľ   | 4            |               |      |         |               |          | 041   |         |         |      |            |   |          |                   |              |          |   |
| Ó        |                                      | <b> -</b>    | œ             |             | 7           | 3        | ৳       | <b>1</b> 3   | -   | '            | <u> </u>      | 20   | ,,-     | 10            | _        | -     | 01      | 8       | 4    | 1          | - | ٦        |                   | •            | CLEON F  | 2 |
|          |                                      | DATA SET     | DENTIFIER     | DEBON!      | 210         | 510      | 574     | SID          |     | 20           | 6             | 8    | 9:0     | 080           |          | 3     | 382     | 83      | 280  | 280        |   |          | :                 |              | BO B     | 7 |
| TEST     |                                      | ð            | DEN           | <b>Dest</b> |             |          |         |              |     |              |               |      |         |               |          |       |         |         |      |            |   | <u> </u> | ] :               |              |          |   |

# TABLE III MODEL DIMENSIONAL DATA

| MODEL COMPONENT : BODY - Bob   |                           |                  |
|--|---------------------------|------------------|
| GENERAL DESCRIPTION :Configuration                                       | 140A/B orbiter            | fuselege         |
| NOTE: Box is identical to Box except                                     | underside of fus          | elago bas boon   |
| refaired to accept W116.   |                           |                  |
| MODEL SCALE: 0.030 MODEL   | DRAWING: SS-ACC           | 1147 Release 12  |
| DRAWING NUMBER: <u>VI.70-000143B</u> , -0002<br>VI.70-000140A, -0001     |                           | 26089, -000145   |
| DIMENSIONS :   | FULL SCALE                | MODEL SCALE      |
| Length (OML: Fwd Sta. $X_0 = 235$ )<br>Length (IML: Fwd Sta $X = 238$ ), | ,In. 1293.3<br>In. 1290.3 | 38.799<br>38.709 |
| Max Width (@ $X_0 = 1528.3$ ), In.                                       | 264.0                     | 7.920            |
| Max Depth (@ $X_0 = 1464$ ), In.   | 250.0                     | 7.500            |
| Fineness Ratio   | 0.264                     | 0.264            |
| Area - Ft <sup>2</sup>   |                           |                  |
| Max. Cross-Sectional   | 340.88                    | 0.3068           |
| Planform   |                           |                  |
| Wetted   |                           | \)               |
| Base   |                           |                  |
|  |                           |                  |

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

# TABLE III (Continued)

| MODEL COMPONENT : BODY - B70   |                                      |   |
|--|--------------------------------------|---|
| GENERAL DESCRIPTION :Configurati   | on 140A/B orbita                     | r fuselege with                         |
| forward fuselage RCS thruster ports, o                                   | therwise B <sub>70</sub> is          | identical to                            |
| B <sub>26</sub> .  |                                      |   |
| MODEL SCALE: 0.030   |                                      |   |
| DRAWING NUMBER: <u>VL70-000140A</u> -00014<br>VL70-000205, -00608        | 40B, -000143B, -<br>9, -008501, -008 | 000145 <u>-00020</u> 0,<br>502, -008296 |
| DIMENSIONS:  | FULL SCALE                           | MODEL SCALE                             |
| Length (CML: Fwd Sta $X_0$ =235), I<br>Length (IML: Fwd Sta $X_0$ =238), | In. 1293.3<br>In. 1290.3             | 38.799<br>38.709                        |
| Max Width (@ $X_0 = 1528.3$ ), In.                                       | 261.0                                | 7.920                                   |
| Max Depth (0 $X_0 = 1464$ ), In.   | 250.0                                | _7.500                                  |
| Fineness Ratio   | 0.264                                | 0.264                                   |
| Area - Ft <sup>2</sup>   |                                      |   |
| Max. Cross-Sectional   | 340.88                               | 0.3068                                  |
| Planform   |                                      |   |
| Wetted   |                                      |   |
| Base   |                                      | -                                       |

+])

| MODEL COMPONENT : CANOPY - C                 |              |             |
|--|--------------|-------------|
| GENERAL DESCRIPTION : Configuration 3        |              |             |
| B <sub>26</sub> .                            |              |             |
| •  |              |             |
| MODEL SCALE: 0.030 MODEL DWG:                | SS-A00147, F | Release 12  |
| DRAWING NUMBER: VL70-000143A                 |              |             |
|  |              |             |
|  |              |             |
| DIMENSIONS:                                  | FULL SCALE   | MODEL SCALE |
| Length (X <sub>0</sub> =434.643 to 578), In. | 143.357      | 4.301       |
| Max Width (@ $x_0 = 513.127$ ), In.          | 152.412      | 4.572       |
| Max Depth (@ $X_0 = 485.0$ ), In.            | 25.00        | 0.750       |
| Fineness Ratio                               |              | -           |
| Area   |              |             |
| Max. Cross-Sectional                         |              |             |
| Planform                                     |              | •           |
| Wetted                                       |              |             |
| Base   |              |             |

| MODEL COMPONENT ELEVON - E.   |                                      |             |
|---|--------------------------------------|-------------|
| GENERAL DESCRIPTION 6.0 in. F.S. Flipper doors centerbody pieces, and | paps machined in<br>tipseals are not |             |
| (Data are for one of two sides.)                                      |                                      |             |
| MODEL SCALE: 0.030  |                                      |             |
| DRAWING NUMBER  |                                      |             |
|   |                                      |             |
| DIMENSIONS  | FULL SCALE                           | MODEL SCALE |
| Area - Ft <sup>2</sup>  | 210.0                                | 0.189       |
| Span (equivalent) , In.   | 349.2                                | 10.476      |
| Inb'd equivalent chord, In.   | 118.0                                | 3.54        |
| Outb'd equivalent chord, In.  | 55.19                                | _1.656      |
| Ratio movable surface chord/<br>total surface chord                   |                                      |             |
| At Inb'd equiv. chord   | 0.2096                               | 0.2096      |
| At Outb'd equiv. chord  | 0.4004                               | 0.4004      |
| Sweep Back Angles, degrees  |                                      |             |
| Leading Edge  | 0.00                                 | 0.00        |
| Trailing Edge   | - 10.056                             | - 10.056    |
| Hingeline (Product of Area & C  | 0.0                                  | 0.0         |
| Area Moment (bizzabaadaagsdiste) ,F                                   | <sup>2</sup> 1587.25                 | 0.0429      |
| Mean Aerodynamic Chord, In.   | 90.7                                 | 2.721       |

( )

| MODEL COMPONENT : BODY FLAP - F  | <u> </u>       |             |
|----------------------------------|----------------|-------------|
| GENERAL DESCRIPTION :Configure   | tion 140A/B    |             |
|                                  |                |             |
|                                  |                |             |
| MODEL SCALE: 0.030               |                |             |
| DRAWING NUMBER : VL70-000140B, - | 000200         |             |
|                                  | •              |             |
|                                  |                | 4           |
| DIMENSIONS:                      | FULL SCALE     | MODEL SCALE |
| Length (Chord), In.              | 84.7           | 2.541       |
| Max Width , In.                  | <u>262,308</u> | 7.869       |
| Max Depth , In.                  | 23.00          | 0.690       |
| Fineness Ratio                   |                | 4           |
| Area - Ft <sup>2</sup>           |                |             |
| Max. Cross-Sectional             | <del></del> ,  |             |
| Planform                         | 142.60         | 0.128       |
| Wetted                           |                |             |
| Base                             | 41.90          | 0.0377      |

(1)

# TABLE III (Cont'd)

| MODEL COMPONENT : OMS POD - M16            |                   |                  |
|--|-------------------|------------------|
| GENERAL DESCRIPTION : Configuration        | 140C orbiter OMS  | pod - short pod  |
| External contour is to referenced draw     | rings with 1/2" a | dded to simulate |
| TPS.                                       |                   |                  |
| MODEL SCALE: 0.015                         |                   | ·                |
| DRAWING NUMBER:                            | 10                |                  |
|  |                   |                  |
|  |                   |                  |
| DIMENSIONS:                                | FULL SCALE        | MODEL SCALE      |
| Length (OMS Fwd Sta X <sub>O</sub> =1310.5 | ),In. 258.50      | 7.755            |
| Max Width (@ $X_0 = 1511$ ), In.           | 136.8             | 4.104            |
| Max Depth (@ $X_0 = 1511$ ), In.           | 74.70             | 2.241            |
| Fineness Ratio                             | 2.484             | 2.484            |
| Area - Ft <sup>2</sup>                     |                   |                  |
| Max. Cross-Sectional                       | 58.865            | 0.053            |
| Planform                                   |                   |                  |
| Wetted                                     |                   |                  |
| Base                                       | ·                 |                  |

OMS

| MODEL COME                              | ONENT: KON NOZZLES - N <sub>28</sub>                        |                            | •                        |
|---|---|----------------------------|--------------------------|
| GENERAL DE                              | SCRIPTION: Configuration L                                  | LOA/B orbiter OMS nog      | zles.                    |
| *************************************** |   |                            |                          |
| MODEL SCAI                              | E: <u>0.030</u>   |                            |                          |
| DRAWING NU                              | MBER: VL70-000140A (Location                                | n), SS-A00106, Releas      | e 9 (Contour)            |
| DIMENSIONS                              | <b>3:</b>   | FULL SCALE                 | MODEL SCALE              |
| MACH 1                                  | io.   | •                          |                          |
| . Gi                                    | n - In.<br>imbal Point to Exit Plane<br>aroat to Exit Plane |                            |                          |
| Ex<br>Th                                | er - In.<br>cit<br>nroat<br>nlet                            |                            |                          |
| Area -<br>Ex                            | rt <sup>2</sup><br>:it                                      |                            |                          |
| T                                       | proat   |                            |                          |
| Gimbal<br><b>Left</b>                   | Point (Station) · In. Nozzle                                |                            |                          |
|   | X0<br>Y0<br>Z0  | 1518.0<br>- 88.0<br>- 492. | 45.54<br>- 2.64<br>14.76 |
| Right                                   | Nozzles<br>XO   | 1518.0                     | 45.54                    |
|   | <b>Y</b> 0<br><b>Z</b> 0                                    | 88.0<br>492.0              | 2.64<br>14.76            |
| Null 1<br>Left :                        | Position - Deg.<br>Nozzle<br>Pitch                          | 15°49'                     | 15%91                    |
|   | Yaw   | 12-171                     | 120171                   |
| Right                                   | Nozzle<br>Pitch<br>Yaw                                      | 15%91                      | 15%91                    |

| MODEL COMPONENT - RUDDER - R                                |                       |                   |
|---|-----------------------|-------------------|
| GENERAL DESCRIPTION Configuration                           | 1400 orbiter rud      | der (identical to |
| configuration 140A/B rudder).                               |                       |                   |
|   |                       |                   |
| MODEL SCALE: 0.030  |                       |                   |
| DRAWING NUMBER VL70-000146B, -0000                          | 95                    |                   |
|   |                       |                   |
|   |                       |                   |
| DIMENSIONS  | FULL SCALE            | MODEL SCALE       |
| Area - Ft <sup>2</sup>                                      | 100.15                | 0.090             |
| Span (equivalent), In.                                      | 201.00                | 6.030             |
| inb'd equivalent chord, In.                                 | 91.585                | 2.748             |
| Outb'd equivalent chord, In.                                | 50.833                | 1.525             |
| Ratio movable surface chord/ total surface chord            |                       |                   |
| At Inb'd equiv. chord                                       | 0.400                 |                   |
| At Outb'd equiv. chord                                      | 0.400                 | 0.400             |
| Sweep Back Angles, degrees                                  |                       |                   |
| Leading Edge  | 34.83                 | 34.83             |
| Trailing Edge   | 26.25                 | 26.25             |
| Hingeline   | 34.83                 | 34.83             |
| (Product of area & c)<br>Area Moment (Noonabbabbagadina) ,F | t <sup>3</sup> 610.32 | 0.0165            |
| Mean Aerodynamic Chord, In.                                 | 73.2                  | 2.196             |
|   |                       |                   |

| MODEL COMPONENT: VERTICAL - V8  |  | •   |
|---|--|---|
| GENERAL DESCRIPTION: Configuration 140C or  | biter vertical to  | il.   |
| (Identical to configuration 140A/B vertical   | teil.)   |   |
| MOTEL SCALE: 0.030  |  | •   |
| DRAWING NUMBER: VL70-0001LOC -0001L6B   |  |   |
| dimensions:   | FULL SCALE   | MODEL SCALE   |
| TOTAL DATA  |  |   |
| Area (Theo) - Ft <sup>2</sup> Planform Span (Theo) - In. Aspect Ratio Rate of Taper Taper Ratio Sweep-Back Angles, Degrees. Leading Edge Trailing Edge O.25 Element Line  Chords: Root (Theo) WP Tip (Theo) WP MAC Fus. Sta. of .25 MAC W.P. of .25 MAC B.L. of .25 MAC | 413.253<br>315.72<br>1.675<br>0.507<br>0.404<br>45.000<br>26.25<br>41.13<br>268.50<br>108.47<br>199.81<br>1463.35<br>635.52<br>0.0 | 0.372 9.472 1.675 0.507 0.404 45.000 26.25 41.13  8.055 3.254 5.994 43.901 19.066 0.0 |
| Airfoil Section<br>Leading Wedge Angle - Deg.<br>Trailing Wedge Angle - Deg.<br>Leading Edge Radius   | 10.0<br>14.92<br>2.0   | 10.0<br>14.92<br>0.060  |
| Void Area   | 13.17  | 0.0019  |
| Blanketed Area  | 0.0  | 0.0   |

| GENERAL DESCRIPTION: Configuration 4   |  |   |
|--|--|---|
| NOTE: Identical to W111 except airfoil thickness.  | ihedral angle  | is along  |
| trailing edge of wing.   |  |   |
| MODEL SCALE: 0.030   |  | المناسبون والمناور والمناور والمراول                        |
| TEST NO.   | DWG. NO. VI7   | 0-000140A00   |
| DIMENSIONS:  | FULL-SCALE   | MODEL SCALE   |
| Area (Theo.) Ft <sup>2</sup> Planform Span (Theo In. Aspect Ratio Rate of Taper Taper Ratio Dihedral Angle, degrees Incidence Angle, degrees | 2690,00<br>936.68<br>2.265<br>1.177<br>0.200<br>3.500<br>0.500 | 2.421<br>28.10<br>2.265<br>1.177<br>0.200<br>3.500<br>0.500 |
| Aerodynamic Twist, degrees Sweep Back Angles, degrees Leading Edge Trailing Edge 0.25 Element Line Chords:                                   | 45.000<br>- 10.056<br>35.209                                   | 45.000<br>- 10.056<br>35.209                                |
| Root (Theo) B.P.O.O. Tip, (Theo) B.P. MAC Fus. Sta. of .25 MAC W.P. of .25 MAC B.L. of .25 MAC   | 689.24<br>137.85<br>474.81<br>1136.83<br>290.58<br>182.13      | 4,136<br>14,244<br>34,105<br>8,717<br>5,464                 |
| EXPOSED DATA Area (Theo) Ft <sup>2</sup> Span, (Theo) In. BP108 Aspect Ratio Taper Ratio Chords  | 1751.50<br>720.68<br>2.059<br>0.245                            | 1.576<br>21.620<br>2.059<br>0.245                           |
| Root BP108 Tip 1.00 b  MAC Fus. Sta. of .25 MAC W.P. of .25 MAC B.L. of .25 MAC Airfoil Section (Rockwell Mod NASA)                          | 562.09<br>137.85<br>392.83<br>1185.98<br>295.30<br>251.77      | 16.863<br>4.136<br>11.785<br>35.579<br>8.829<br>7.555       |
| XXXX-64  Root <u>b</u> =  Tip <u>b</u> =   | 0.113  | 0.113   |
| Data for (1) of (2) Sides  Leading Edge Cuff Planform Area Ft2 Leading Edge Intersects Fus M. L. 6 Sta                                       | 113.18<br>500.0<br>1025.0                                      | 0.102   |

TABLE IV.

FUSELAGE PRESSURE TAP LOCATIONS -

| 9    | ORENTER- IM. | ~ /K    |     |    |     |    |         | P   |     | 1  | RADIAL         | 78.  |                 | LOCATION      | 7/0          | 1.           | 1  | 19           | DEGREES       | 83  |                | ĺ              | 1    |
|------|--------------|---------|-----|----|-----|----|---------|-----|-----|--|----------------|--|-----------------|---------------|--------------|--------------|----|--------------|---------------|-----|----------------|----------------|------|
| FULL | Mod          | //X     | 0   | 2  | 4   | 35 | 2       | 8   | 100 | 8  | 110 120 135 40 | 1  | 3               | 8             | 19           | 3            | 3  | 183          | 169           | 7   | 180 W          | 200            | 12 1 |
| 235  | 705          | 0       | 1   |    |     |    |         |     |     |  |                |  | $\vdash$        |               |              | _            | -  |              |               | -   | -              |                |      |
| 283  | 7.35         | .008    | 8   |    |     |    |         | 0   |     |  |                | T  | $\vdash$        | T             | 十            | $\vdash$     | ╁╌ | T            | 十             | +~  | , M            | <del>  '</del> |      |
| 572  | 795          | .023    | "   | 12 | 13  | 14 | 15      | 3   |     | Ť  | 1              | $f^-$  | <del> `</del>   | 80            | -            | $\vdash$     | +- | †-           | 十             | 18  | +-             | 12             | 7    |
| 295  | 19.85        | 38      |     | 24 | 25  | 22 | 27      | 28  |     | "  | 82             | 1  | <del>  "`</del> | R             | -            | ╁            | ┼  | ╁            | ╁             | 1 6 | +              | _              |      |
| 325  | 9.75         | 070     |     | 35 | 37  | 38 | 33      | \$  |     | -  | *              | †  | 14              | 23            | -            | +            | ╁  | +            | ╁             | 12  | _              |                |      |
| 330  | 11.40        | .//2    | 47  | 48 | 6\$ | 8  | 18      | Z   |     | 1  | 53             | <del>                                     </del> | 10              | 54            | _            | ╁            | ╫  | ╁            | ╁             | 18  | +              | ~~             |      |
| 3    | 13.20        | .158    |     |    |     |    | ·       |     |     |  |                |  | $\vdash$        | <del> -</del> | +-           | -            | ┼  | ╁┷           | 18            |     | -              |                | J.   |
| 8    | 13.50        | .166 60 | 8   | 61 | 62  | 63 | 3       | 63  |     | 130  | 99             | +-   | 13              | 3             | -            | ├            | ╁  | +3           | 19            | 13  | 10             | _              | 1.   |
| 445  | 1395         | .177    |     |    |     |    |         |     |     | <del>                                     </del> | -              | <del>                                     </del> | $\vdash$        | 12            | 2            | 72           | +_ | +            | <del>. </del> | -   | -              |                | Τ.   |
| 28   | 200          | -204 Z  | 8   | 26 | 77  | 82 | 8       | 80  |     | 9  | 18             | 100  | 8               | 63            | -            | -            | 8  | 14           | <del> </del>  | 18  | <del>  `</del> | 23             | TA   |
| 260  | 16.80        | 121     | 89  |    | 8   |    | 16      | 26  |     | [3   | 83             | -  | 150             | M             | <del> </del> | ├            | 8  | 10           | ┼             | 18  | 00             | 18             |      |
| 623  | 8.75         | 126.    | 8   |    | 8   |    | 3       | /0/ |     | 2  | 102            | <b> </b>   | 13              | 60            | -            | <del> </del> | Ž  | V            | ·             | Ş   |                | 200            | T-   |
|      | 27           | .378    | 101 |    | 8   | 7  | 011601  | 2   |     | ~  | ///            | -  | 112             | N             | <u> </u>     |              | 13 | 100          | -             | 1   |                | 1 8            | 1    |
|      | 2.0          | 43      | 2   |    | Z   |    | 811     | 8/  |     | 13   | 02/            | -  | 121             | -             | _            | _            | 13 | N            | -             | 23  | 30             | 8              | 1 -  |
| 8    | 200          | 2%      | য়  |    | 3   |    | 7       |     |     |  |                |  | _               | ,             | _            |              | -  | <del> </del> | _             | _   | N              | 8              | ┼    |
| 8    | 22.40        | 239.    | 27  |    | 27  | Ť  | 180 (3) | 16  |     | 132  | 7              | -  | 133             | <i>b</i>      | _            | <u> </u>     | 1  | 3            | L             | 3   | 00             | 6              | 1=   |
| 18   | 32.46        | .23     | 137 |    | 8/  |    | 07/66/  | 3   | -   | 3  | 134            | -  | 123             | 12            |              | _            | -  | -            | ļ             | 163 | 7              | 13             | +    |
|      |              |         |     |    |     |    |         |     | ļ   |  |                |  | ĺ               | I             | I            | ı            | ı  |              |               |     |                |                |      |

TABLE IV. - Concluded.

( )

FUSELAGE PRESSURE TAP LOCATIONS

|                           | _  | -                  | _               | _              |                |             |            |
|---------------------------|--|--------------------|-----------------|----------------|----------------|-------------|------------|
|                           | 88   |                    | 6/              | 28             | 37             | 4           | 8          |
|                           | 38   | 9                  | 0               | 0              | 0              | 0           | 1          |
|                           | 36   |                    |                 |                |                |             | Π          |
|                           | 3  |                    |                 | Π              | Π              | Π           | Γ          |
|                           | R  |                    |                 |                |                |             | Γ          |
|                           | 8  | 8                  | 191             |                |                |             |            |
| 8                         | 1  |                    |                 |                |                |             |            |
| 66                        | 62   |                    |                 |                |                |             | Γ          |
| 9                         | \$   | 13                 |                 | 12             | \$             | À           | Γ          |
| RADIAL LOCATION ~ DEGREES | 162  |                    |                 |                |                |             | Γ          |
| 3                         | 13   |                    |                 |                |                |             |            |
| 17                        | 12/  |                    |                 |                |                |             |            |
| Ú                         | 8  | 152                | 69/             | B              | 83             | \$          |            |
| 7                         | 140  |                    |                 |                |                |             |            |
| 74/2                      | 135  | 12/                | 16/162          | 13/            | 18/ 182        | 24/6        |            |
| 3                         | 120  | 12/2/              | 16              | 11/12          | 181            | 18          | 20 80      |
|                           | 9/   |                    |                 |                |                |             | 8.8        |
|                           | Ś  | 147 46 145         | 03 (2) (6)      | 110/10/10      | 138 179 180    | JEB 659 150 |            |
| Ð                         | 8  | 188                | 8               | 631            | 13             | 63          |            |
|                           | 8  | ¥                  | 8               | 831            | 178            | 188         |            |
|                           | 18   |                    |                 |                |                |             |            |
|                           | 8  | *                  | 67              | 12             | 17             | 18          |            |
|                           | 8  |                    |                 |                |                |             |            |
|                           | 0  | 15                 | X               | 3              | 7              | 2           |            |
| ×                         | X/6  | 779                | 128             | 879            | 126            | .20 BC      | 8          |
| 768                       | Photo  | 37.35              | 380             | 47.25          | 62             | 3           | 8          |
| QBUTER- M.                | FULL March 1/2 0 20 40 55 70 90 105 110 130 135 140 150 151 156 162 165 169 14 180 351 350 360 175 | 245 57.35 ,779 445 | 1300 380 821 52 | B15 415 879 KL | MED 429 921 /2 | 180 411     | 530 At 999 |
|                           |  |                    |                 |                |                | -24         | _          |

| N K          |      | 0       | `   |      | 34     | ·    |          | 19      |         |             | 88    |             |          | 2//    |     |
|--------------|------|---------|-----|------|--------|------|----------|---------|---------|-------------|-------|-------------|----------|--------|-----|
| \$\$<br>\$\$ |      | 6       | 0   |      | /3     | 77   |          | ħ       | 7       |             | 71    | 14          |          | 71     | 13  |
|              |      |         |     |      |        |      | .955     | 255     | 897     | 7.00        |       | 205 296     |          | •      |     |
|              |      |         |     | .885 | 228    | 24/  | -9.9     | 152     | 797     | .953        | 282   | 20%         | 8        | 3/0    | 628 |
|              | ·    |         |     | 8    | 228    | 3%   | 879 -919 | 253     | 302 502 | 8           | 182   | 28          |          | 30     | 322 |
| VS           |      |         |     | 385  | 227    | 239  | 63       | 252     | 38      | 188         | 280   | 293 294     | 026.028. | 328    | 321 |
| LOCATIONS    |      |         |     | 8    | 222    | 238  | 8%.      | 152     | 260     | 780 808 857 | 279   | 292         | 775      | 307    | 320 |
| 100          |      |         |     | .700 | 225    | 237  | 169.     | 250     | 677     | .760        | 378   | 162         | 13       | 90€    | 3/9 |
| 720          | .793 | 2/6     | 1   |      |        |      |          |         |         | 402 .565    | 277   | 88          | 85       | 305    | 318 |
| i I          | 127  | 512     | 1   | 169. | 722    | 236  | 390      | 2.19    | 282     | 402         | 276   | 682         | \$       | 32     | 317 |
| PRESSURE     | .633 | 2/4     | ١   | :362 | 223    | 235  | .246     | 245     | 197     | 17.7        | 202   | 388         | 8        | 303    | 3/6 |
|              | :547 | 2/3     | ١   | .229 | 22     | 1331 | .086.163 | 200     | 260     |             | 274   | 182         | 8        | 302    | 315 |
| WING         | 624. | 2/2     | 1   | 7860 | 221    | 88   | .086     | 346     | 259     | 111. 880.   | 273   |             |          | 38     | 3/4 |
|              | W.   | Ŕ       | -   | 8    | 220    | 232  | 020 020  | 245     | 288     | ·020 · C40  | 272   | 282 582 188 | 8        | 38     | 3/3 |
| LEFT         | E11  | 210     | 1   | .020 | 29     | 23/  |          | 244 245 | 257     | 020         | 727   | 280         | .020     | 88     | 3/2 |
|              | .04/ | 209     | 1   | 010. | 218    | 230  | 90.      | 243     | 256     | 90          | 22    | 283         | 0/0      | 300    | 3// |
|              | 0    | 308     | 1   | 0    | 217    |      | 0        | 242     |         | 0           | 697   |             | v        | 237    |     |
|              | X/c  | 20      | BOT | x/c  | 100    | EST  | 1/2      | 902     | BOT     | ×           | Ø     | 100         | X/C      | Q      | BOT |
| %            |      |         |     |      | 04/682 |      |          |         |         |             | 220   | •           |          |        |     |
| 7            |      | .235/10 |     |      | 8      |      |          | 34 170  |         |             | . KZ) |             |          | 234.28 |     |

TABLE V. - Concluded.

| W. W.     |              | 2          | C7/        |               | •           | 8   |            | B   | ,   |            | 8       |     |       | *       |     |      | 8   |    |
|-----------|--------------|------------|------------|---------------|-------------|-----|------------|-----|-----|------------|---------|-----|-------|---------|-----|------|-----|----|
| 24        |              | 3          | ŧ          |               | 6           | Ø   |            | 9   | 6   |            | 0/      | 8   |       | 90      | 1   |      | 4   |    |
|           |              |            |            |               |             |     |            |     |     |            |         |     |       |         |     |      |     |    |
|           |              |            |            | L.            | <u> </u>    |     |            |     |     |            |         |     |       |         |     |      |     | ·  |
|           | ş            |            | 347        | \$            |             |     |            |     |     |            |         |     |       |         |     |      |     |    |
| 3.W.S     | 88.          | 385        | **         | ģ             |             |     |            |     |     |            |         |     |       |         |     |      |     |    |
| LOCATIONS | 83           | 334        | 345        | 83            |             |     |            |     |     | 07         |         | 38  |       |         |     |      |     |    |
| 707       | 175          | 333        | WE 34      | 30 278        |             |     | 8          | 357 | 3%  | 8          | 376     | 385 |       |         |     |      |     |    |
| 747       | 22.          |            |            | 32.           | <b>2</b> 5E | 343 | 839        | 358 | 382 | 250        | 375     | 384 |       |         |     |      |     |    |
| 1         | 13           |            |            | .280          | 33/         | 77% | 82         |     | 38  | 32.00      | 32      | 383 | 238   | 324     | 100 |      |     |    |
| PRESSURE  | ğ            |            |            | an.           | 330         | 188 | 39         | 350 | 363 | <b>B</b>   | 375     | 38  |       |         | doo |      |     |    |
| PRES      | Ŕ            |            |            | 8             | 229         | 326 | 8          | 353 | 362 | 88         | 372     | 188 | B3 62 | 392     | 399 |      |     |    |
| MING ,    | <i>081</i> : |            |            | 8             | 328         | 239 | <i>B</i> : | 325 | 38/ | 637        | 37/     | 38  | .365  | 166     | 38  |      |     |    |
| W         | 90.          |            |            | <i>30</i> ·   | 327         | 338 | <u>8</u>   | 38  | 360 | 80         | 370     | 379 | 157   | 168 066 | 397 |      |     |    |
| LEFT      | 051 90 020   |            |            | 031. 30. 020. | 326         | 337 | 020        | 350 | 359 | 0.00.00.00 | 368 369 | 328 | 180   | 657     | 396 |      |     |    |
| 7         | 0/0          |            |            | 920           | 325         | 336 | 90         | 340 | 358 | 0/0        |         | 377 | 020   | 338     | 395 | .723 | 403 |    |
|           | 0            |            |            | 0             | 324         |     | 0          | 368 |     | 0          | 367     |     | 0     | Œ       |     | .#1  | 402 |    |
|           | 1/2          | 100        | <i>801</i> | 1/2           | B           | 807 | <i>%</i>   | 18  | 807 | ž          | 90      | BOT | ķ     | B       | B   | ž    | 200 | an |
| %         |              | 641 300 DD |            |               | 673 355     |     |            | 355 |     |            | 27      |     |       | 13      |     |      | 163 |    |
| 1         |              | <u>z</u> . |            |               | 673         |     |            | 8   |     |            | 8       |     |       | 226-    |     |      | 9   |    |

TABLE VI.

OBBITER VERTICAL TAIL & SPEED BONKE PRESSURE TAF LOCATIONS

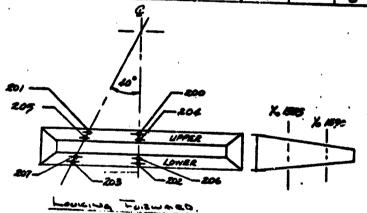
| VEETICEL | VERTICAL (LHOMY) |              |     |                 |         | x/c,     |                    |         |      |                                    |      |     |              |
|----------|------------------|--------------|-----|-----------------|---------|----------|--------------------|---------|------|------------------------------------|------|-----|--------------|
| 2 Sth    | E. Model         | 11           | 0   | .025            | .08     | .15      | 3                  | :52     | 589  | 06. 87. 88. 52. 08. 71. 50. 820. 0 | 8.   | 342 | 37.5<br>37.5 |
| 550      | 16.5             | .153         | 430 | 431             | 432     | E\$ 2E\$ |                    | 434 436 | 438  | 160                                |      | 8   | 8            |
| 909      | 080              | .316         | 860 | 438 439 410 441 | 4,00    |          | 442                | 443     | 74%  | 570                                | 777  | 6   | 11           |
| 645      | 19.35            | .458         |     |                 |         |          |                    |         | PPDI | SON                                | 1446 | Ė   | 97           |
| 63       | 222              | .600 407 448 | 100 | 870             | 40      | 88       | de 450 451 452 des | 452     | 653  | ded                                | 250  | 6   | 50           |
| 720      | 21.6             | .720         |     |                 |         |          |                    |         | 1453 | 1954                               | 2311 | 3   | 35           |
| 765      | 22.95            | .820         | 350 | 456 457         | 658 459 | 650      | 460                | B       | 462  | <b>CM</b> 3                        | 711  | 6   | 15           |
| 792      | 23.76            | .925         | 465 | 466 467         | 467     | 897      | 699                | 110 00  | 112  | 210                                | 92   | 6   | 20           |
|          |                  |              |     |                 |         |          |                    |         |      |                                    |      |     |              |

|                | _                | _    |           |      | _    |      | -       |
|----------------|------------------|------|-----------|------|------|------|---------|
|                | y K              | 5    | 0/        | 51   | 92   | 92   | 30      |
|                | 12 S             | 5    | 5         | 5    | 5    | 5    | 6       |
|                | 8                | 805  | 80        | 85   | 820  | 82   | (a)     |
|                | . es             | 100  | 809       | BU   | 819  | 834  | RX      |
| 8              | 8                | 893  | 828       | 613  | 818  | 823  | 828     |
| 1/50,          | .25              | 85   | BOK   BOT | 28   | 218  | 822  | 822 628 |
|                | 0/               | 801  | 208       | 8//  | 816  | 821  | RX      |
|                | 85/ <sub>U</sub> | 0//- | .254      | .407 | .547 | .706 | 758     |
| Geake (Lesion) | 2 Mast           | 0.81 | 18.9      | 8.61 | 20.7 | 21.6 | 22.5    |
| SPEED B        | 2 50ME           | 009  | 630       | 999  | 6%   | 720  | 750     |

### TABLE VII.

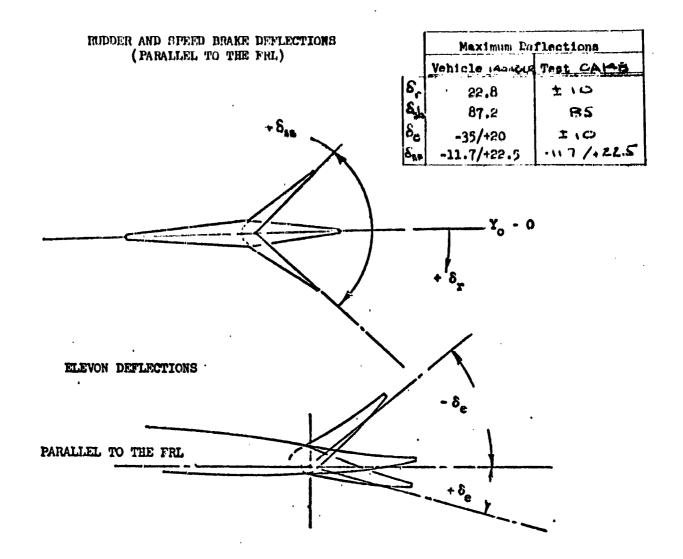
#### BOOYFLAP PRESSURE TAP LOCATIONS

| ORBIT         | EL-X.          |       | 0-1 | ASSRESS. | ] "           |       |
|---------------|----------------|-------|-----|----------|---------------|-------|
|               | Model<br>Scale |       | 0   | 40       | 146.<br>74.53 | S.No. |
| 1555 W        | 46.65          | 1.018 | 200 | 201      | -             | MPS   |
| <u> 1955C</u> | 76.60          | 1.018 | 202 | 203      |               |       |
| 1590 U        | 47.70          | 1.046 | 204 | 205      | 2             | -     |
| 590L          | 47.70          | 1.046 | 206 | 207      |               |       |

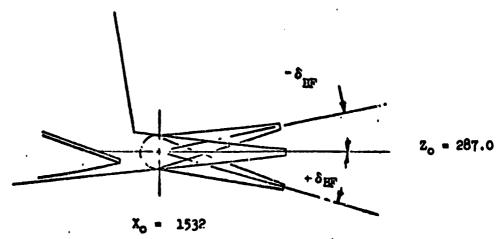


a. Orbiter Axis Systems

Figure 1. - Axis systems and sign conventions

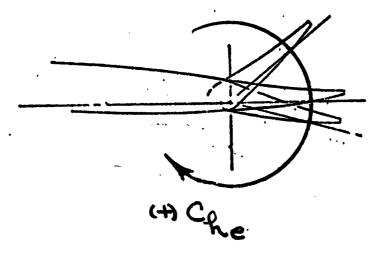


#### BODY FLAP DEFLECTIONS



b. Definition of Angular Measurements

Figure 1. - Continued.



c. Elevon Hinge Moment Sign ConventionFigure 1. - Concluded.

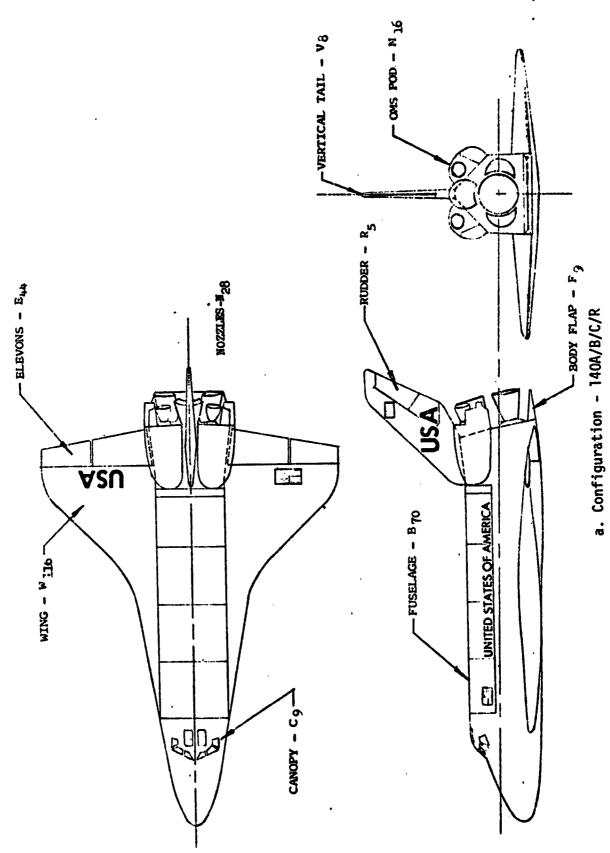
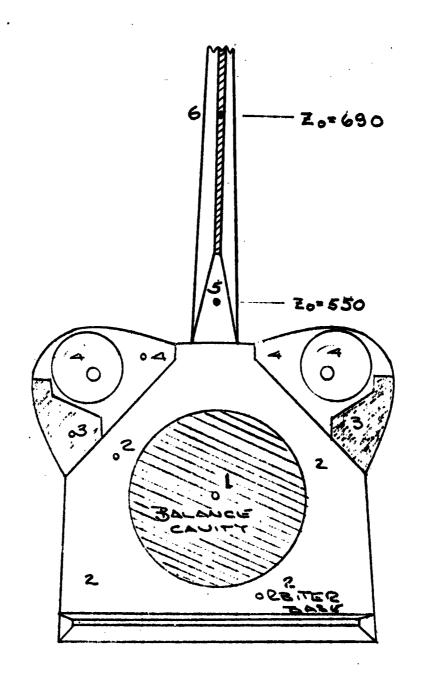
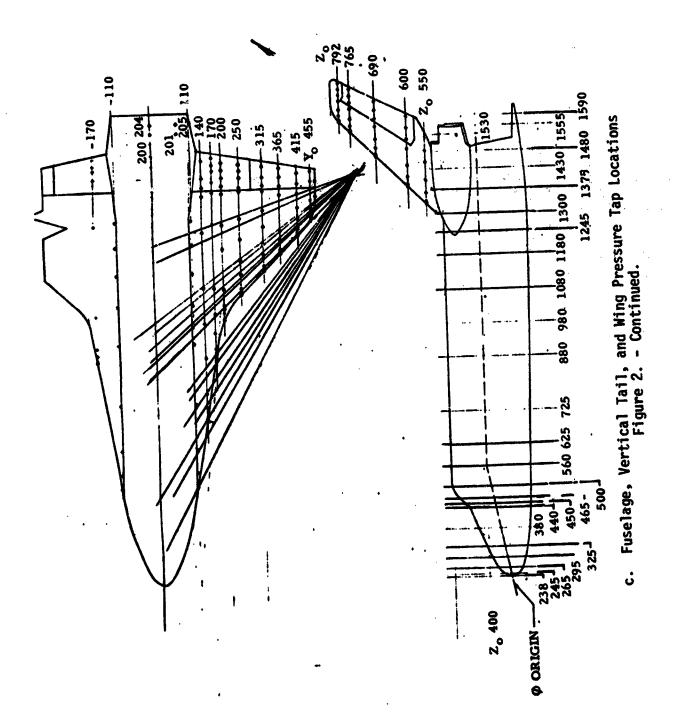


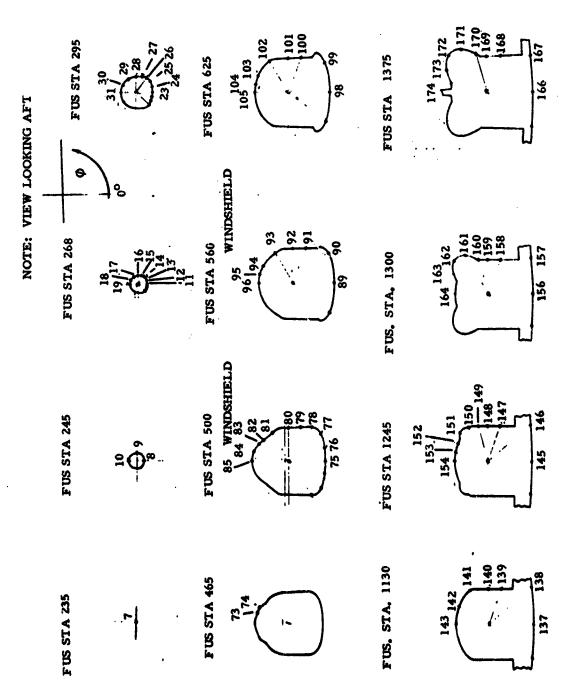
Figure 2. - Model sketches.



| AREA NO.           | PROJECTED<br>BRIAL VALUE |
|--------------------|--------------------------|
| <b>\Delta</b> \(\) | 0 076699 42              |
| A2                 | 0.21569542               |
| <b>A3</b>          | 0 034072 (16             |
| Δ.4                | 0074167(42               |

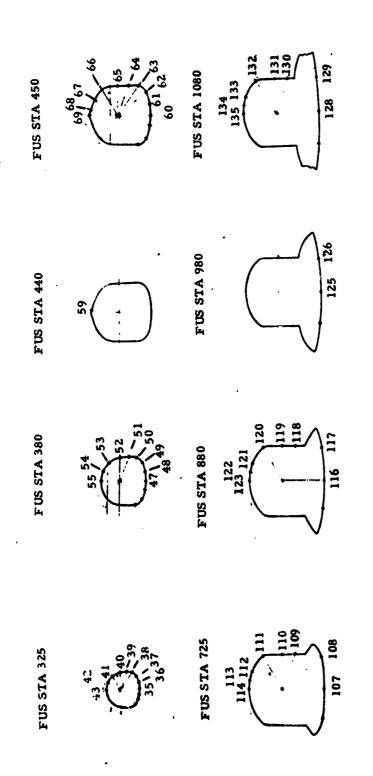
b. Base Pressure Taps and AreasFigure 2. - Continued.





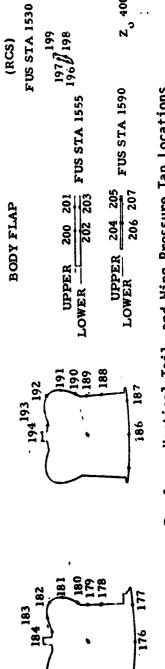
c. Fuselage, Vertical Tail, and Wing Pressure Tap Locations Figure 2. - Continued.

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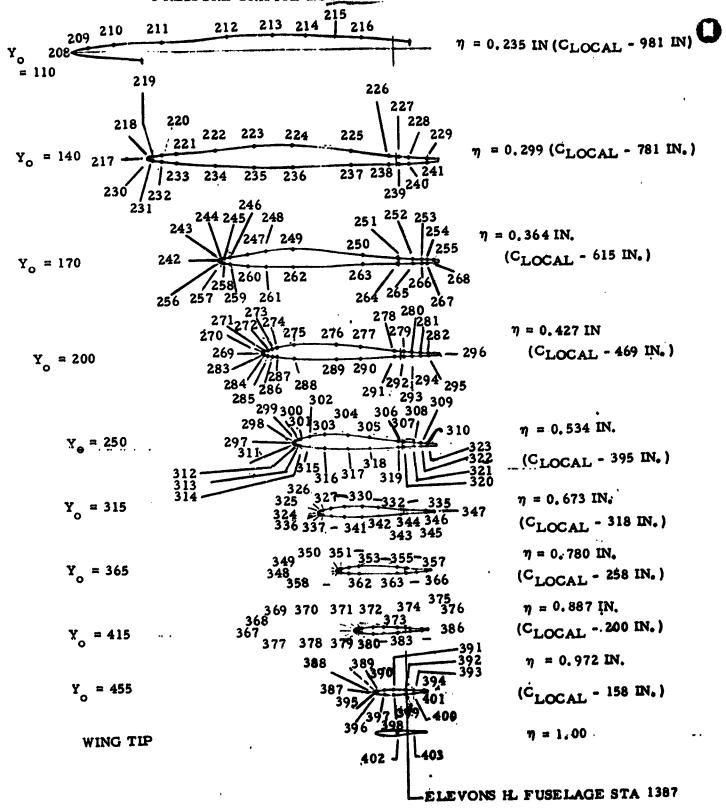


FUS STA 1480

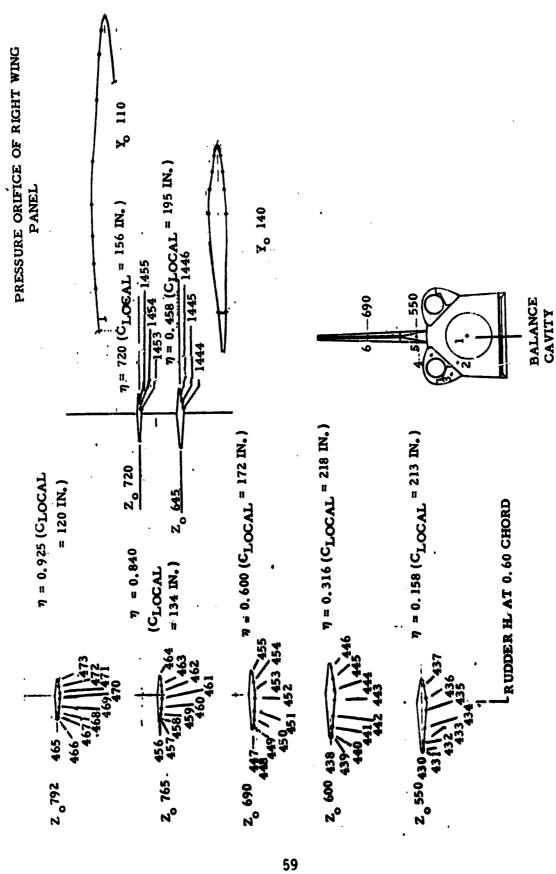
FUS STA 1430

. Fuselage, Vertical Tail, and Wing Pressure Tap Locations Figure 2. - Continued.

# PRESSURE ORIFICE LOCATION OF LEFT WING PANEL.



c. Fuselage, Vertical Tail, and Wing Pressure Tap Locations Figure 2. - Continued.

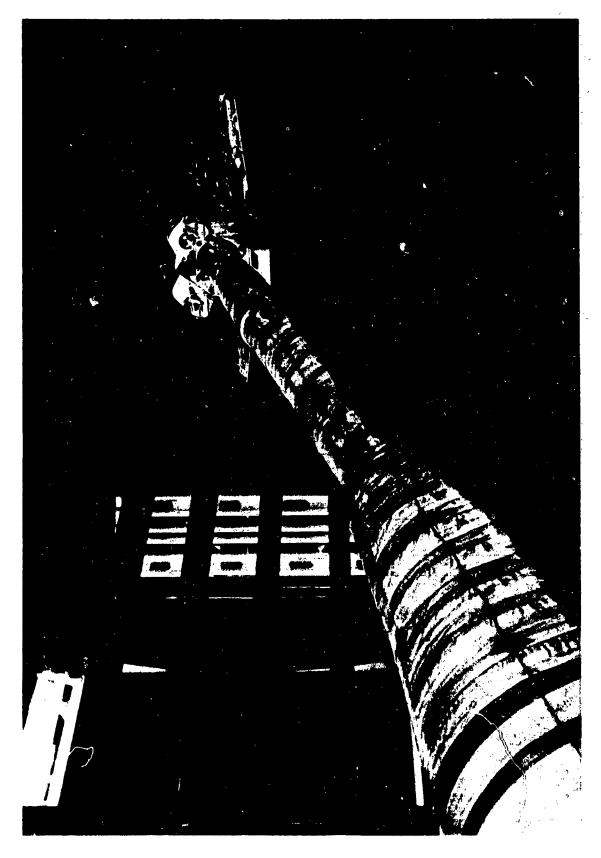


Fuselage, Vertical Tail, and Wing Pressure Tap Locations

Figure 2. - Concluded.



a. Three Quarter Front View of model 47-0 in the ARC 11  $\times$  11 UPWT Figure 3. - Model installation photographs.



b. Three Quarter Rear View of Model 47-0 in the ARC ll x ll UPWT Figure 3. - Concluded.

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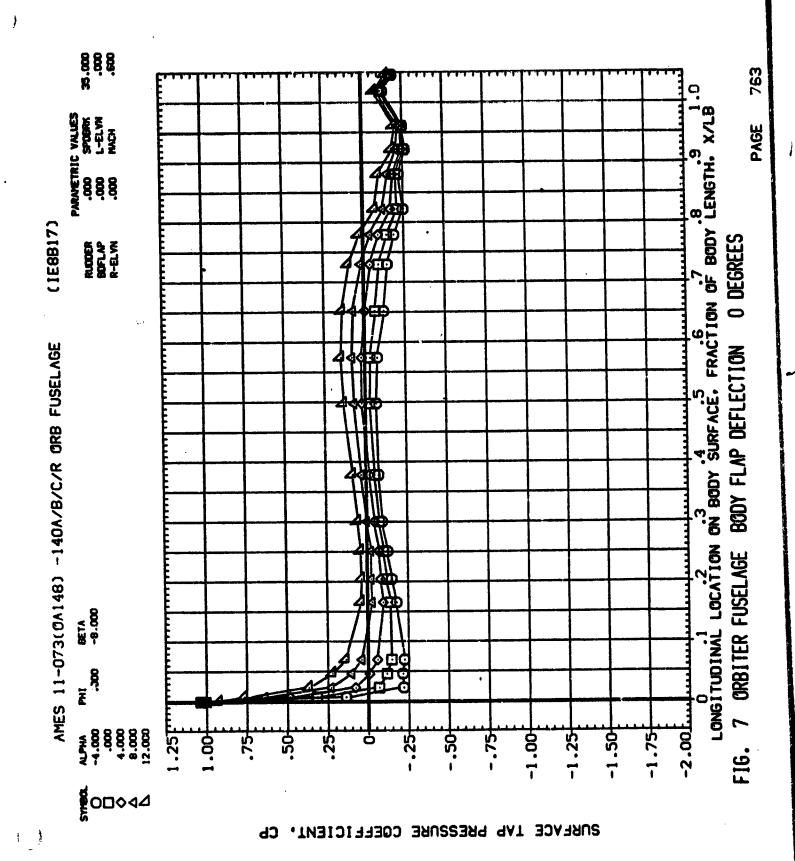
#### DATA FIGURES

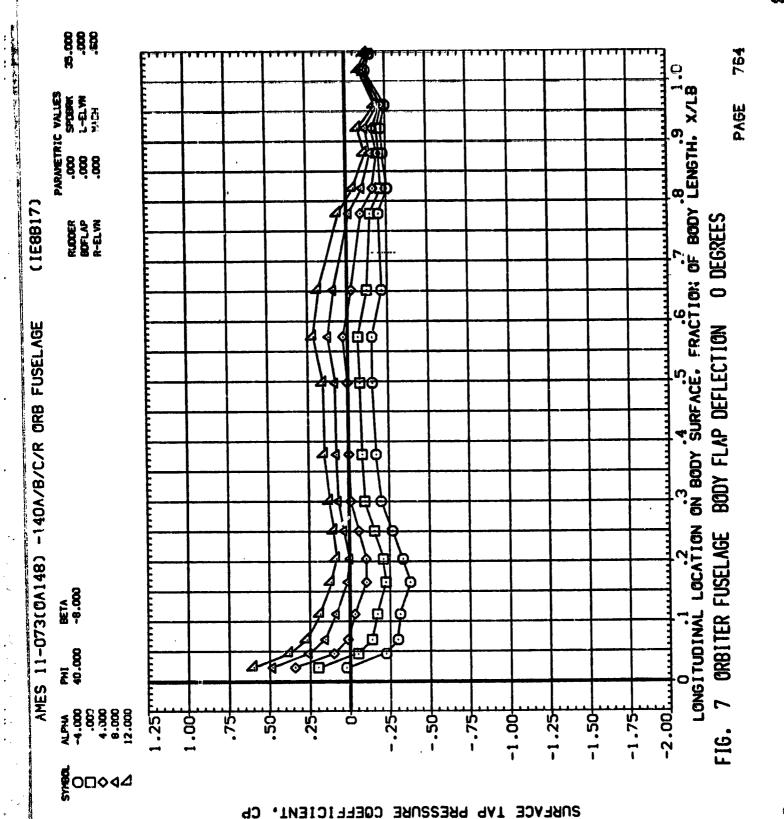
Volume 1 Plotted force data

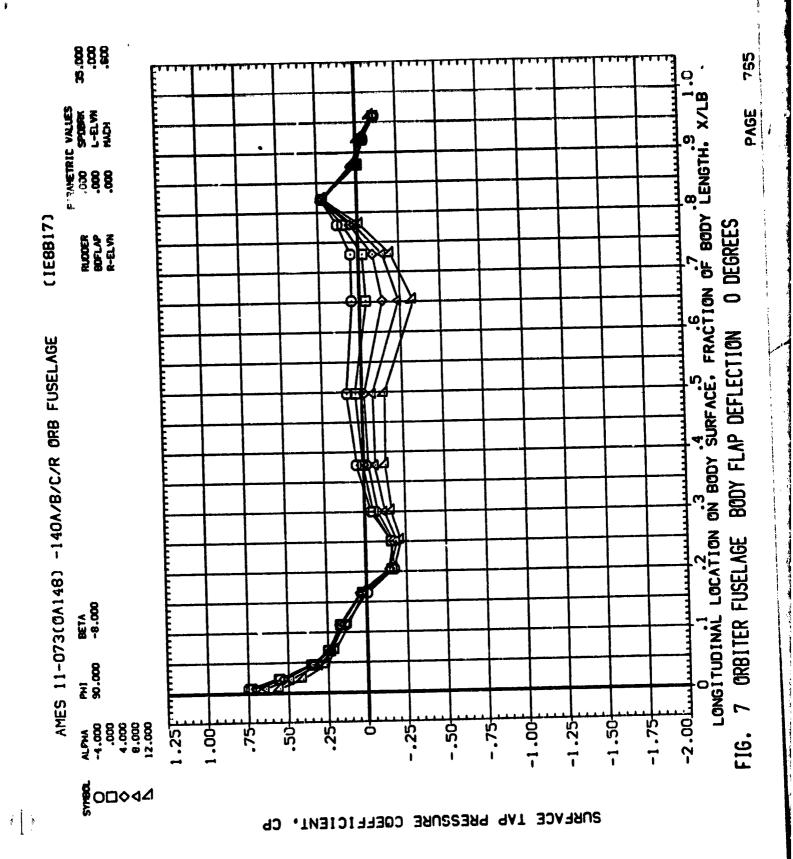
Volume 2 Plotted pressure data

Tabulations of plotted data are available on request from Data Management Services

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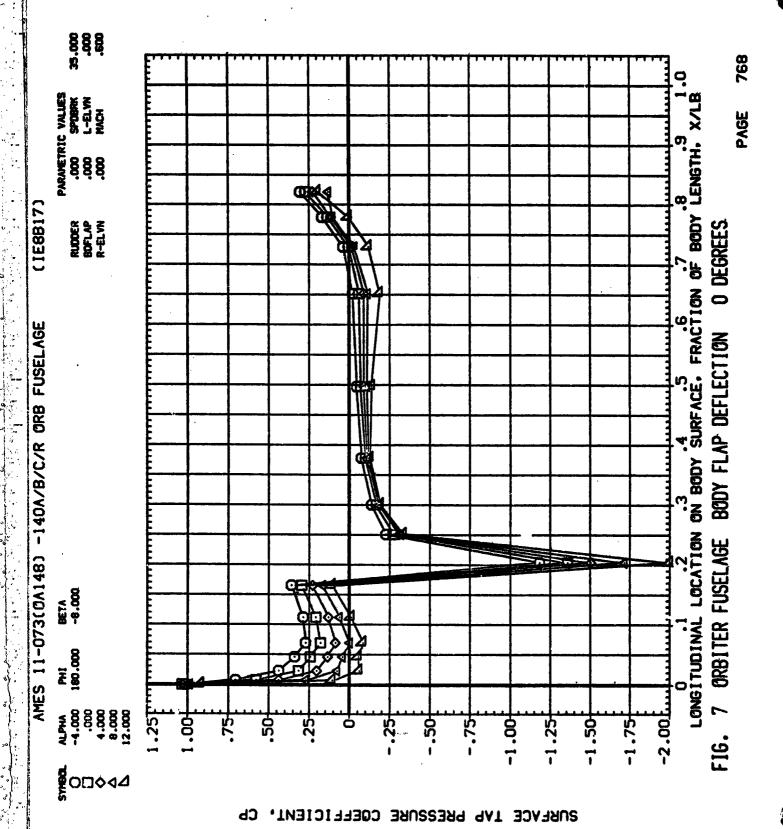


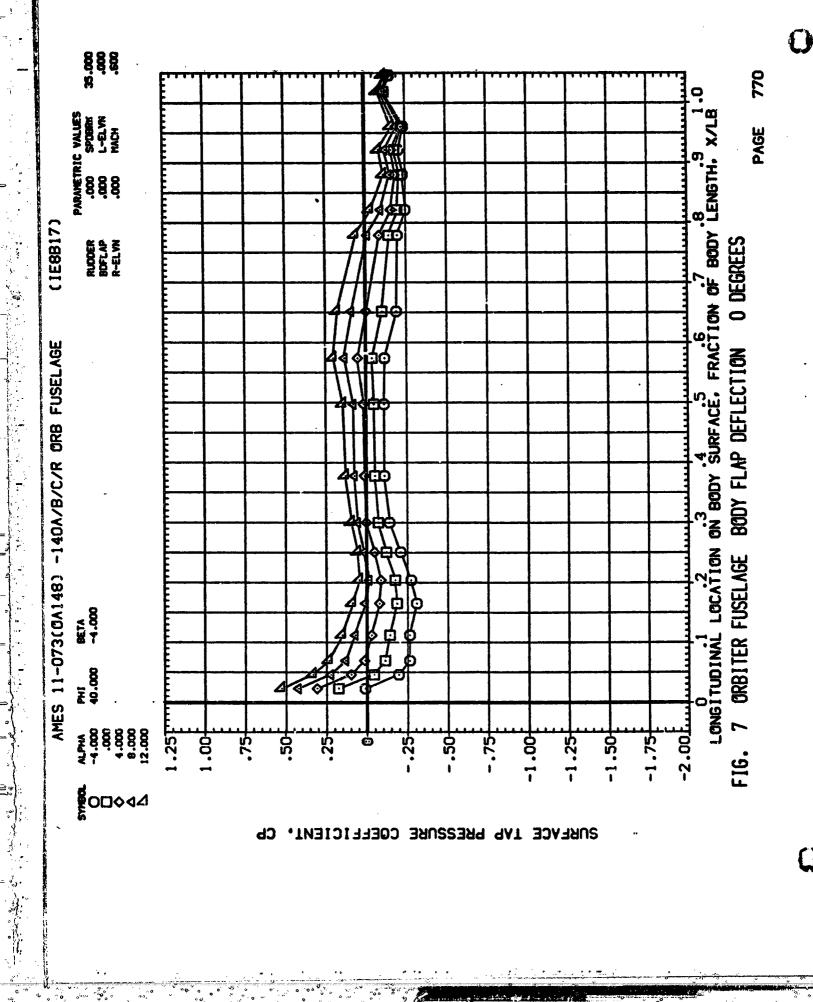


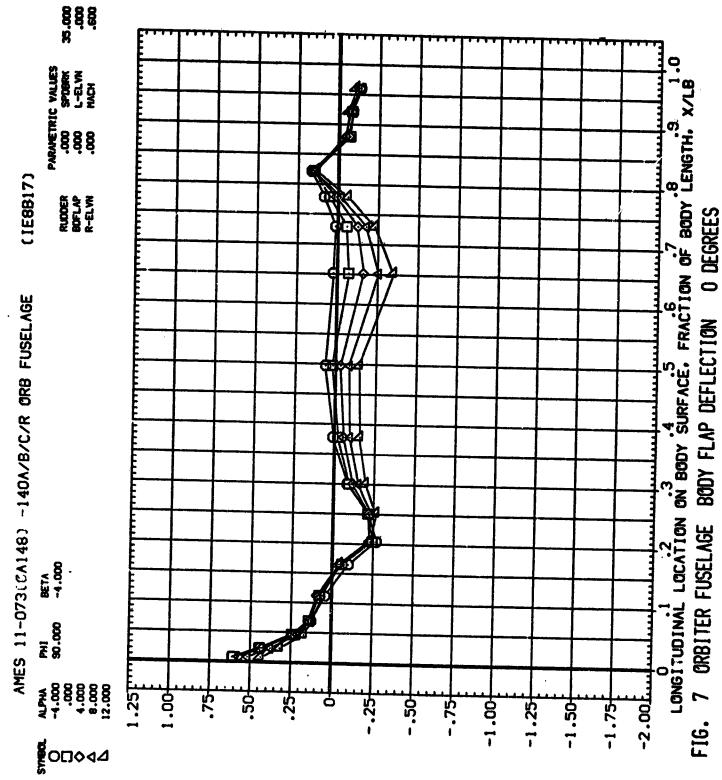
SURFACE TAP PRESSURE COEFFICIENT,

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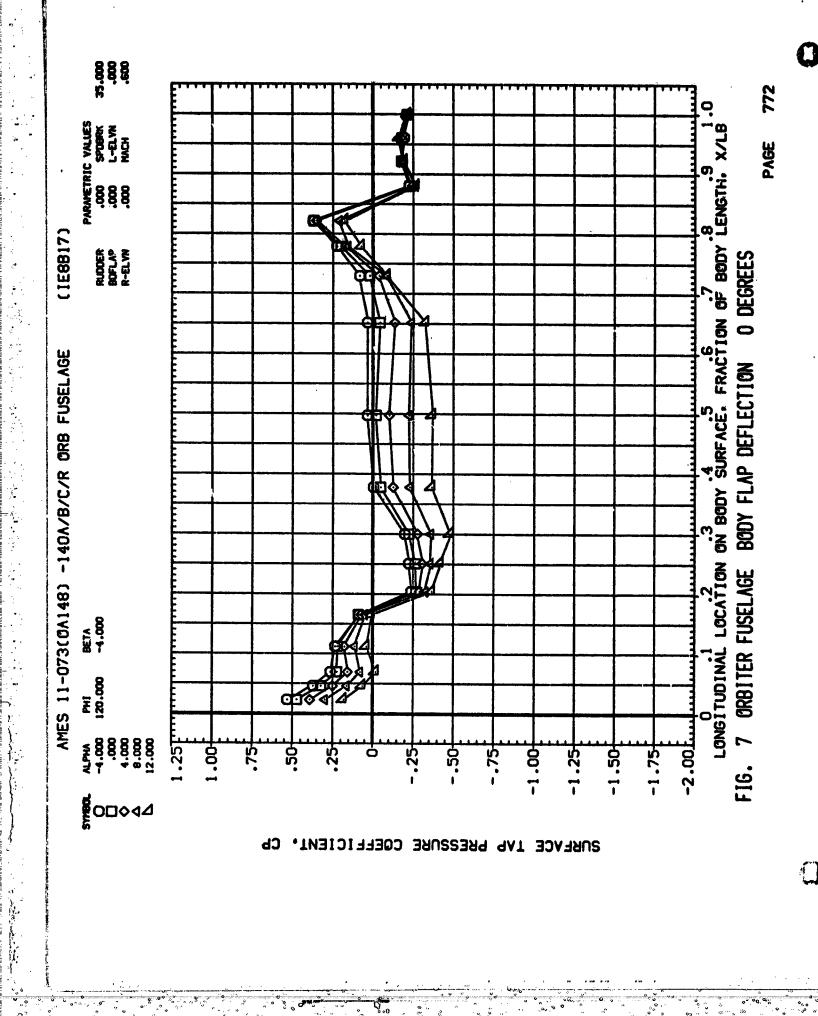


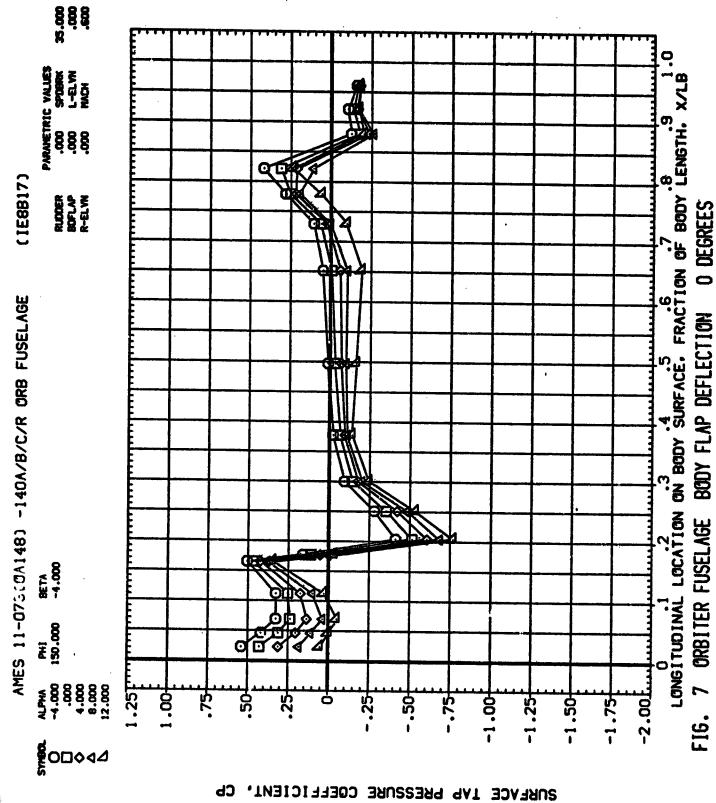


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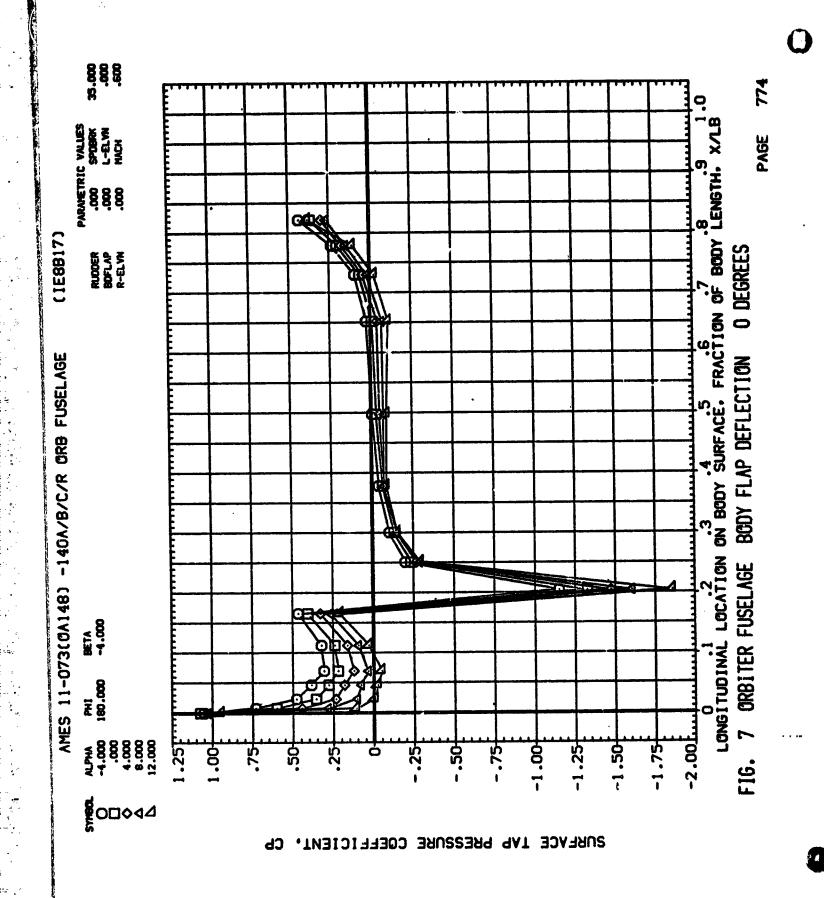
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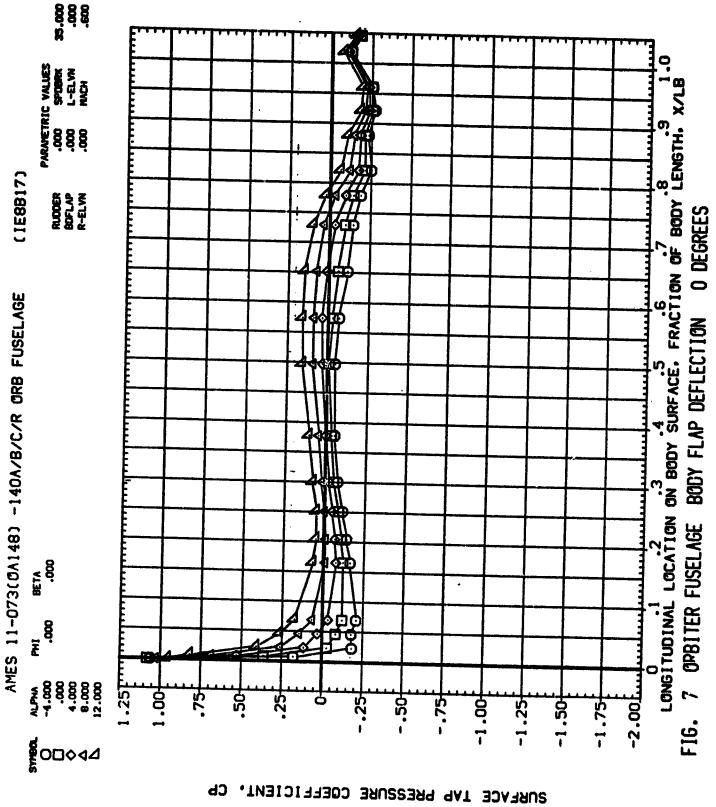
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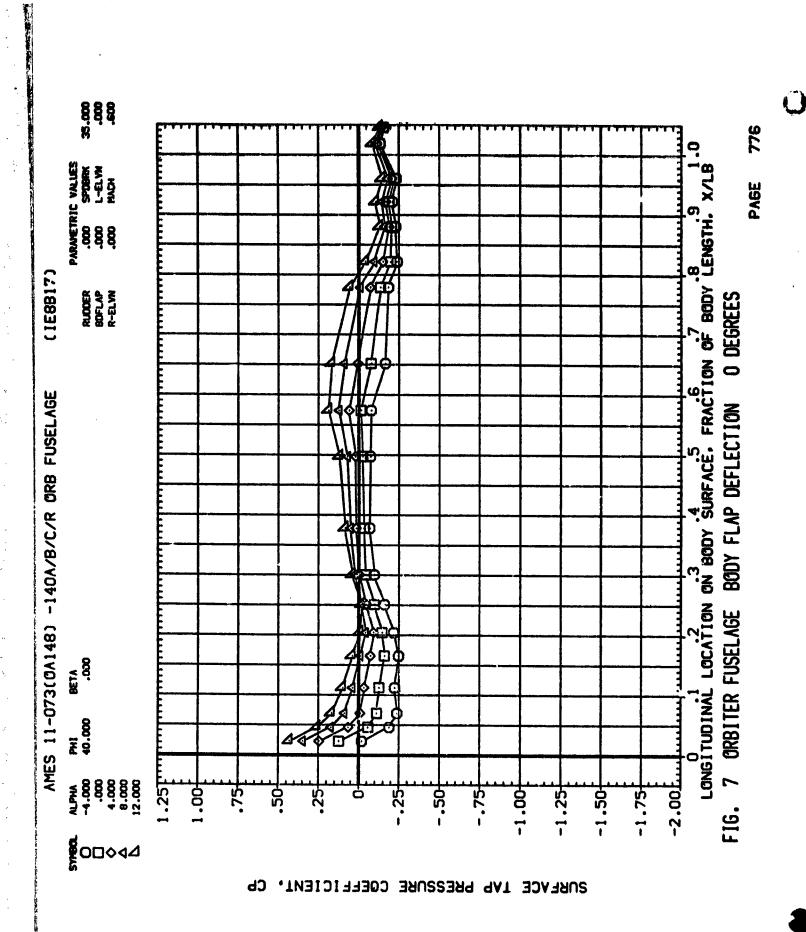


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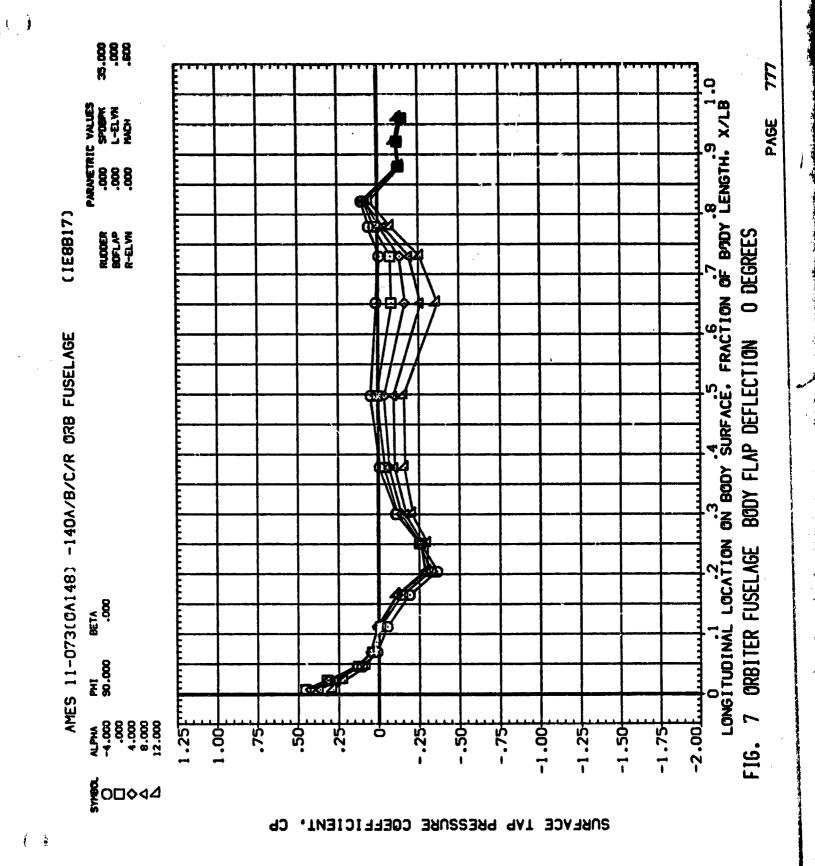


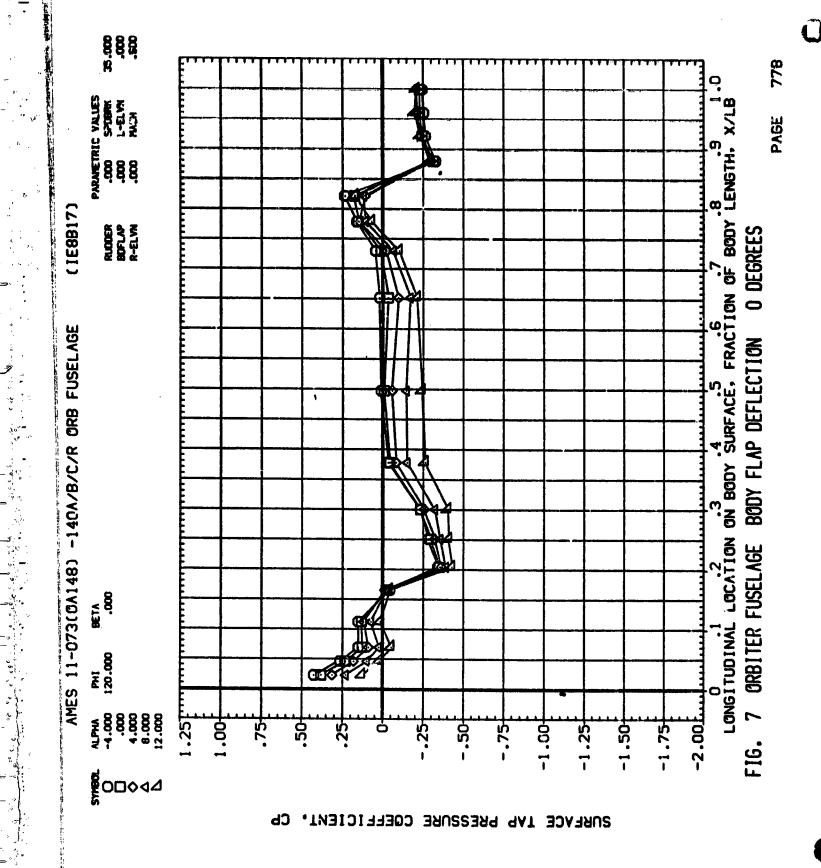


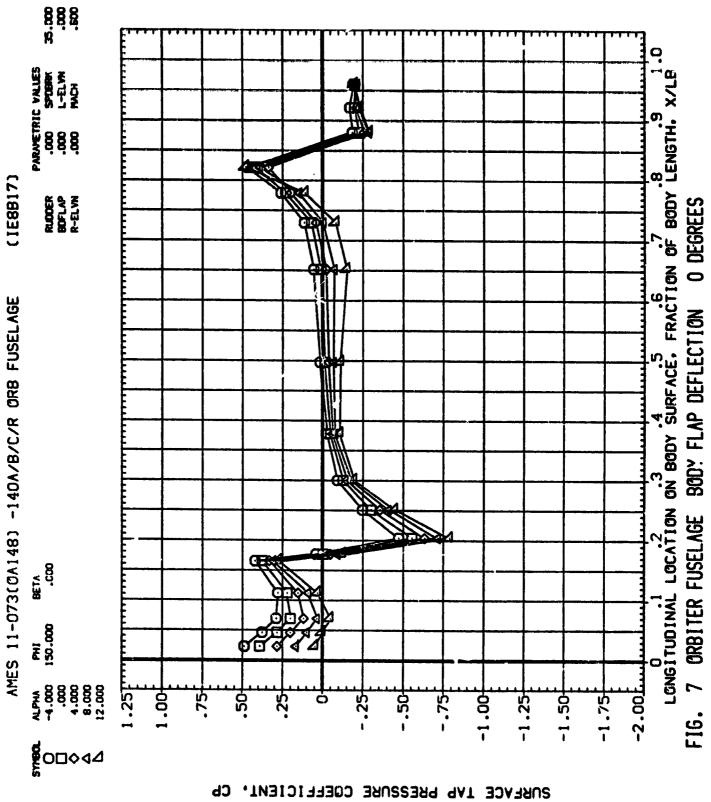
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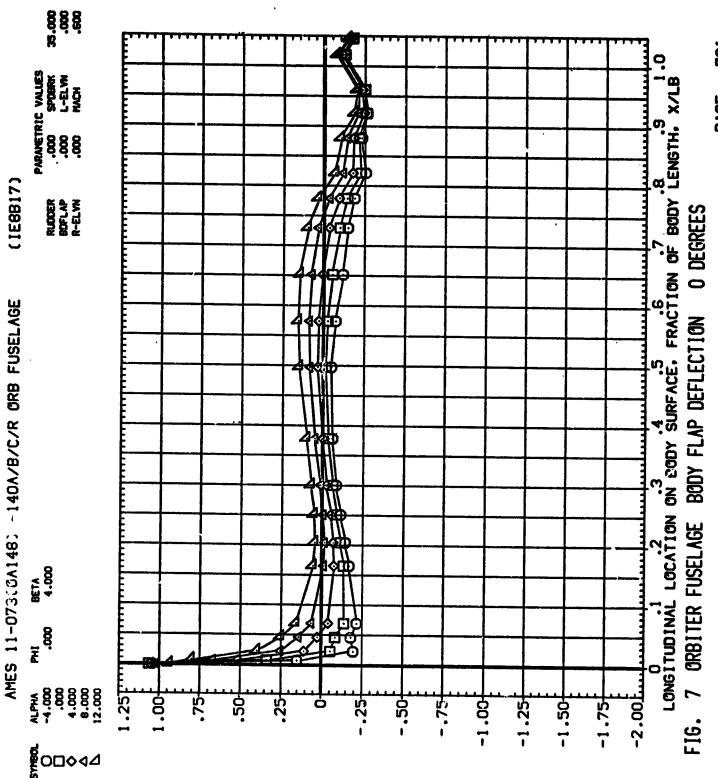


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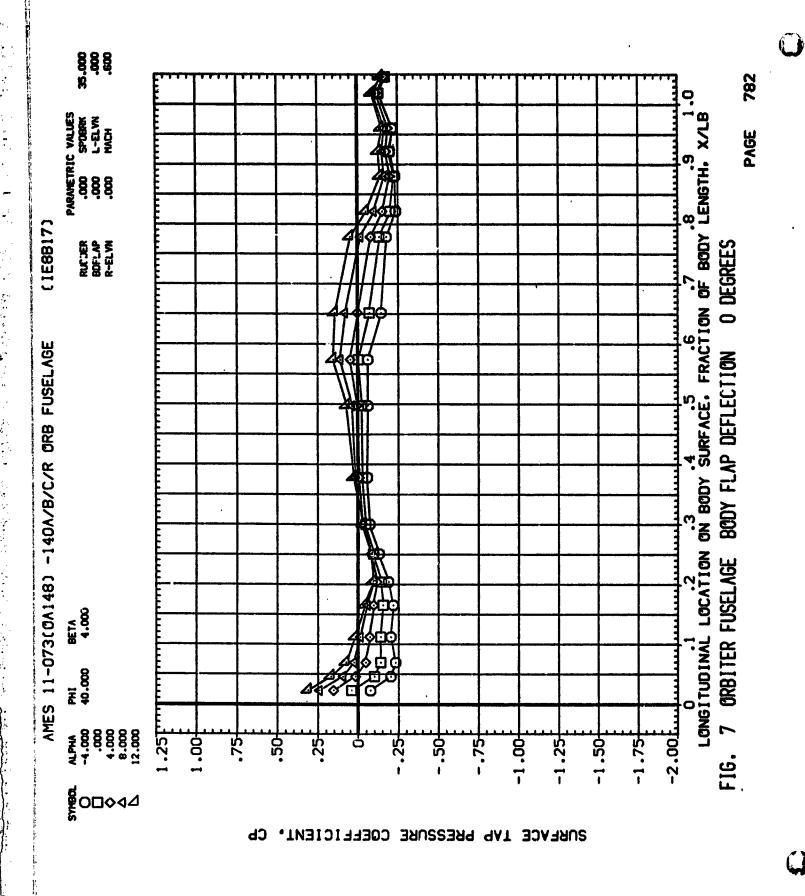
(1E8B17) 8. 8.8.8. 780 LONGITUDINAL LOCATION ON BODY SURFACE, FRACTION OF BODY LENGTH, X/LB PARAYETRIC VALUES .000 SPOBRK .000 L-ELVN .000 NACH PAGE RUDDER BOFLAP R-ELYN O DEGREES AMES 11-073(0A148) -140A/B/C/R ORB FUSELAGE BODY FLAP DEFLECTION ORBITER FUSELAGE 8ETA .000 7±1 180.000 ALPHA -4.000 -000 4.000 8.000 1.00 -2.00£ -1.00 -1.25 -1.50 -.50 -.75 -1.75 F16. **€**0□◊4△ SURFACE TAP PRESSURE COEFFICIENT,

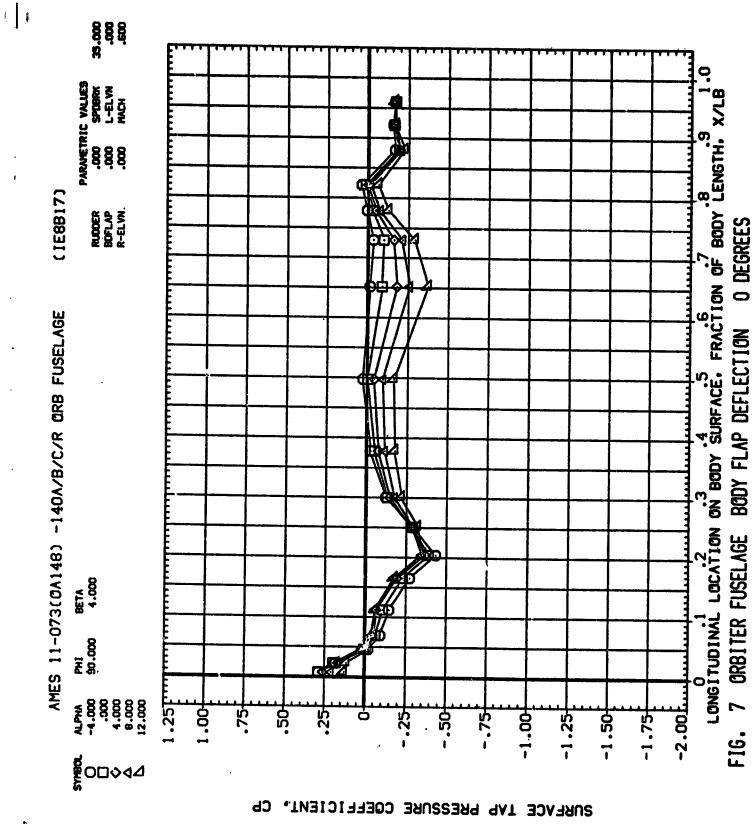


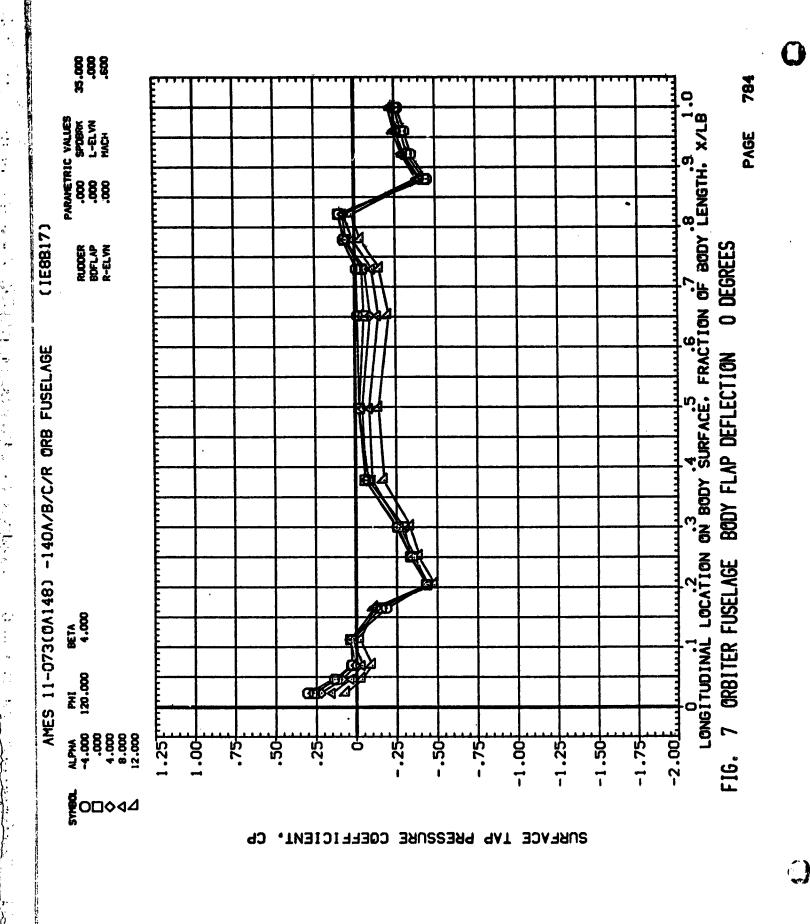
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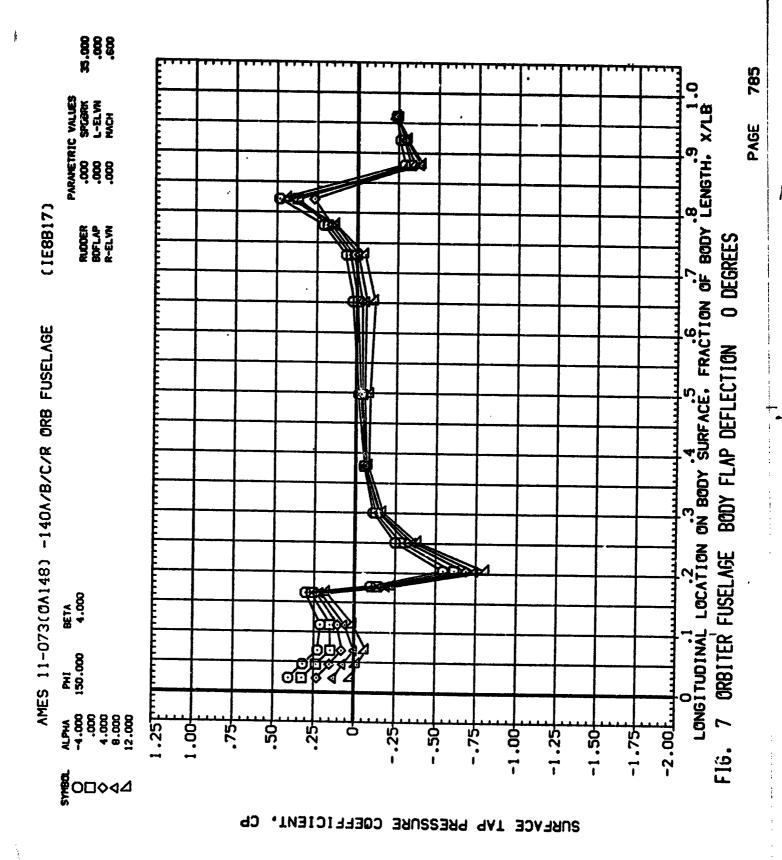
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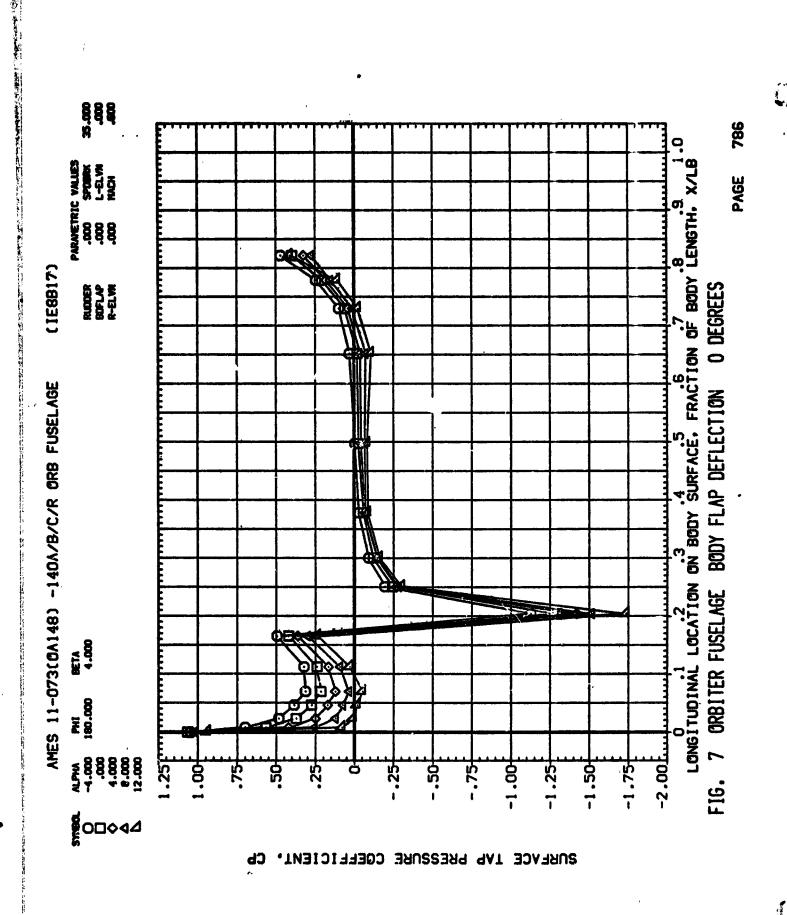
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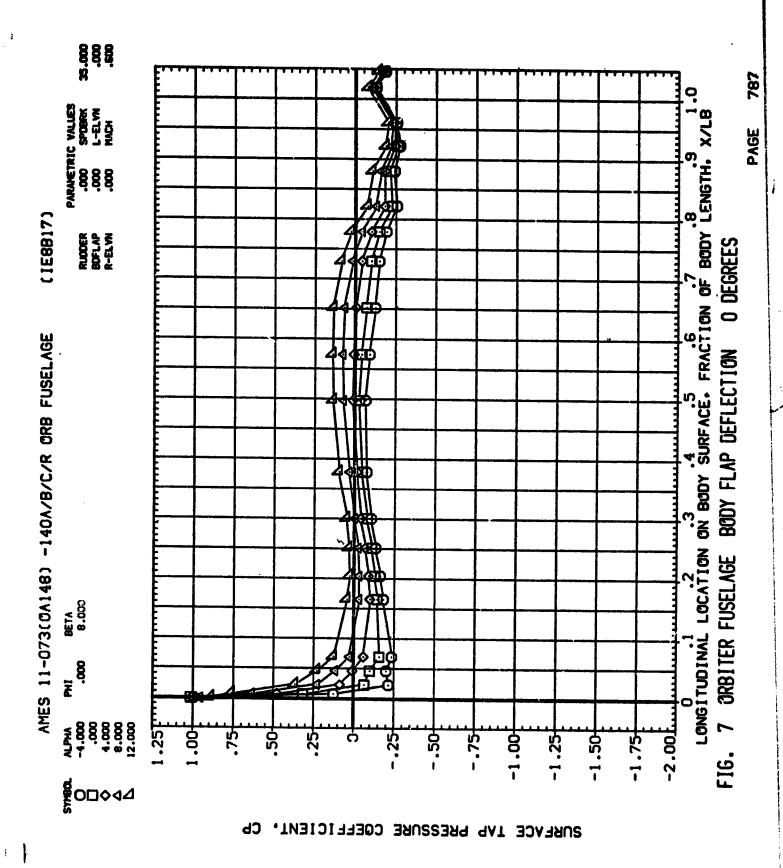


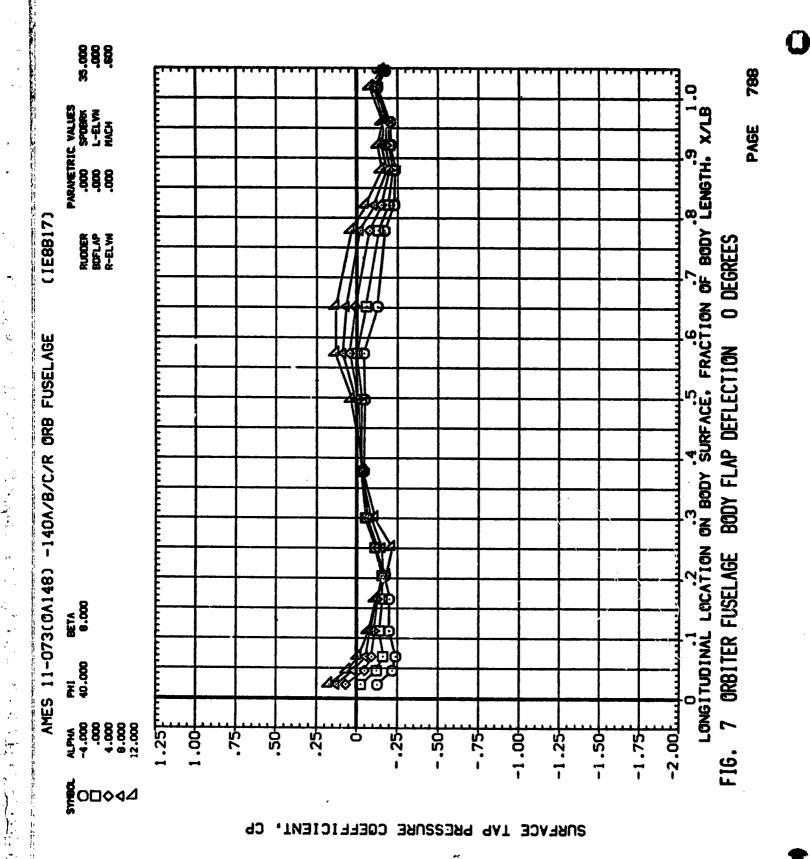












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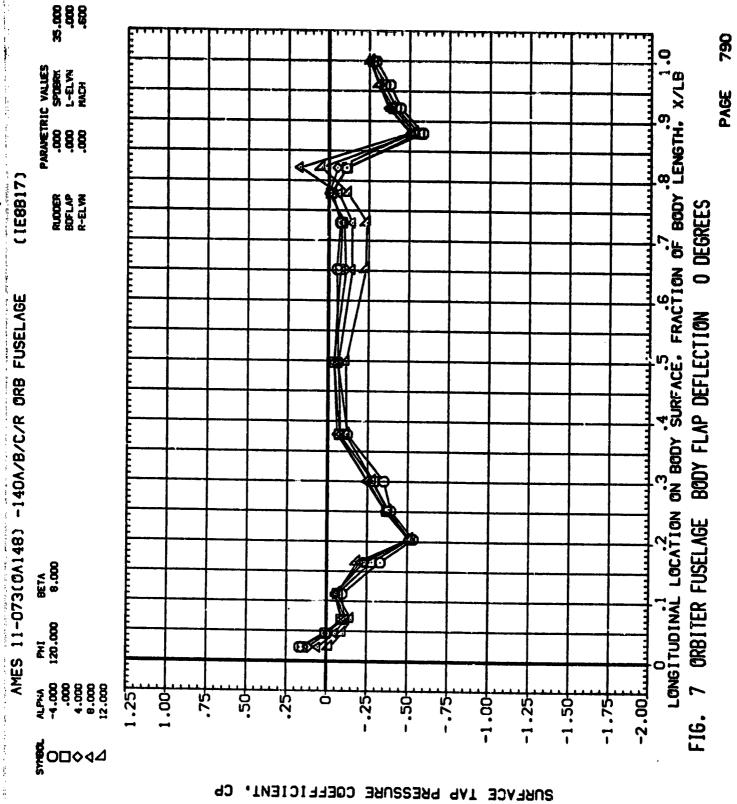
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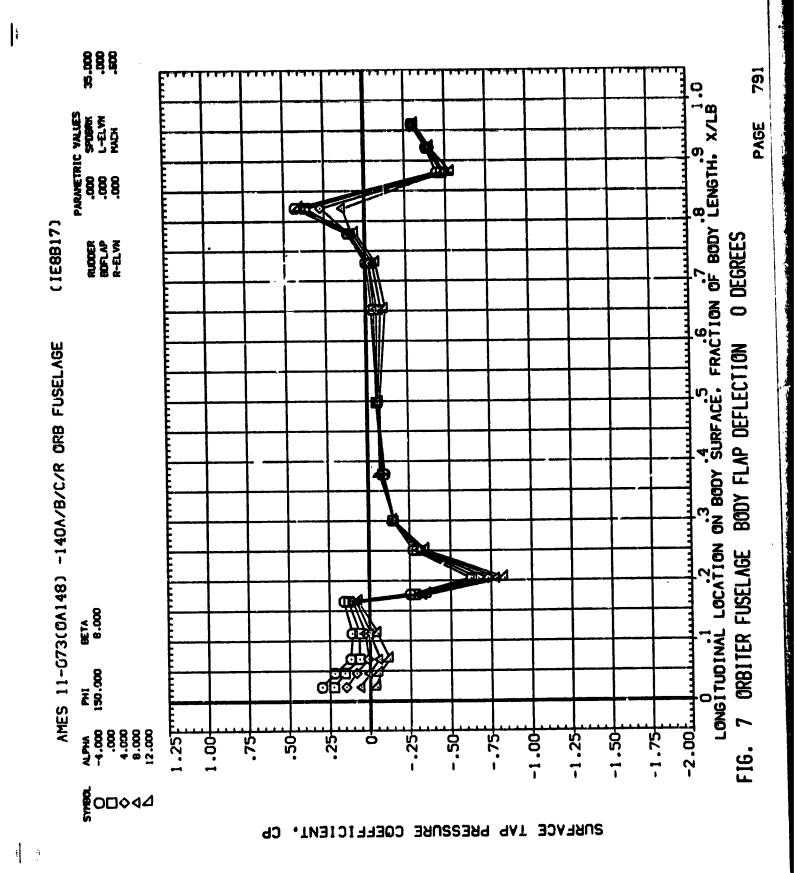
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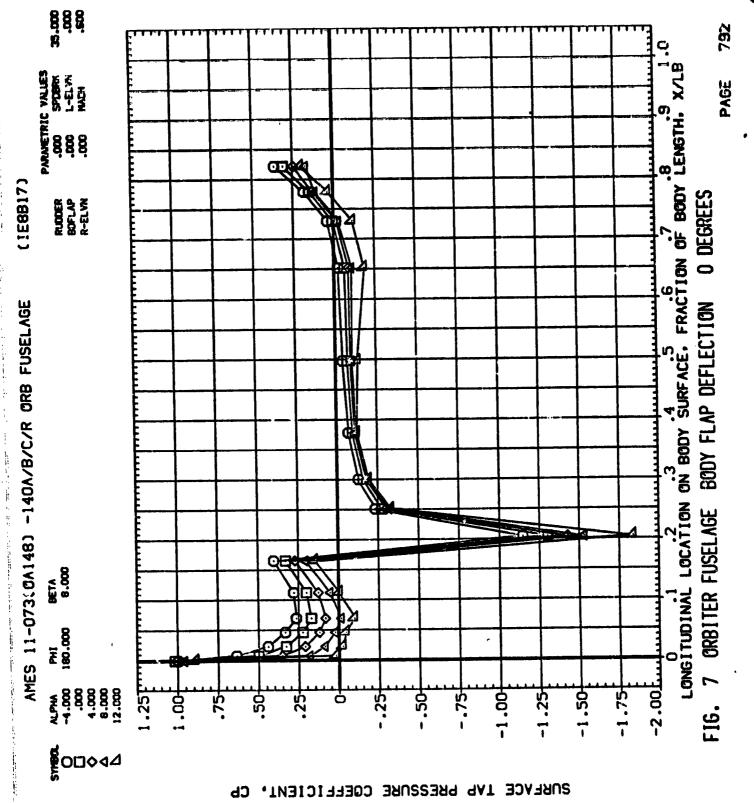
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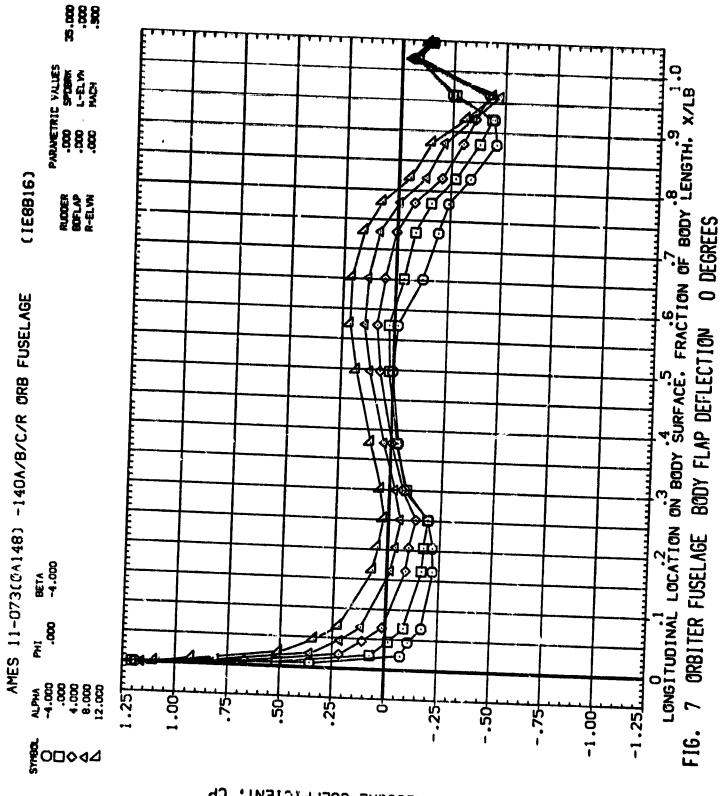


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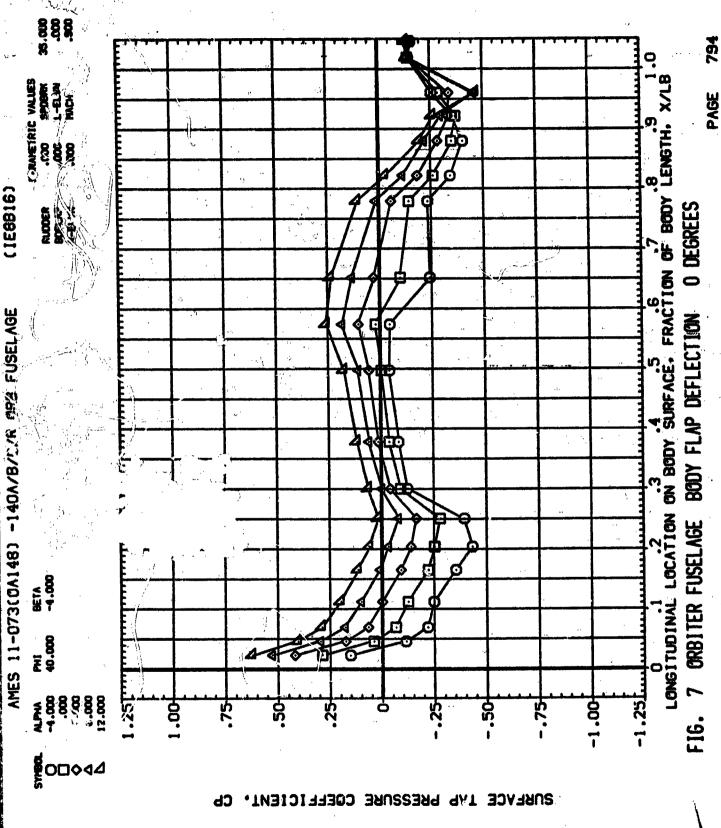


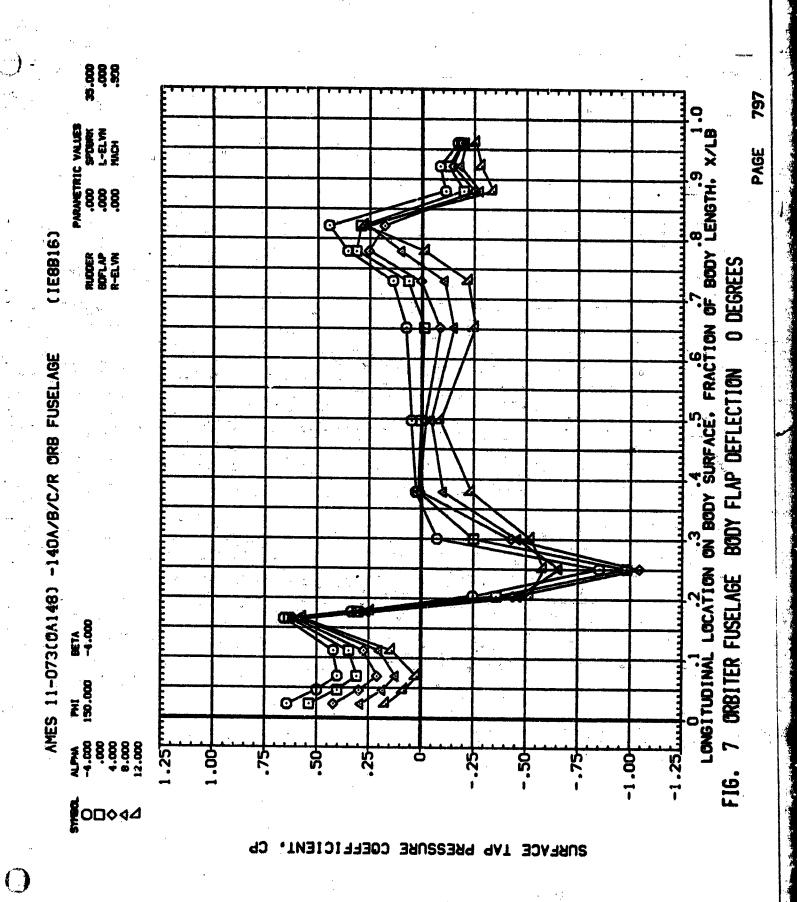


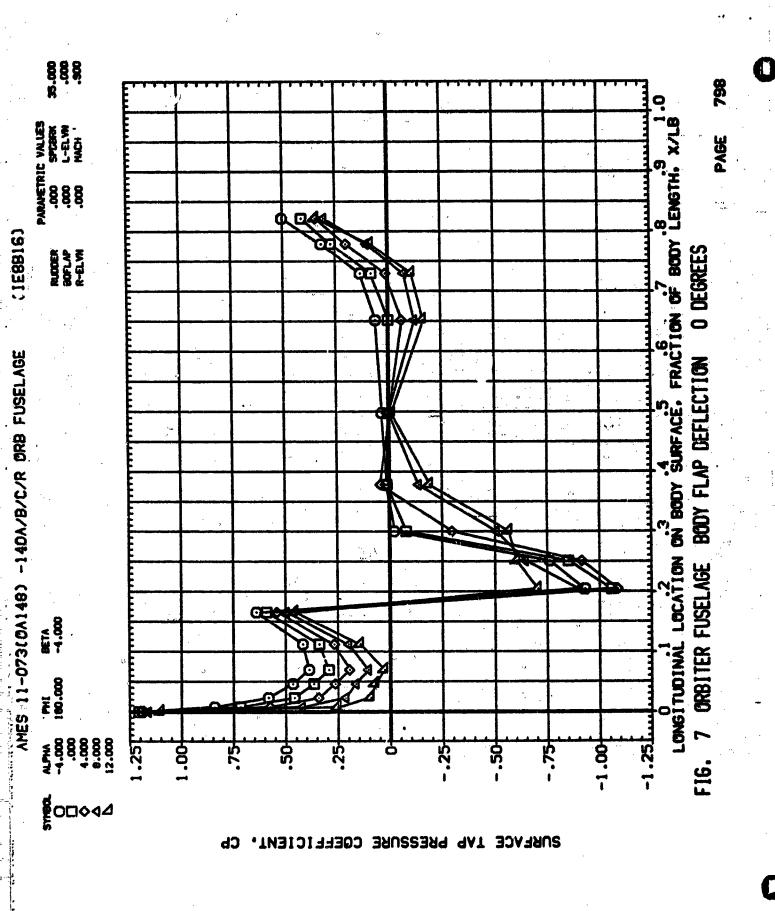
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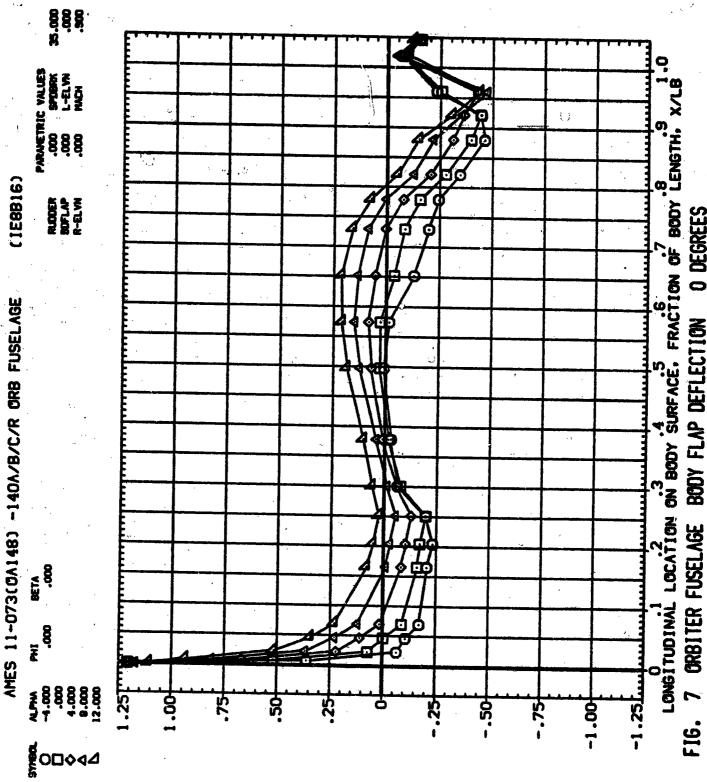


SURFACE TAP PRESSURE COEFFICIENT, CP

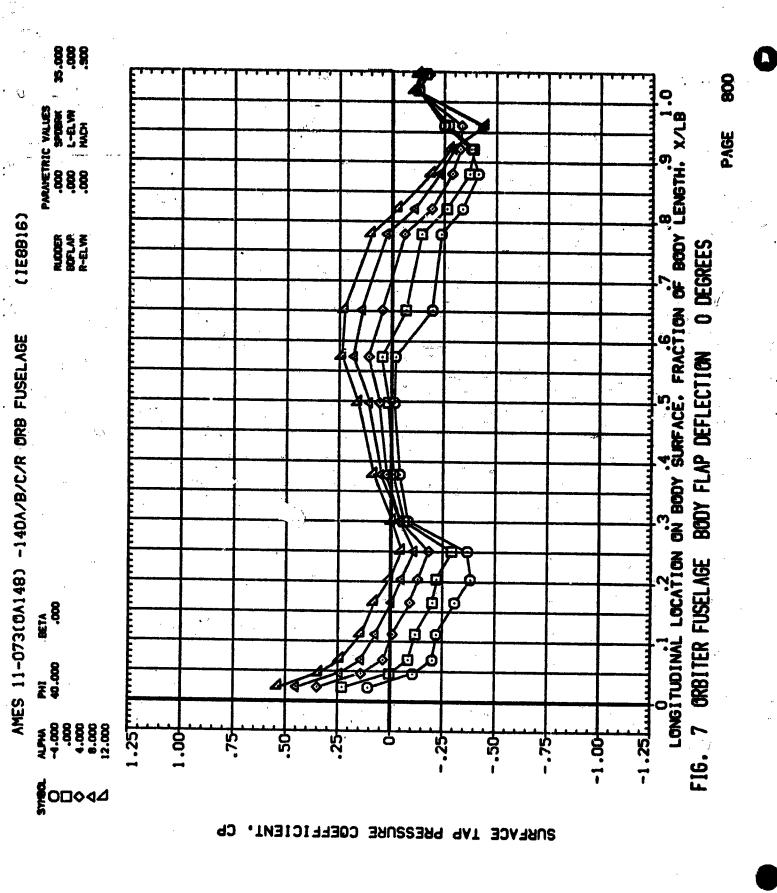


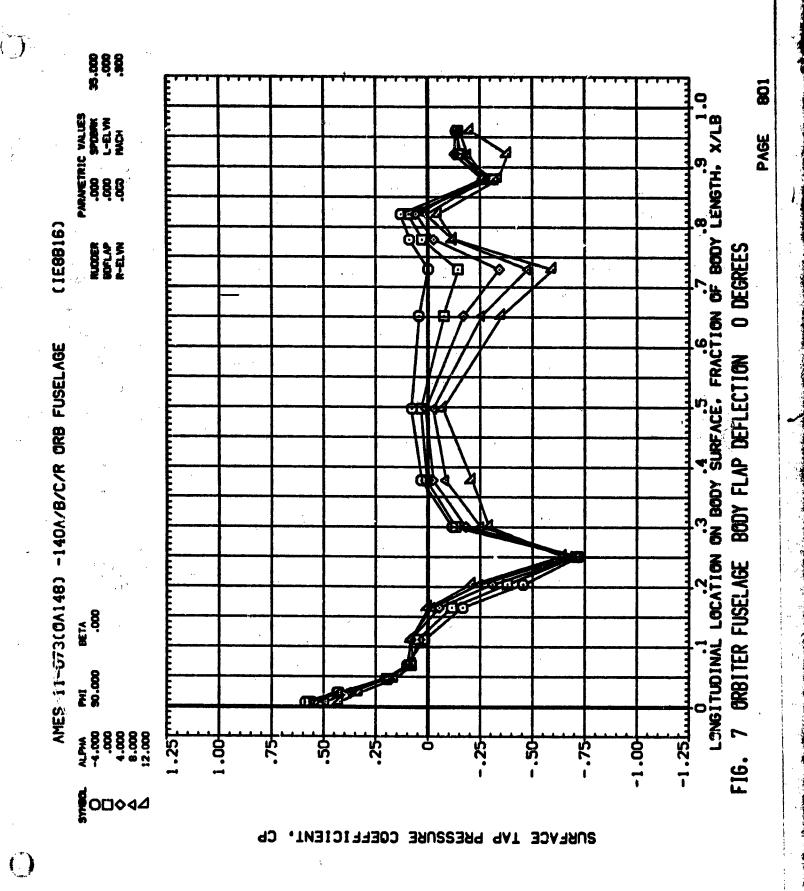


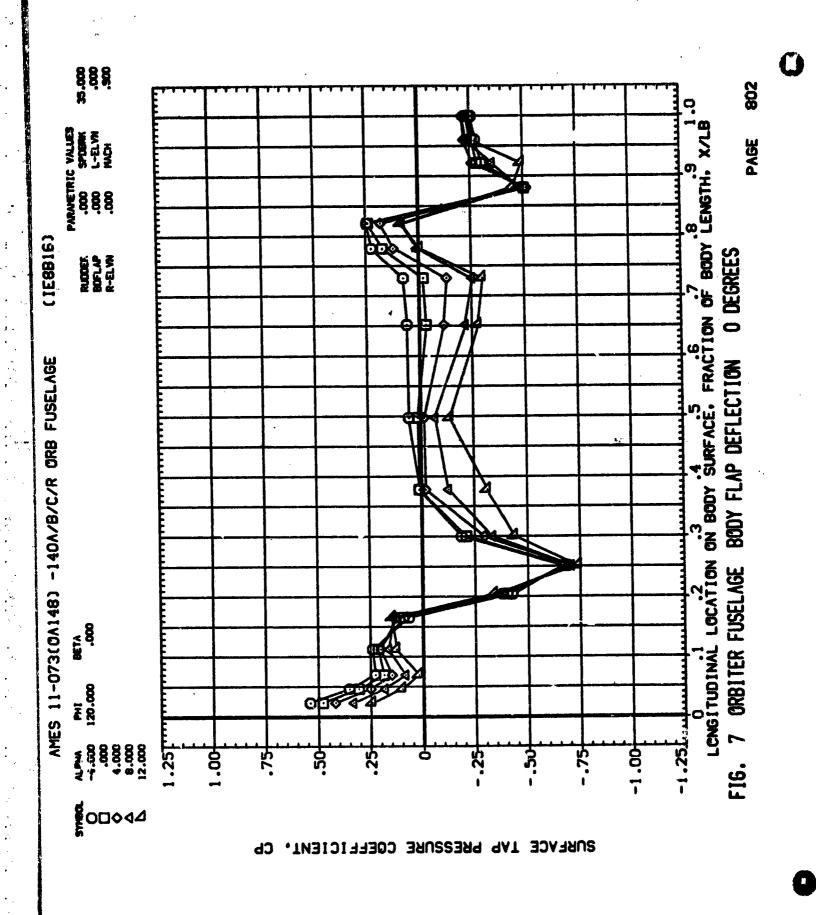




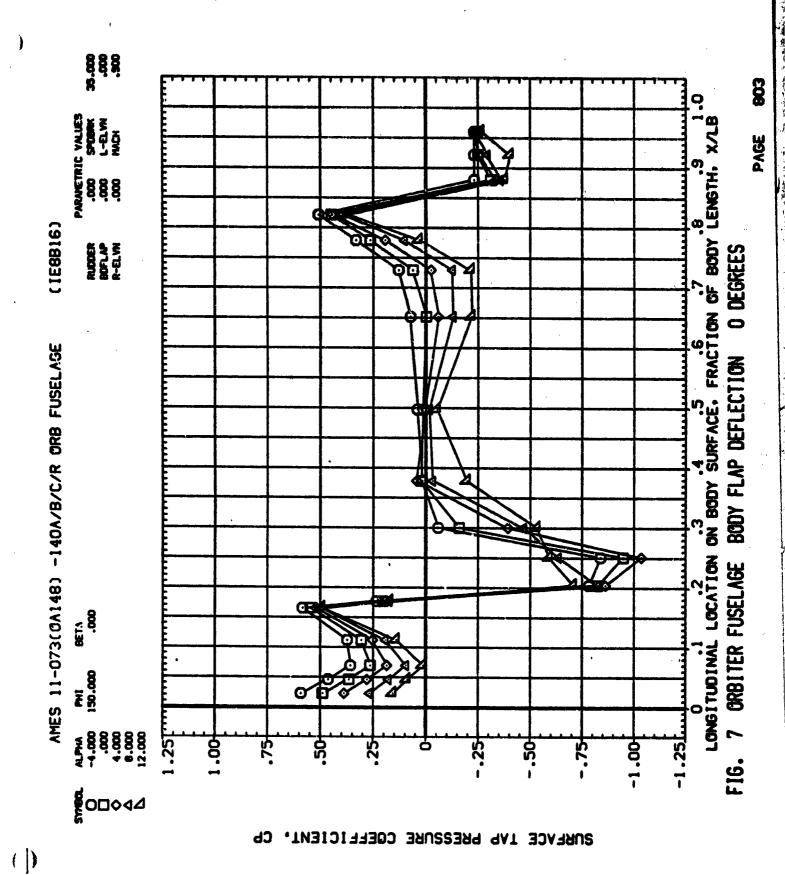
SURFACE TAP PRESSURE COEFFICIENT.

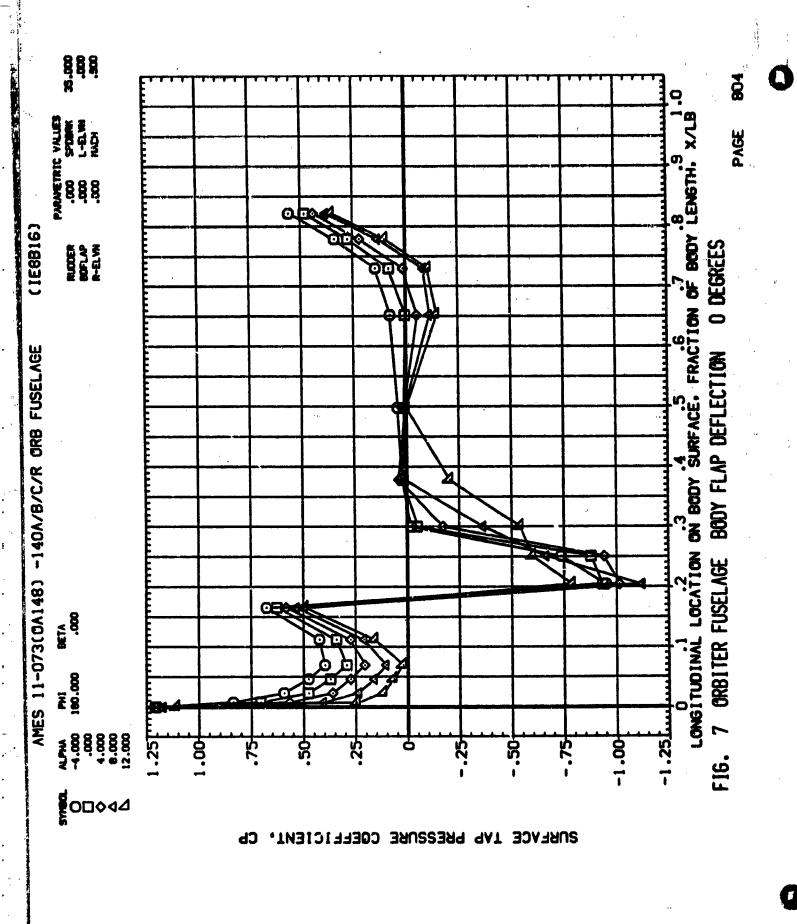






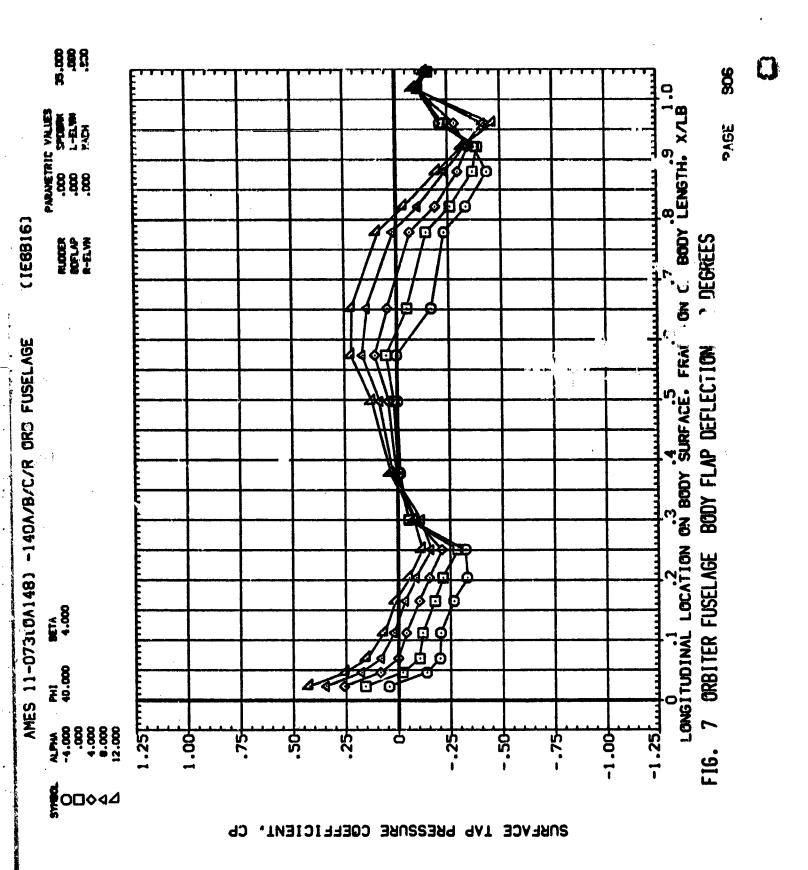
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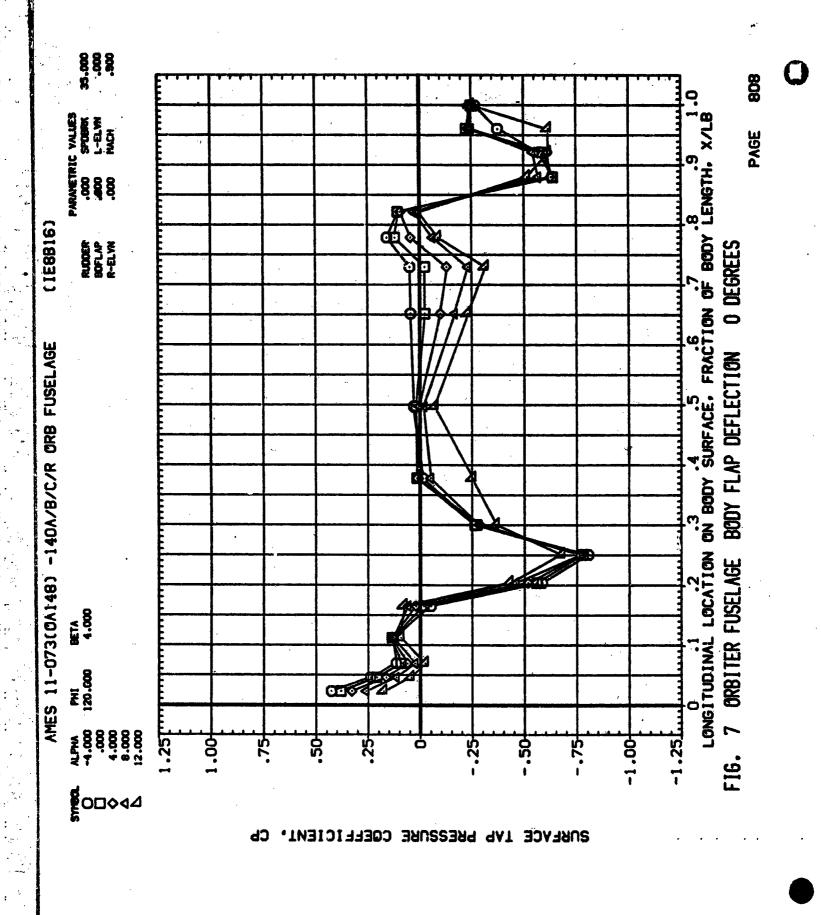


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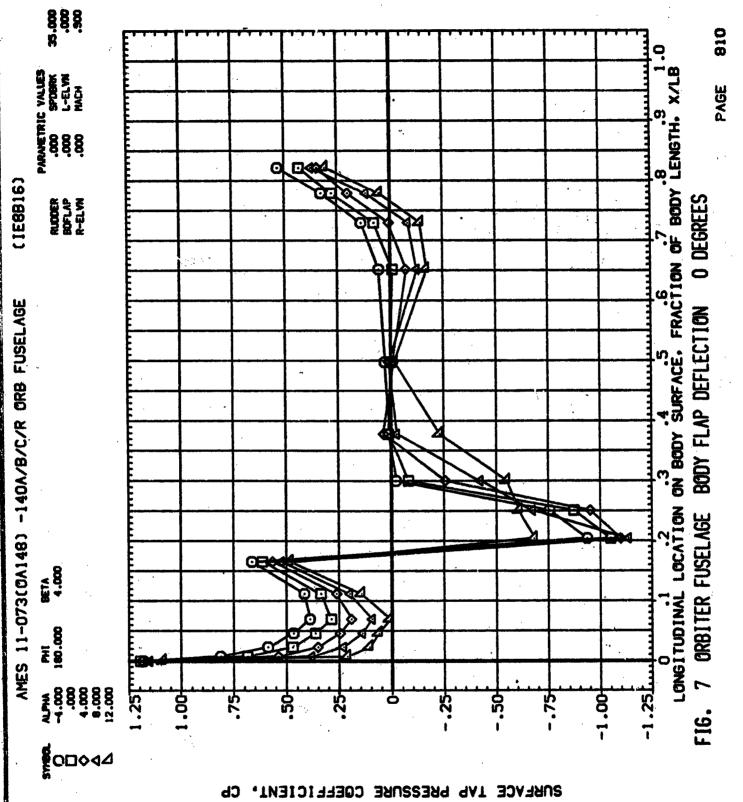
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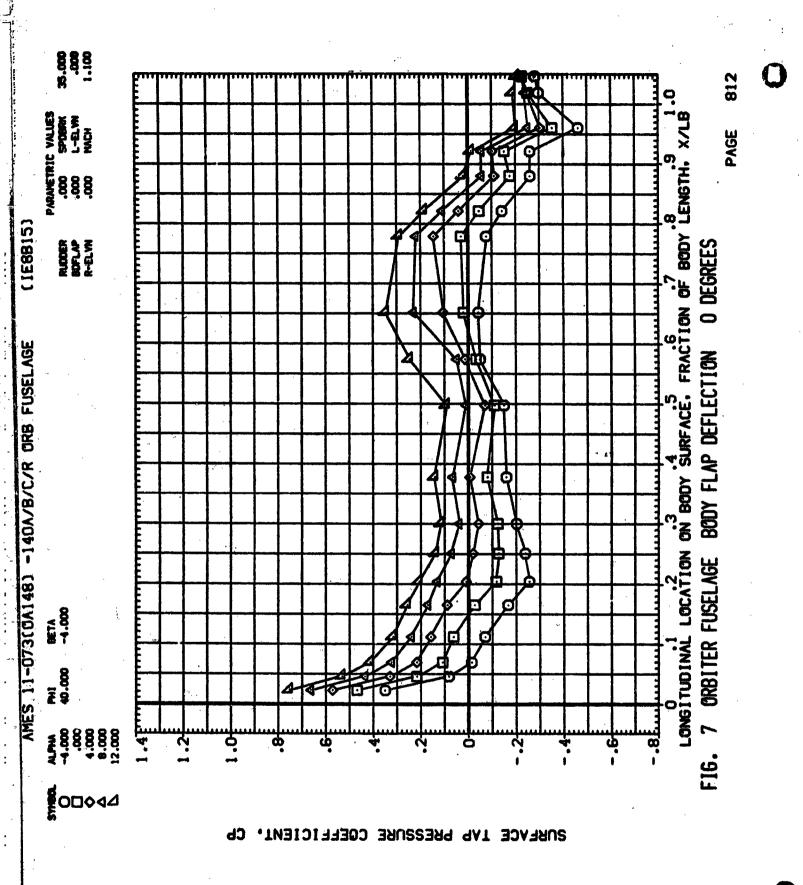


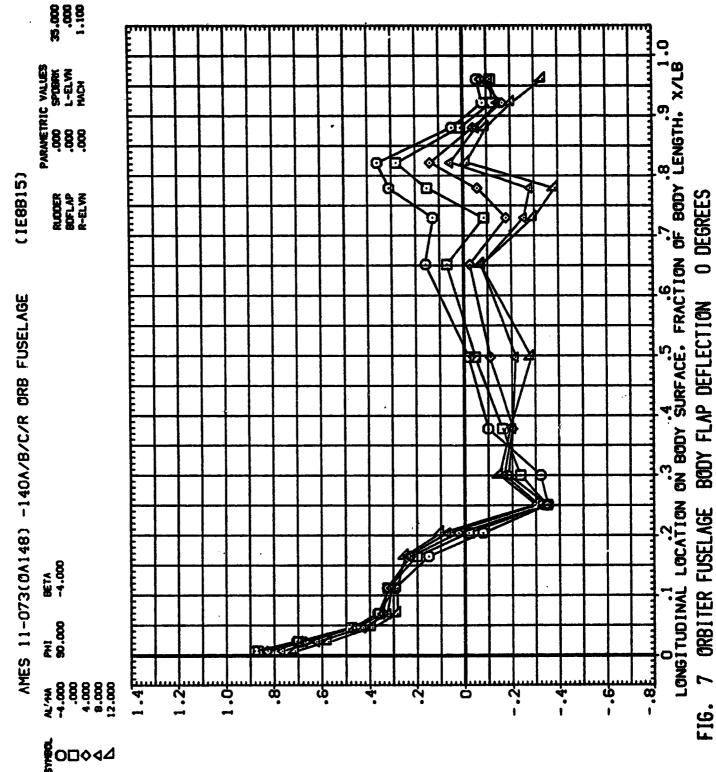
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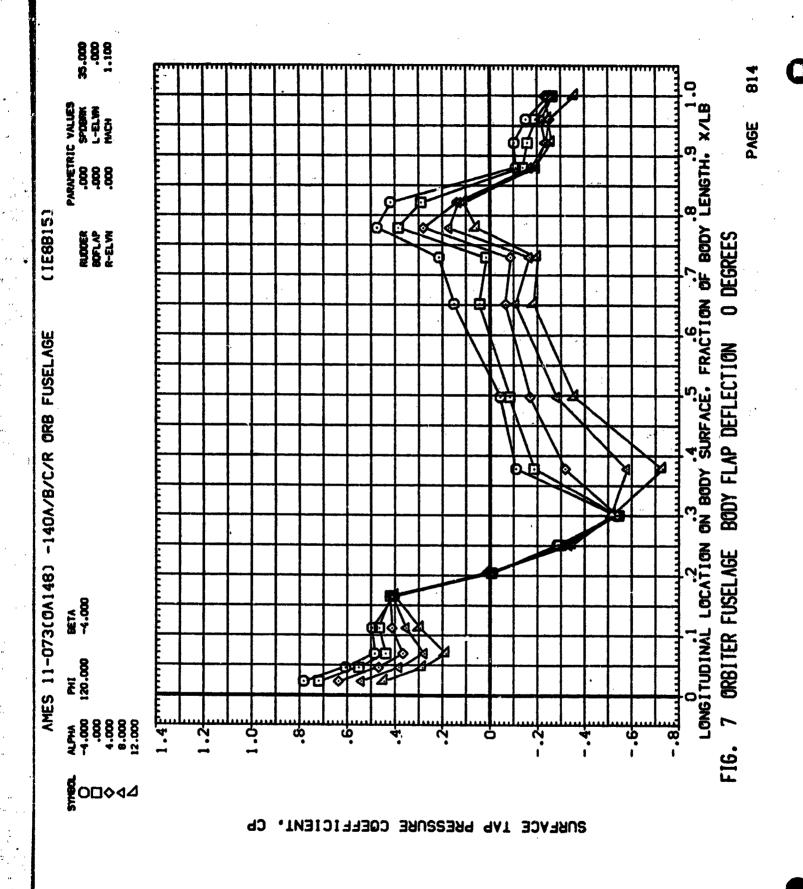




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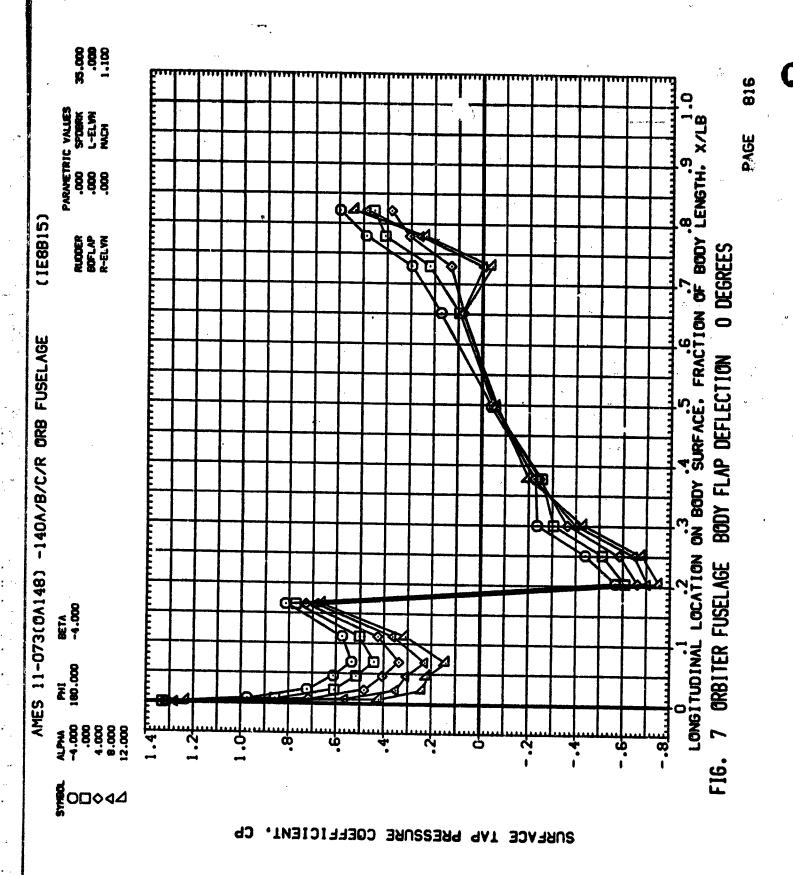
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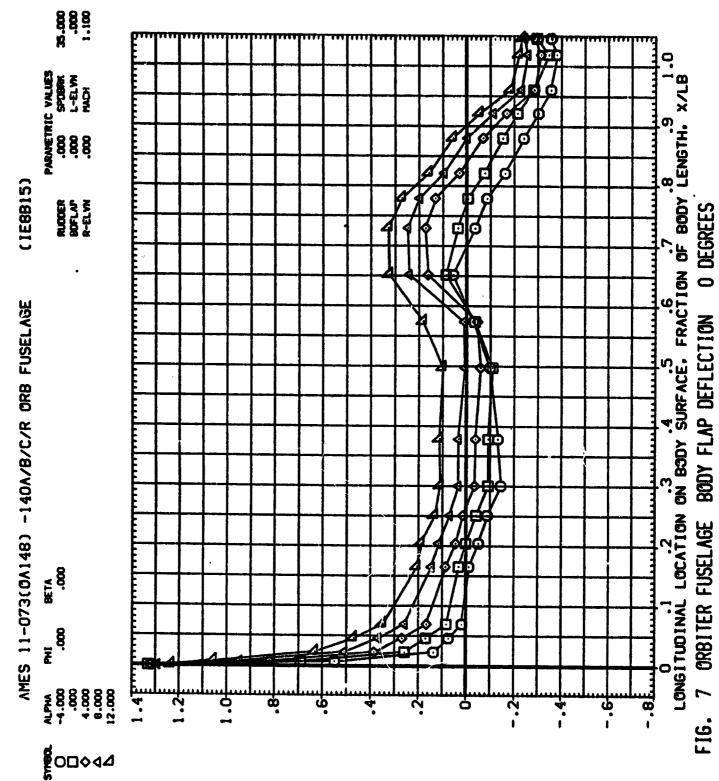
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SURFACE TAP PRESSURE COEFFICIENT, CR

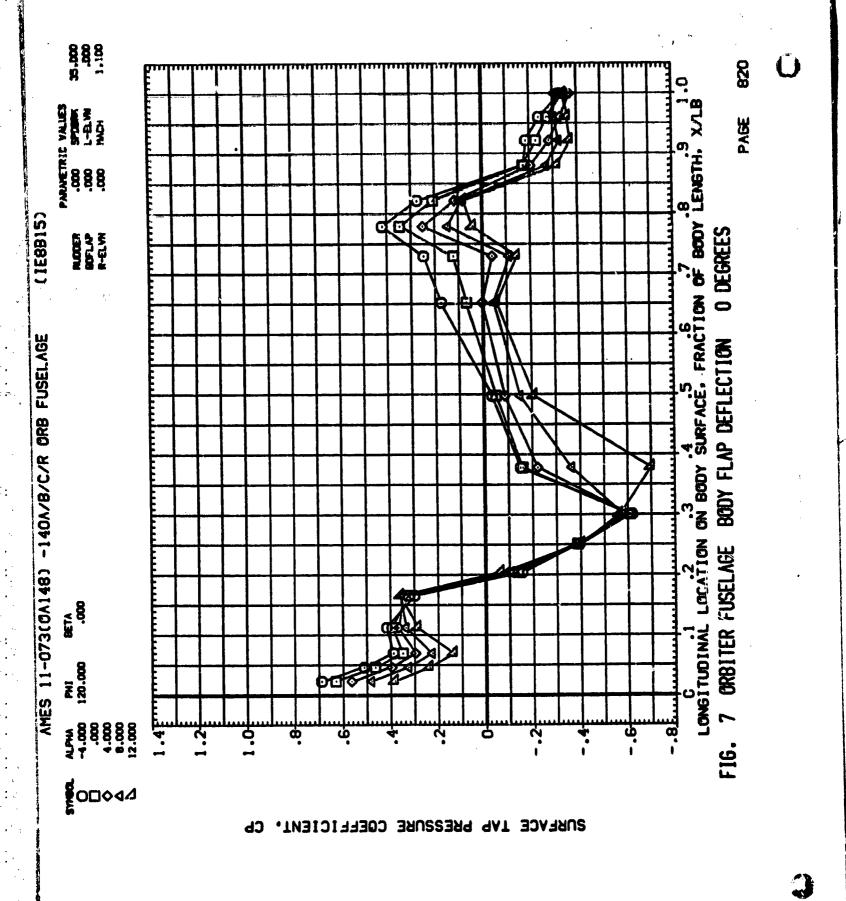


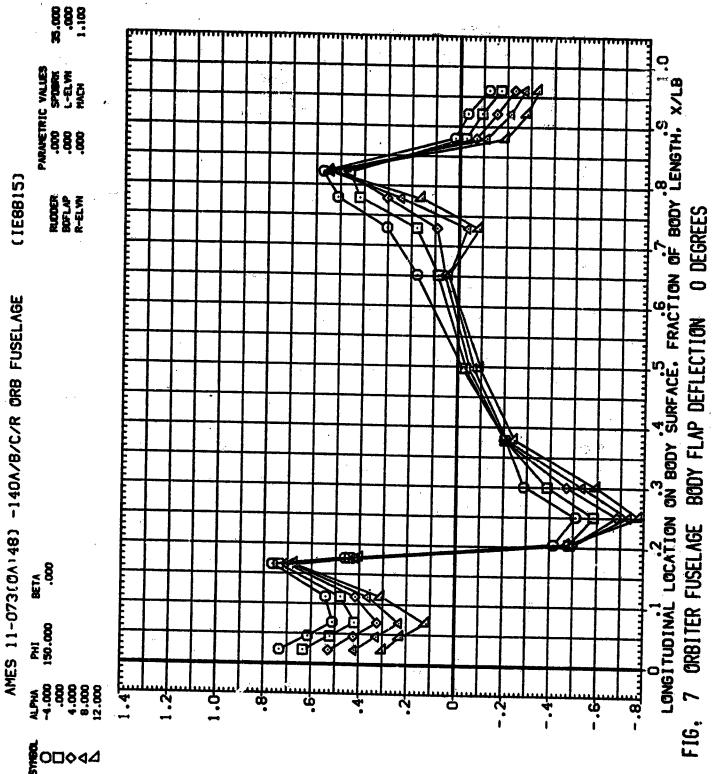


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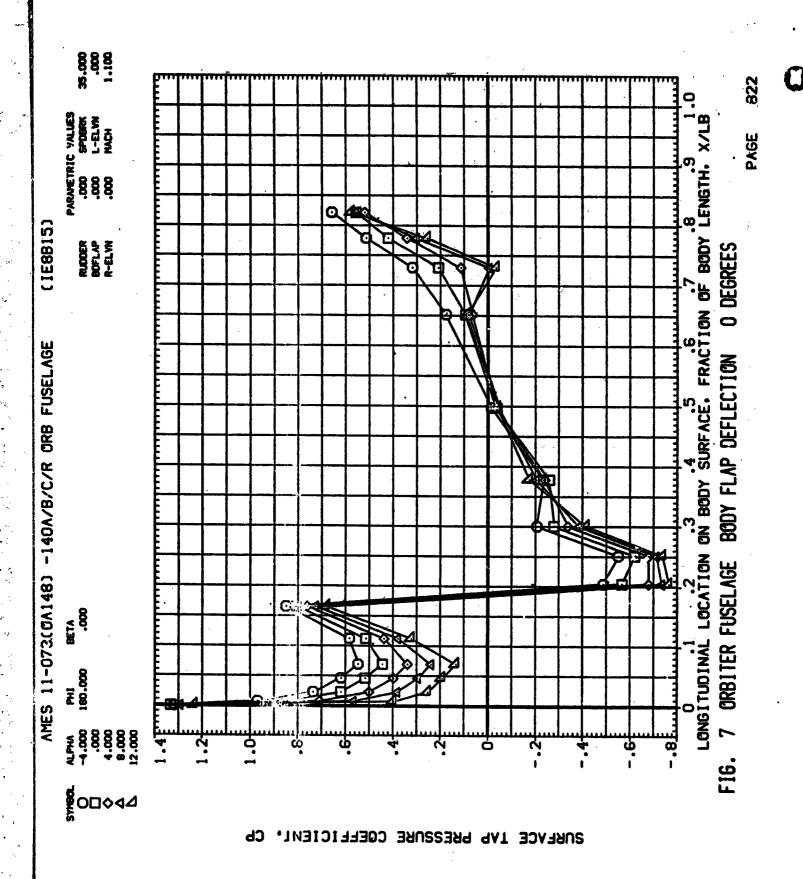
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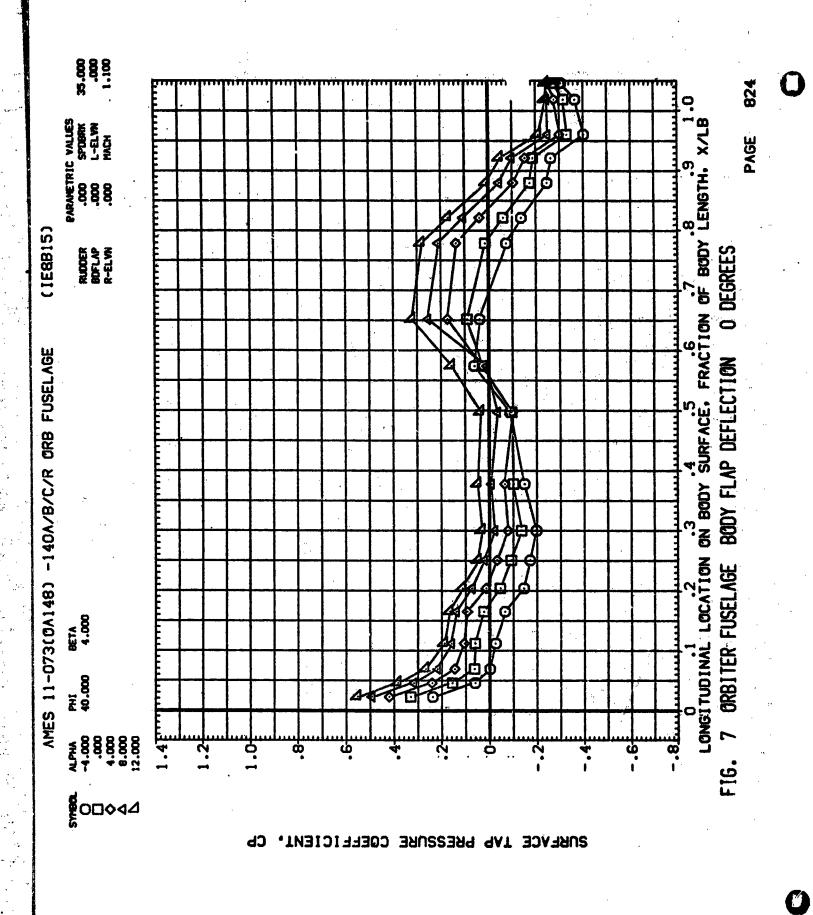


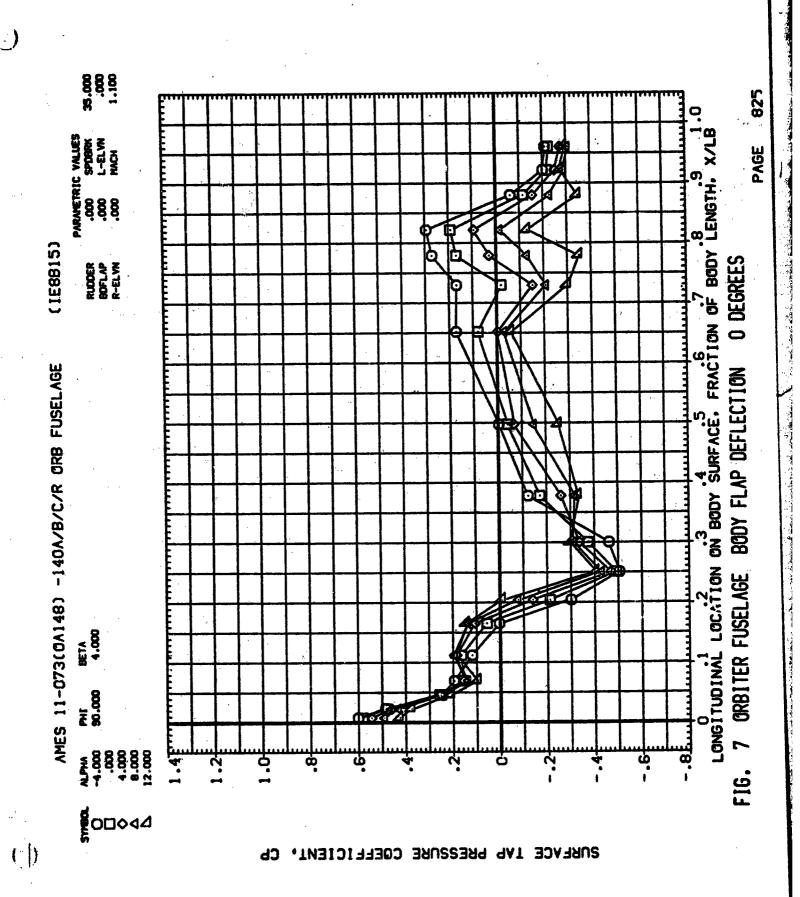
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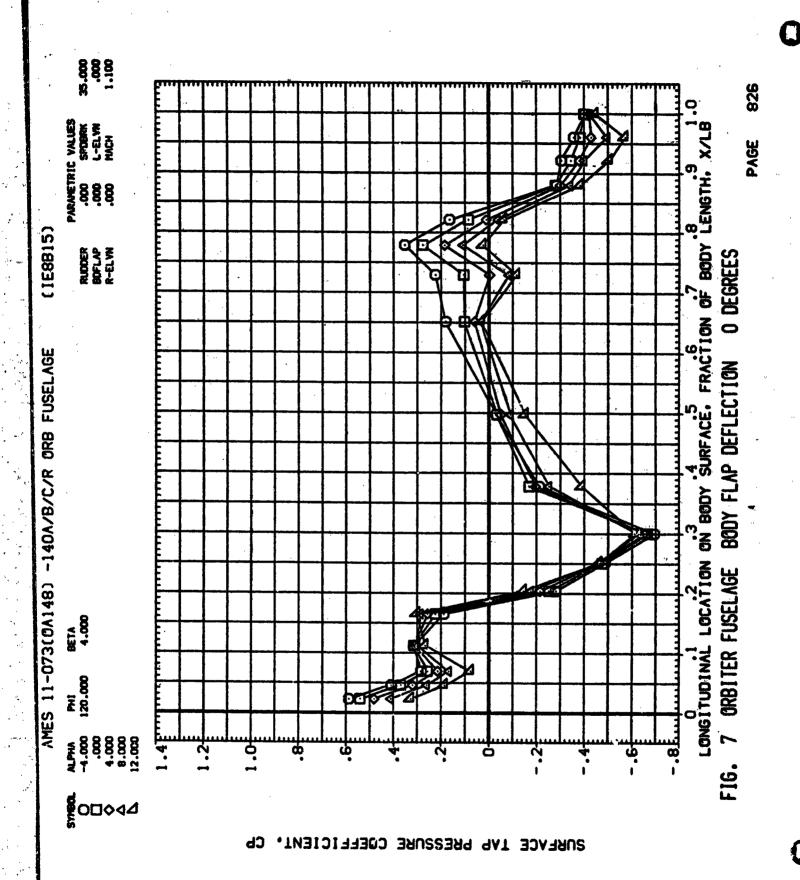
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SURFACE TAP PRESSURE COEFFICIENT,







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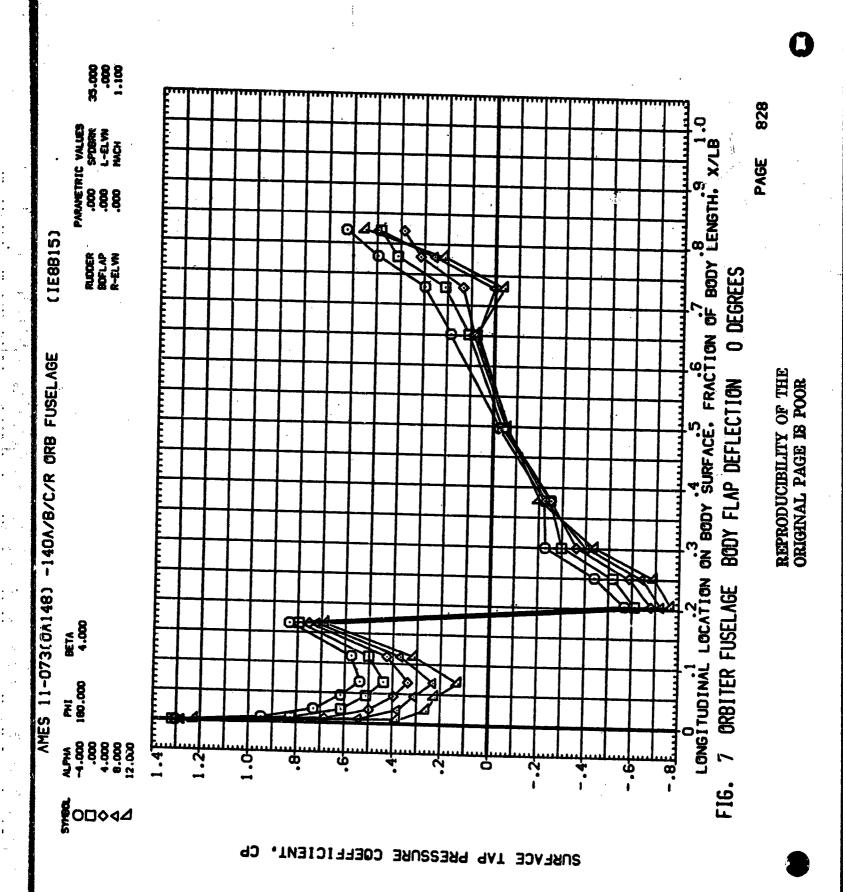
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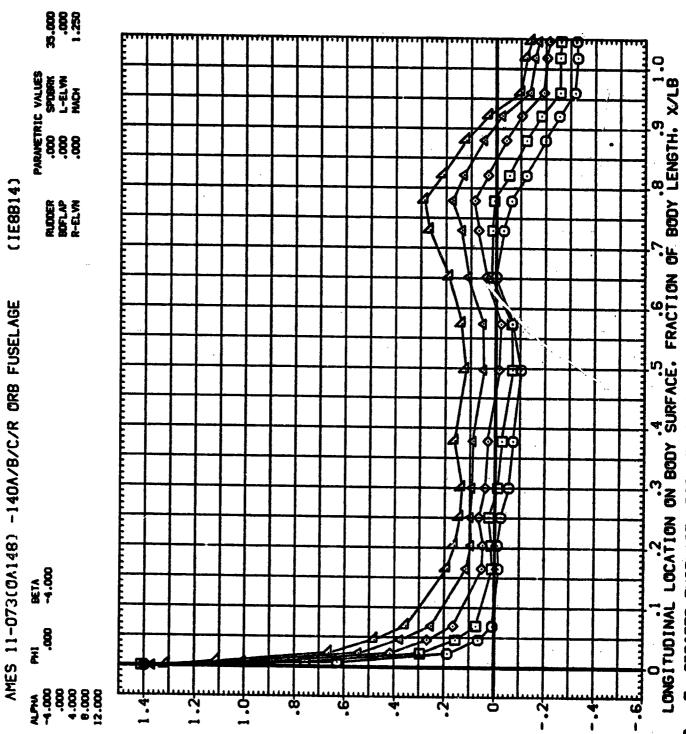
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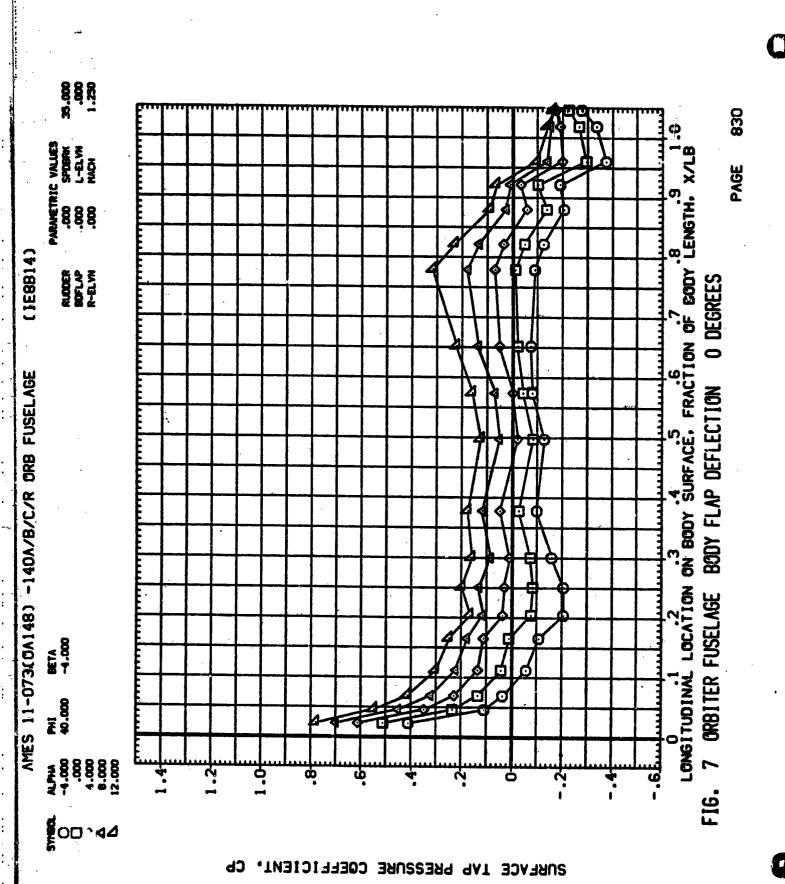


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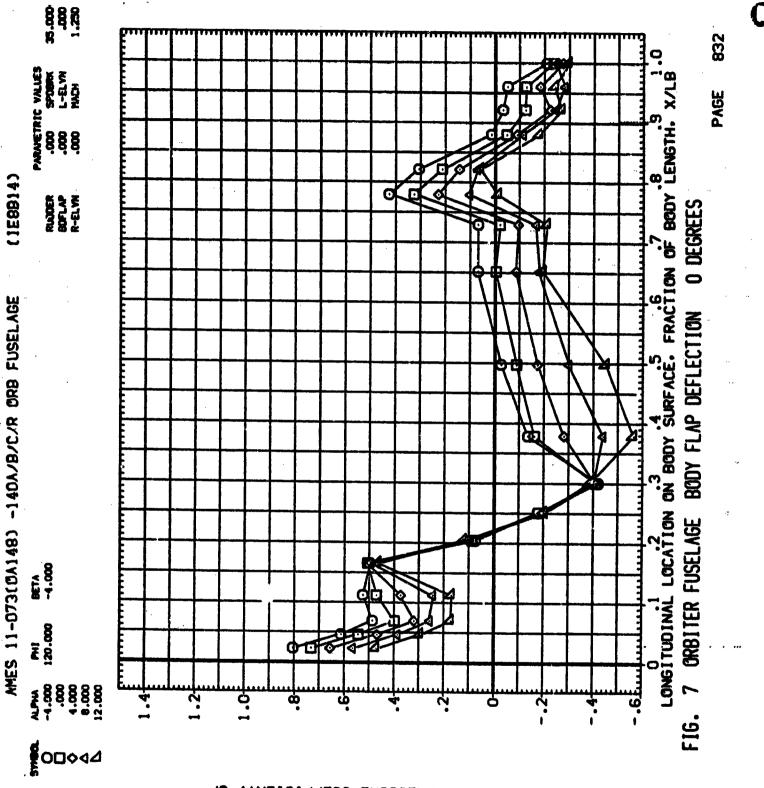
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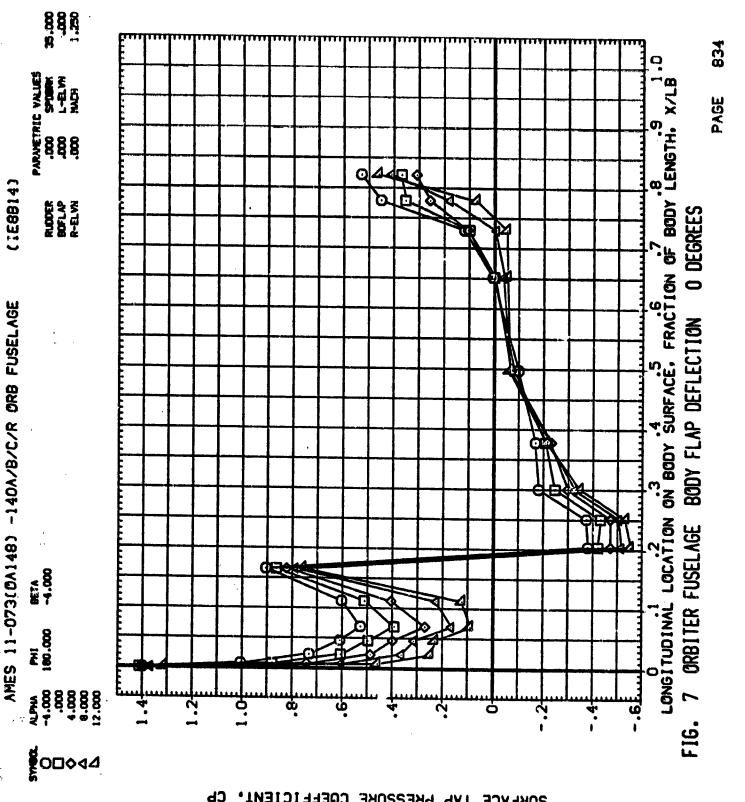
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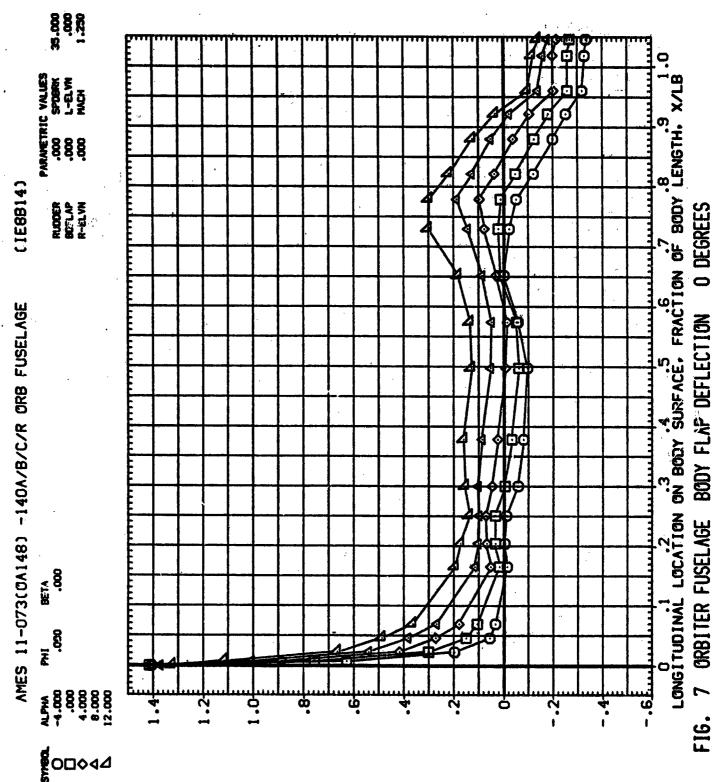
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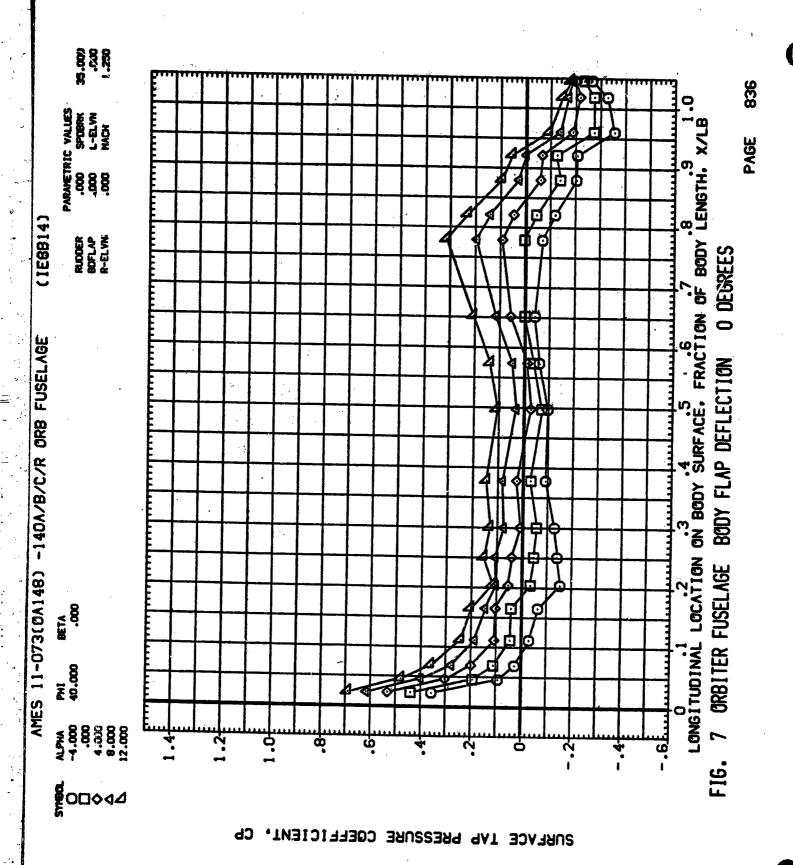
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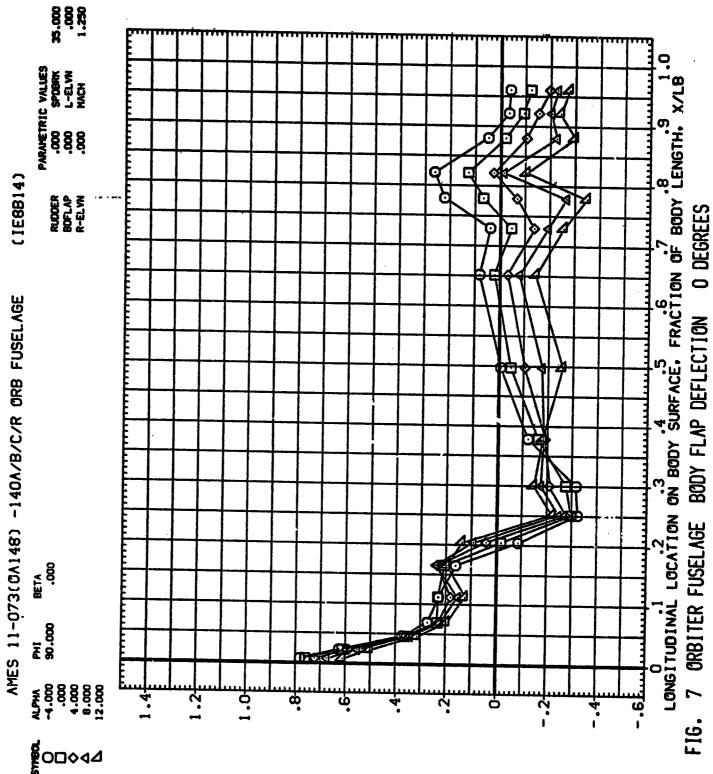


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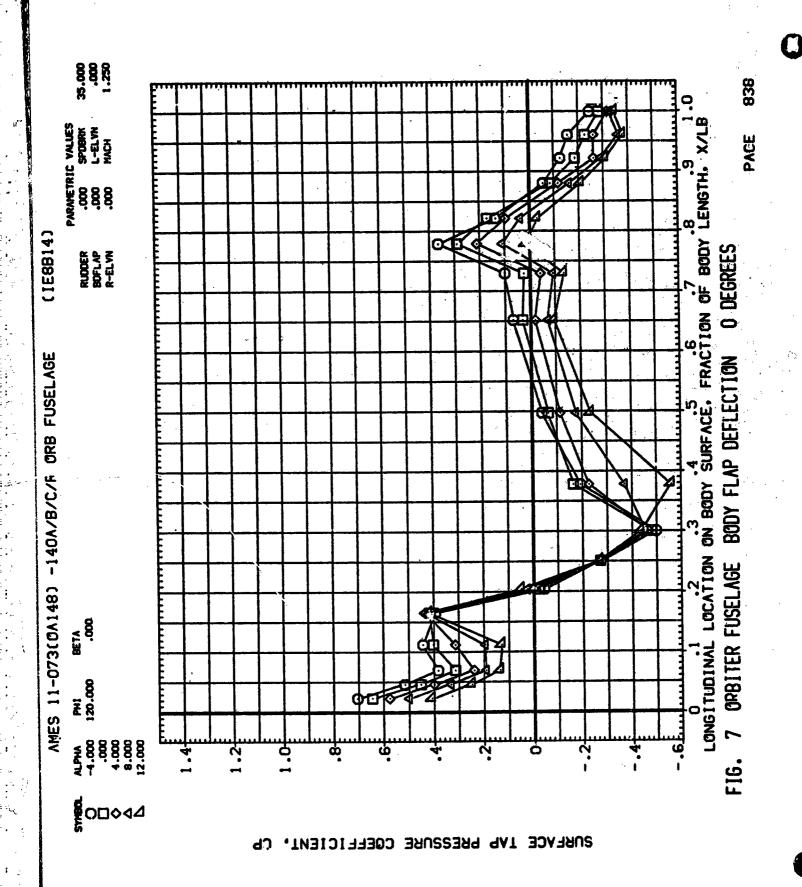


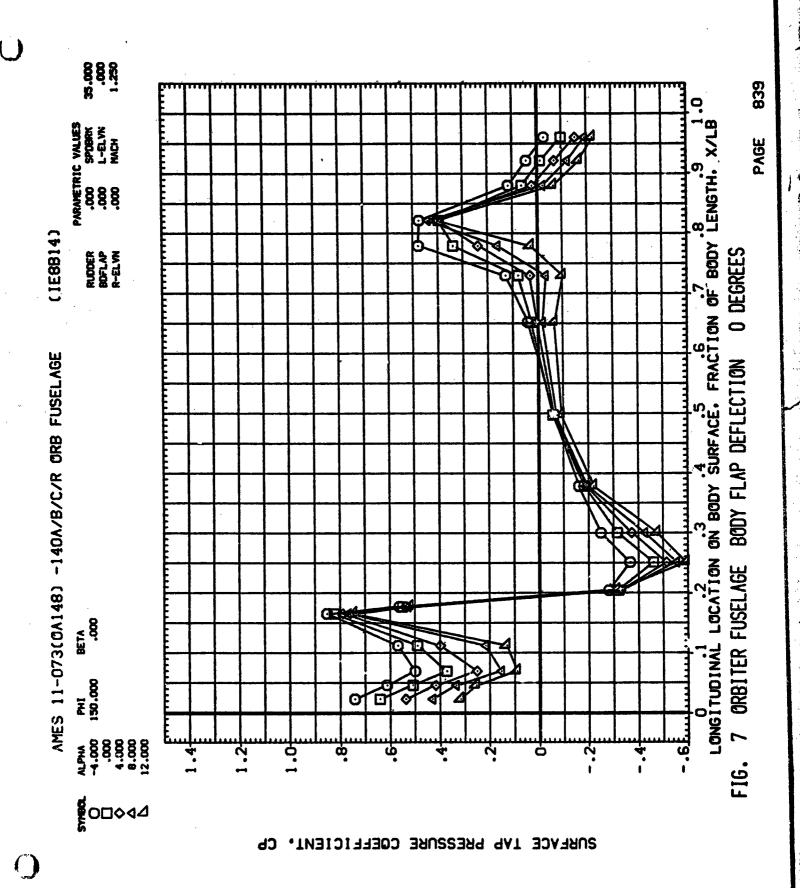
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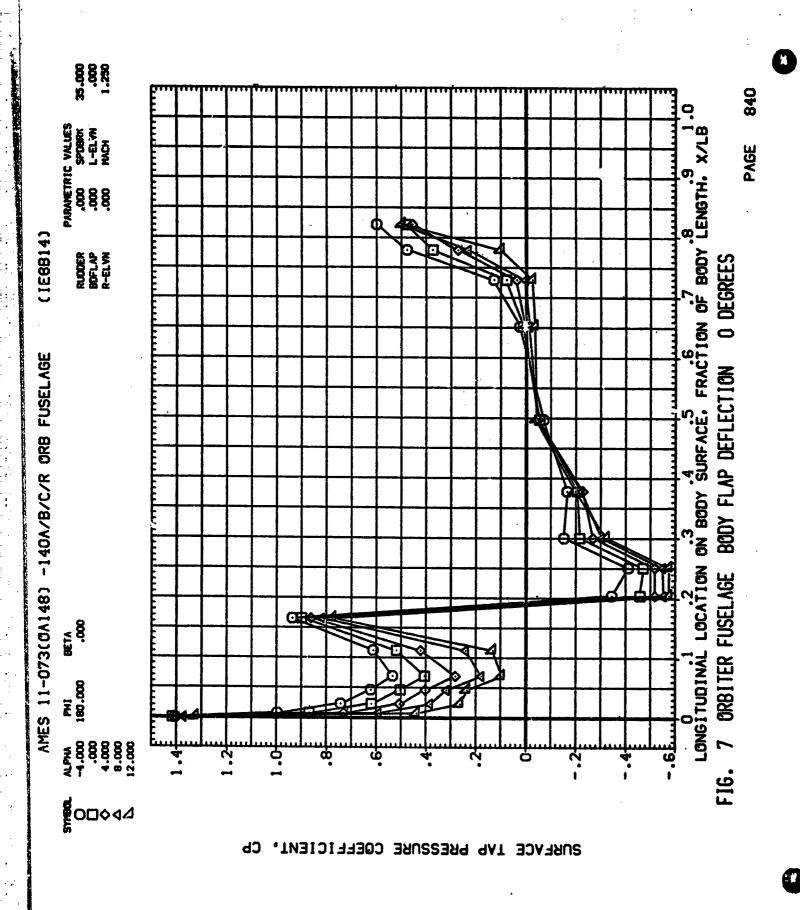


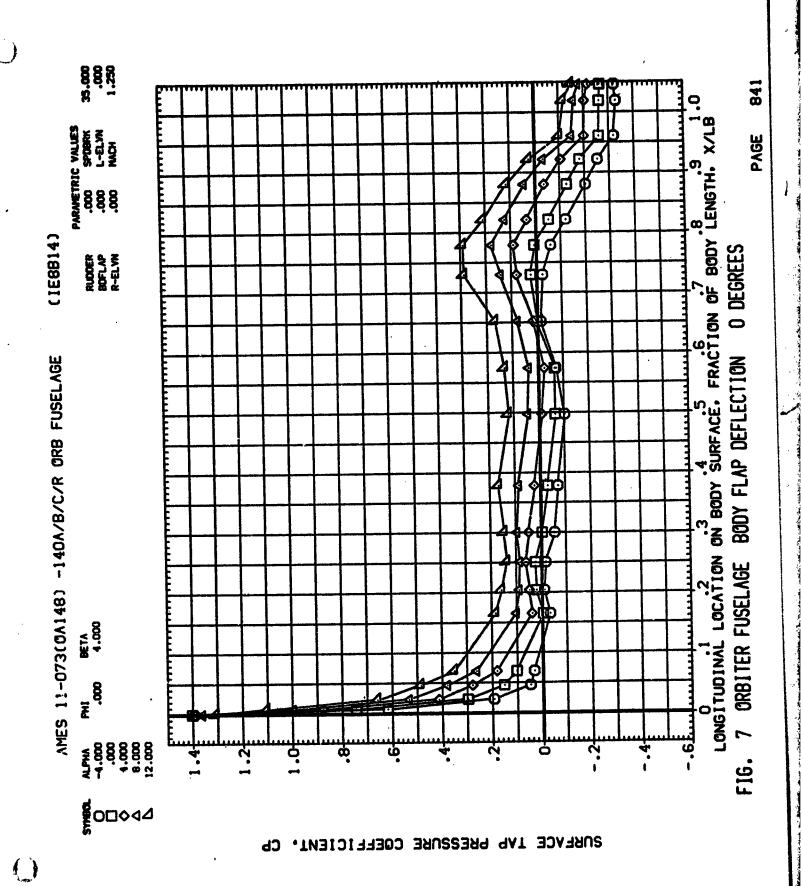


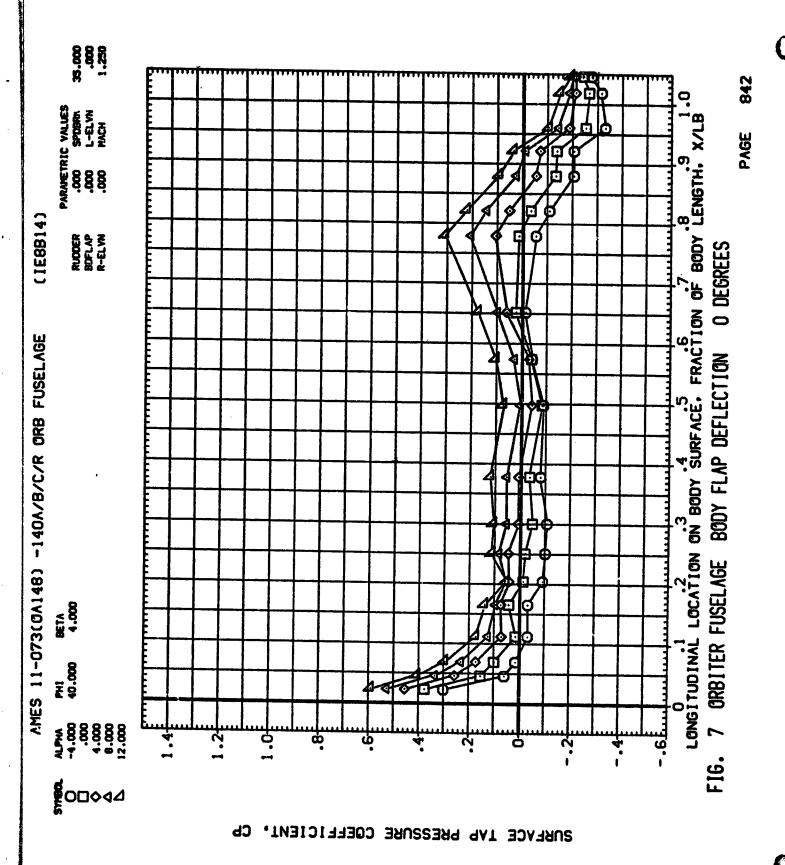
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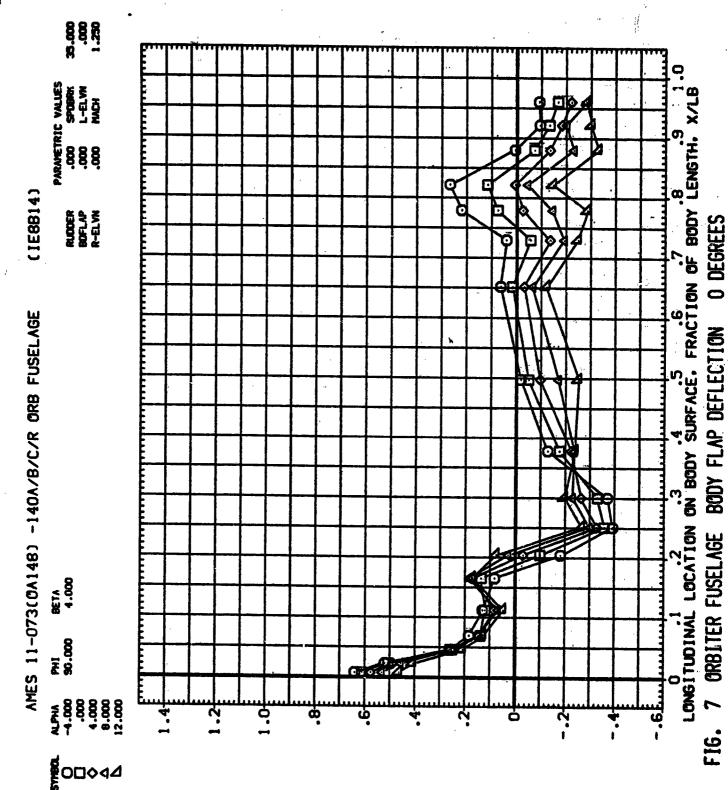




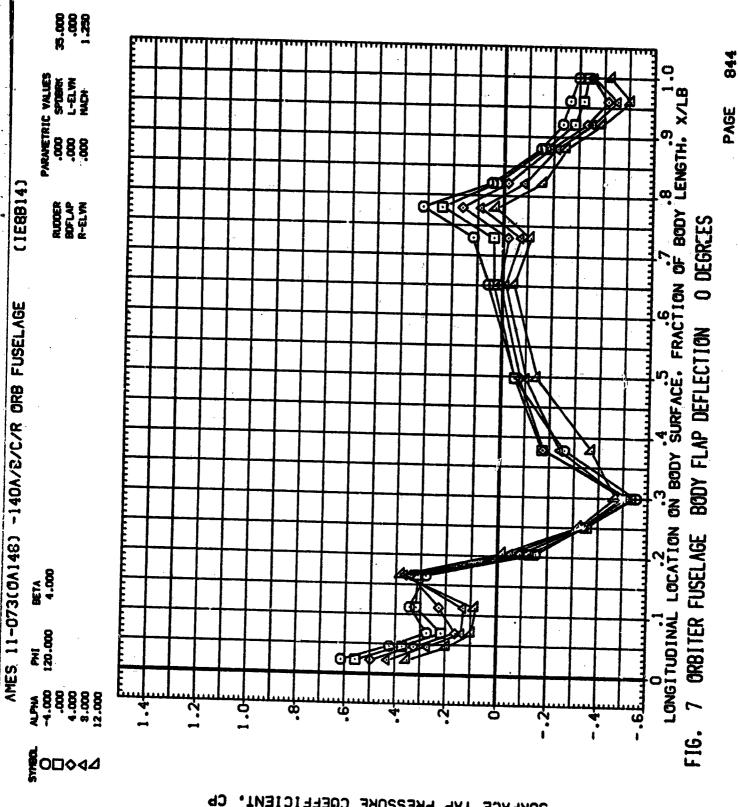




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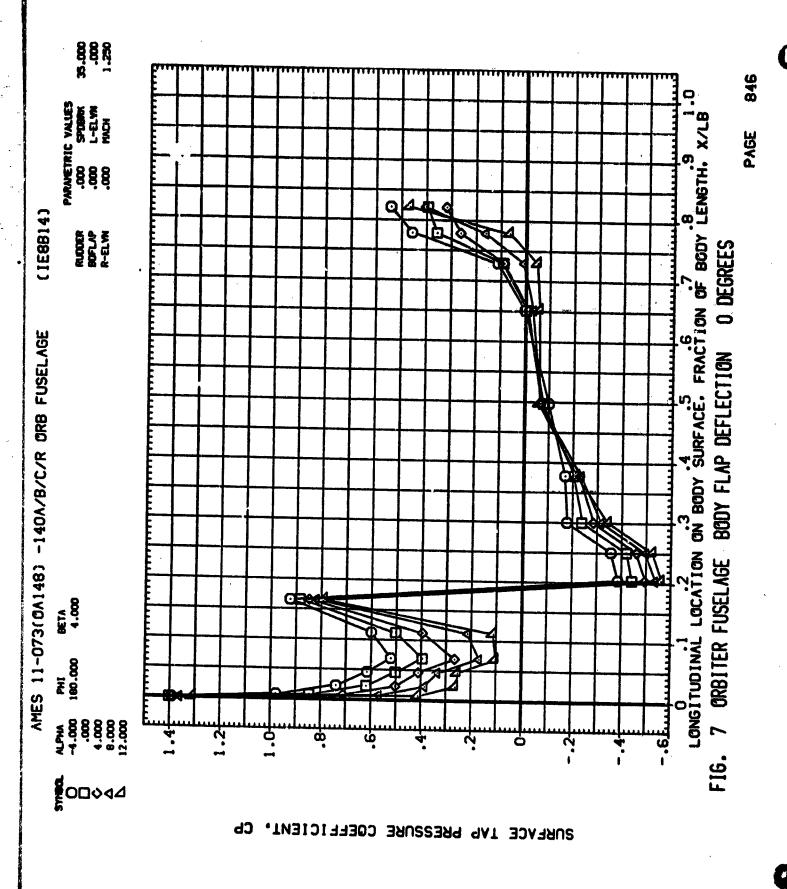


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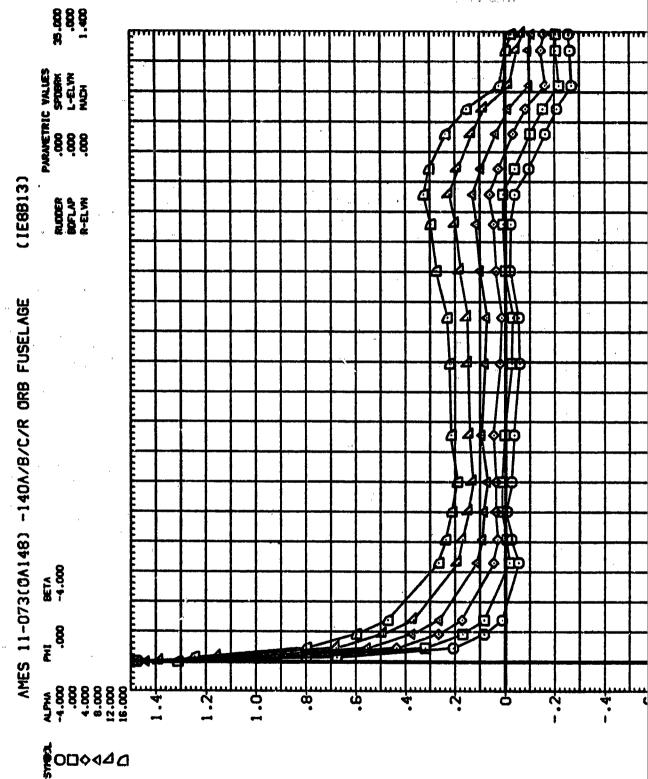


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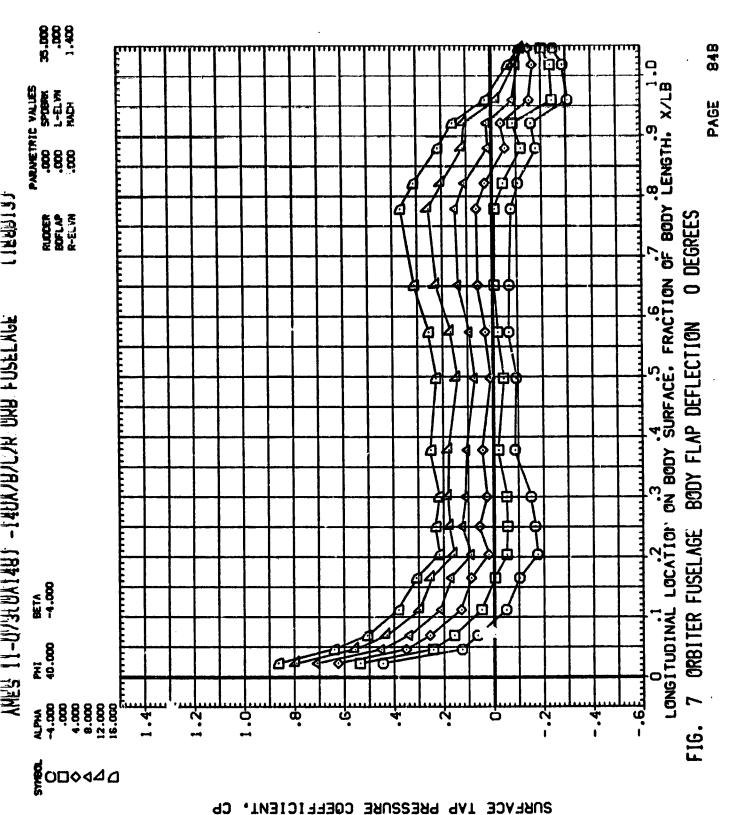
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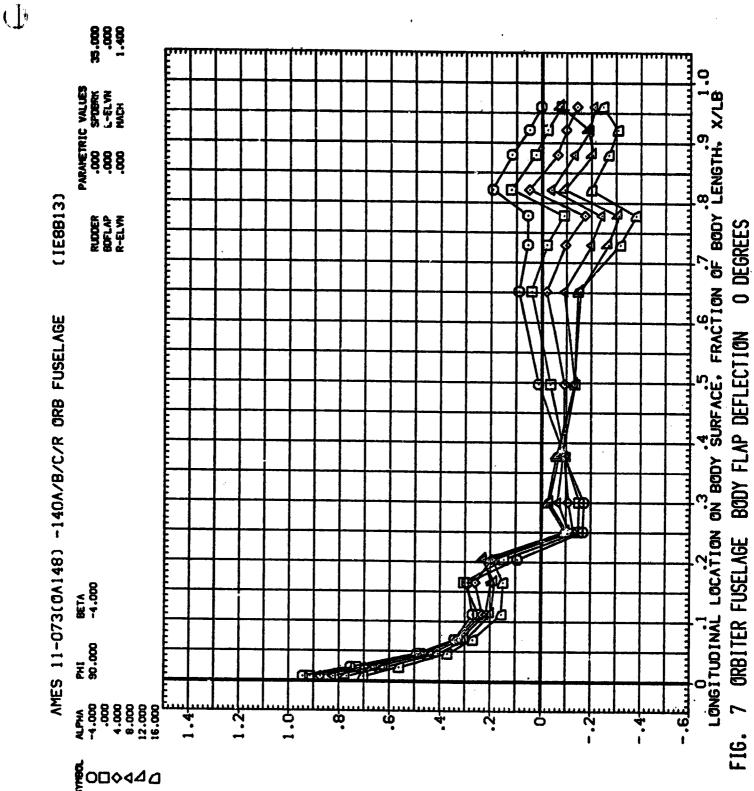


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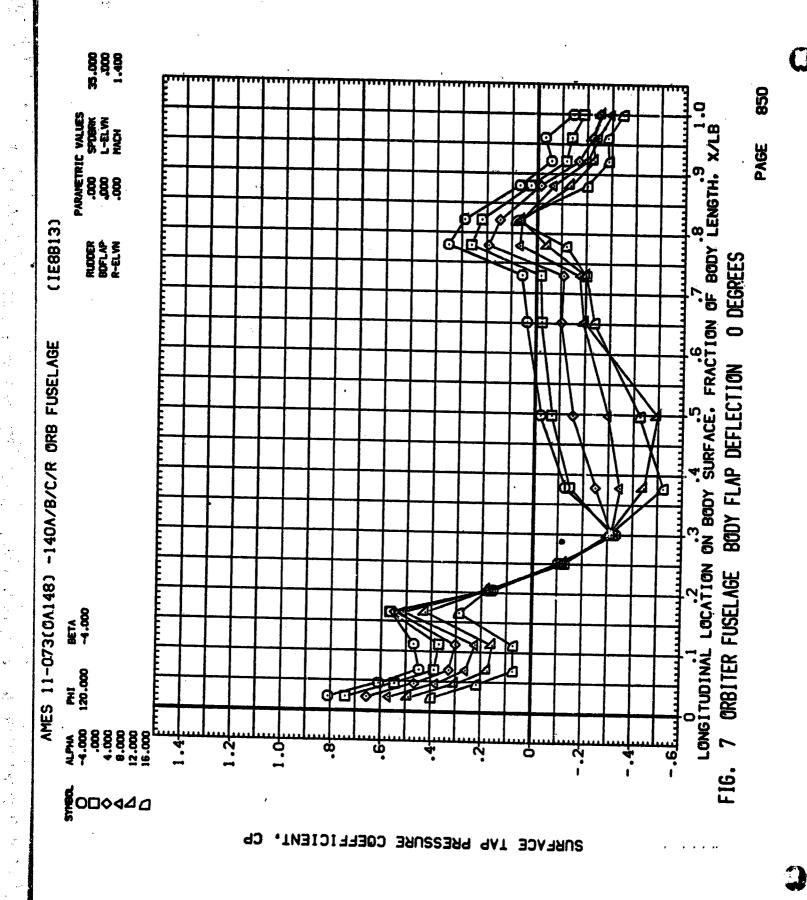


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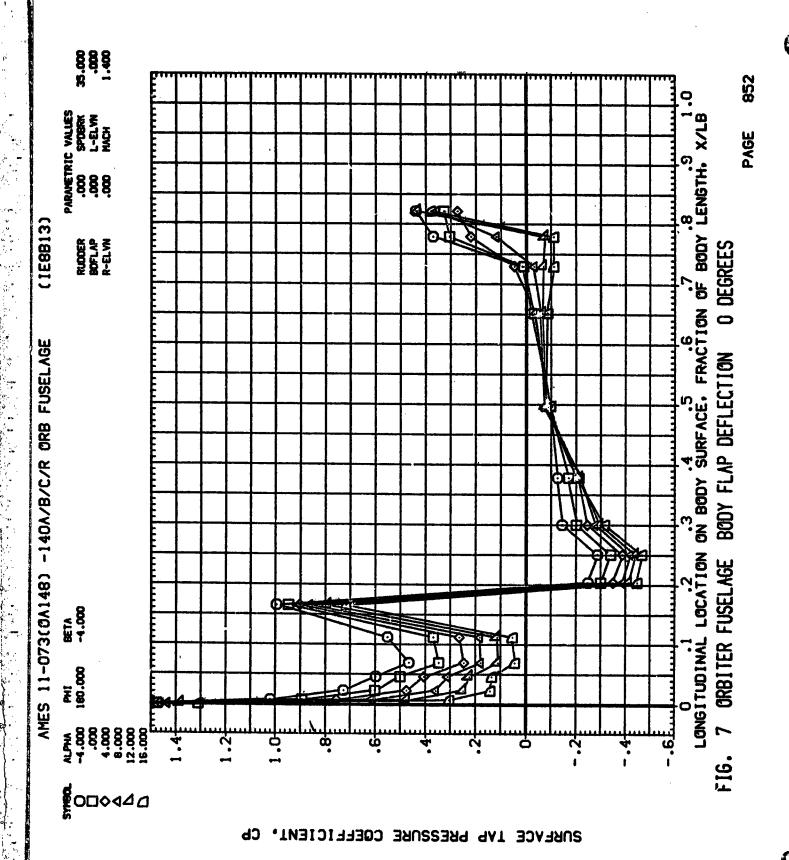
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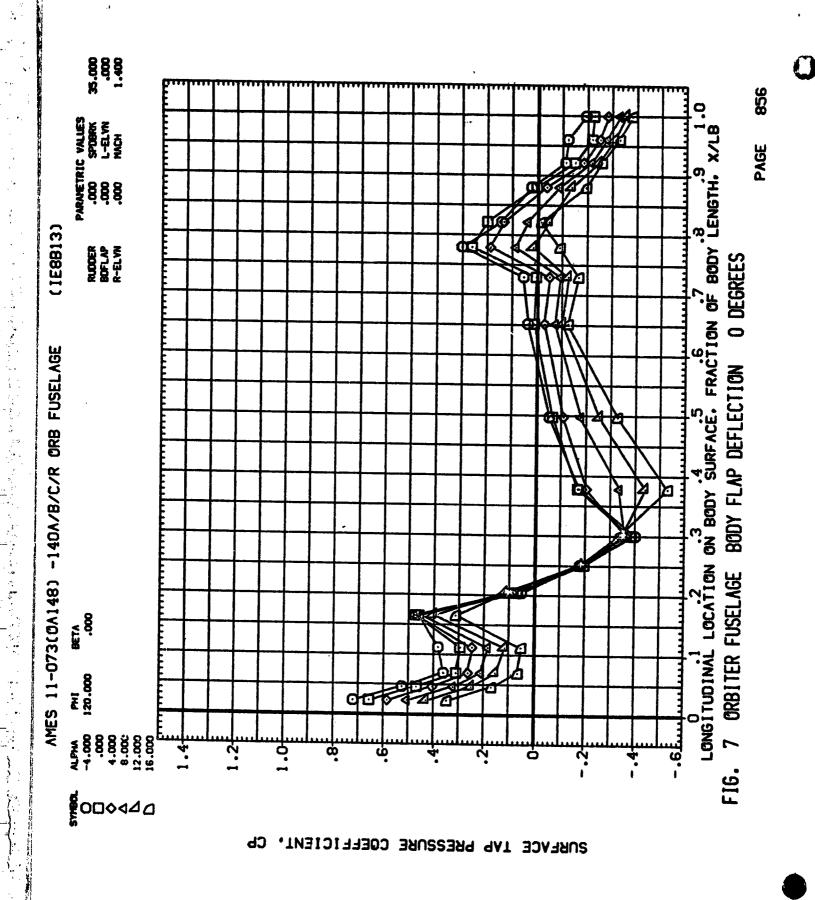
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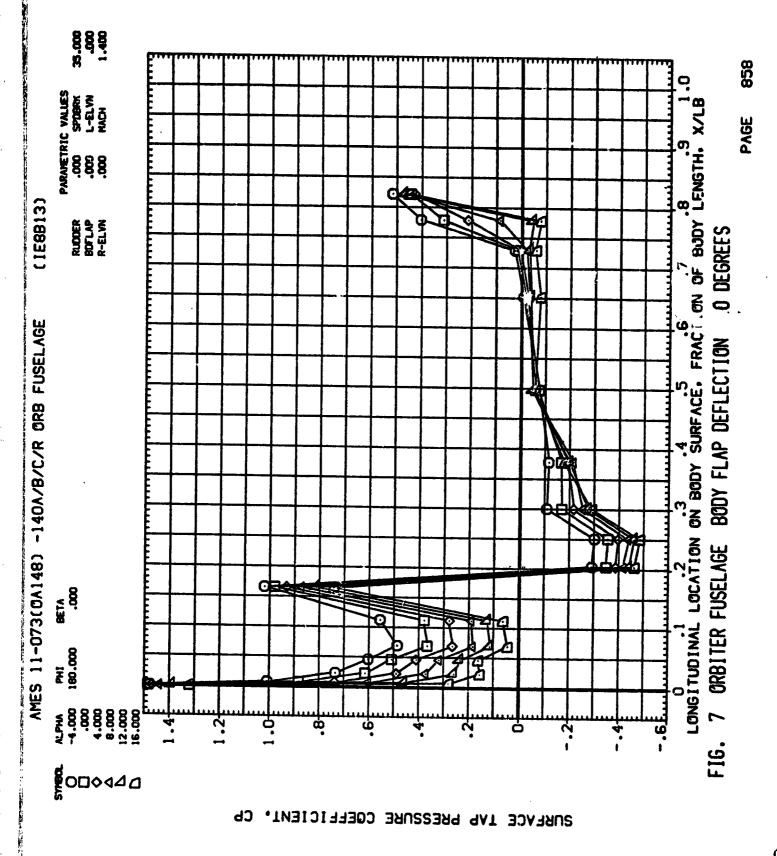
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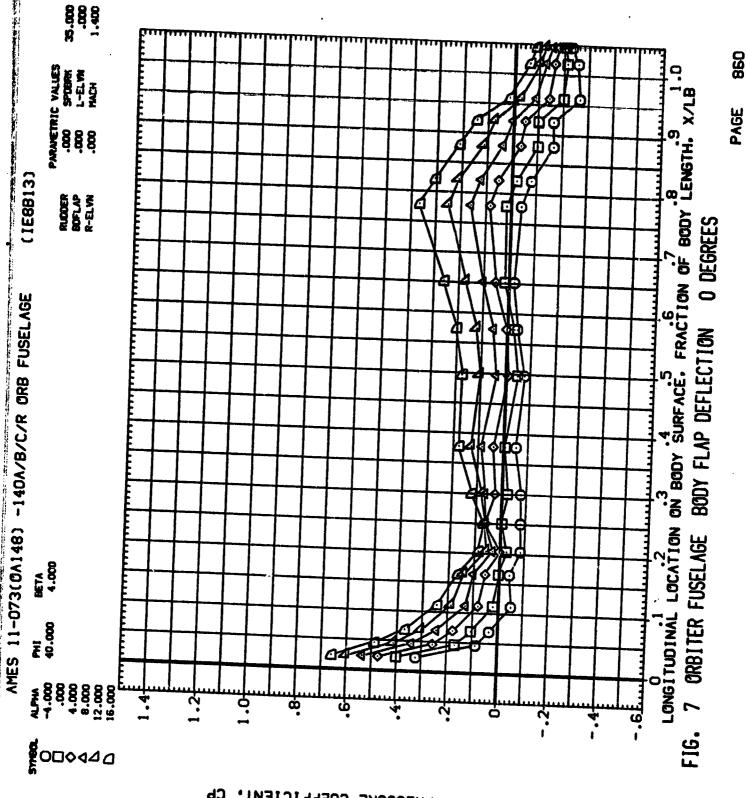


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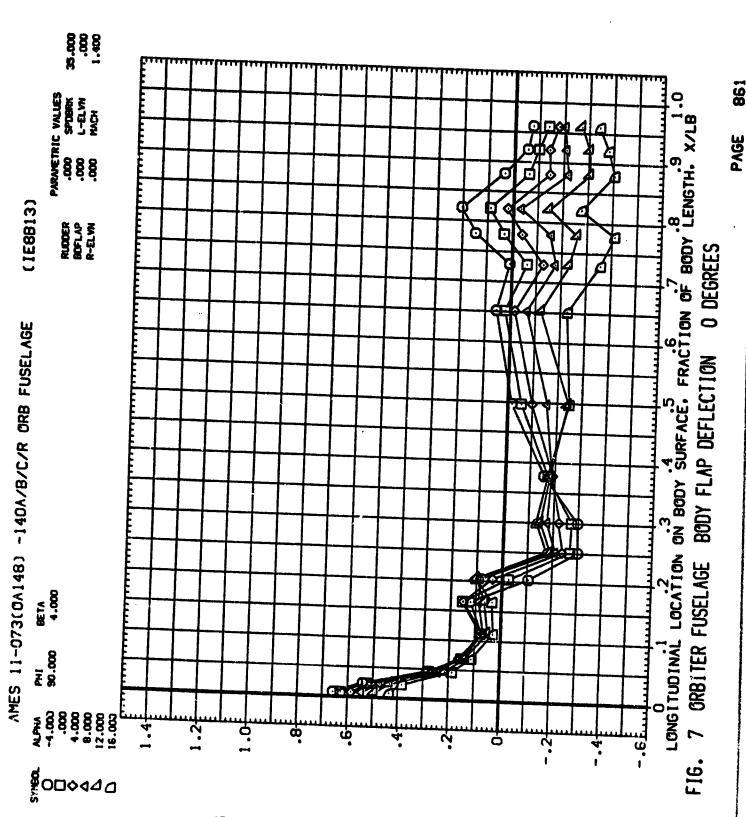
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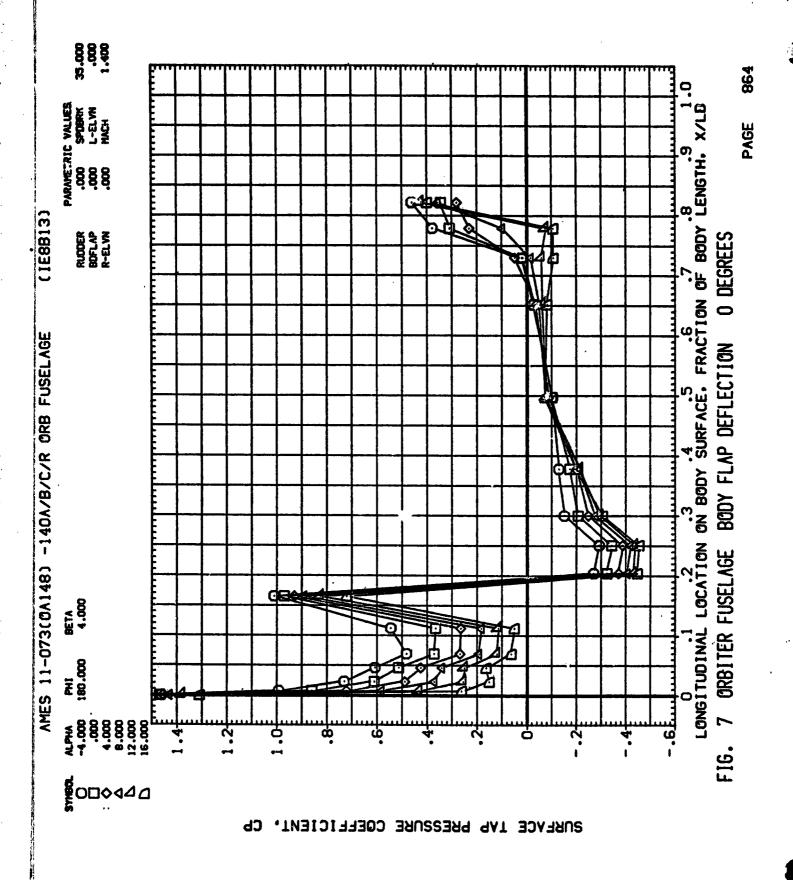


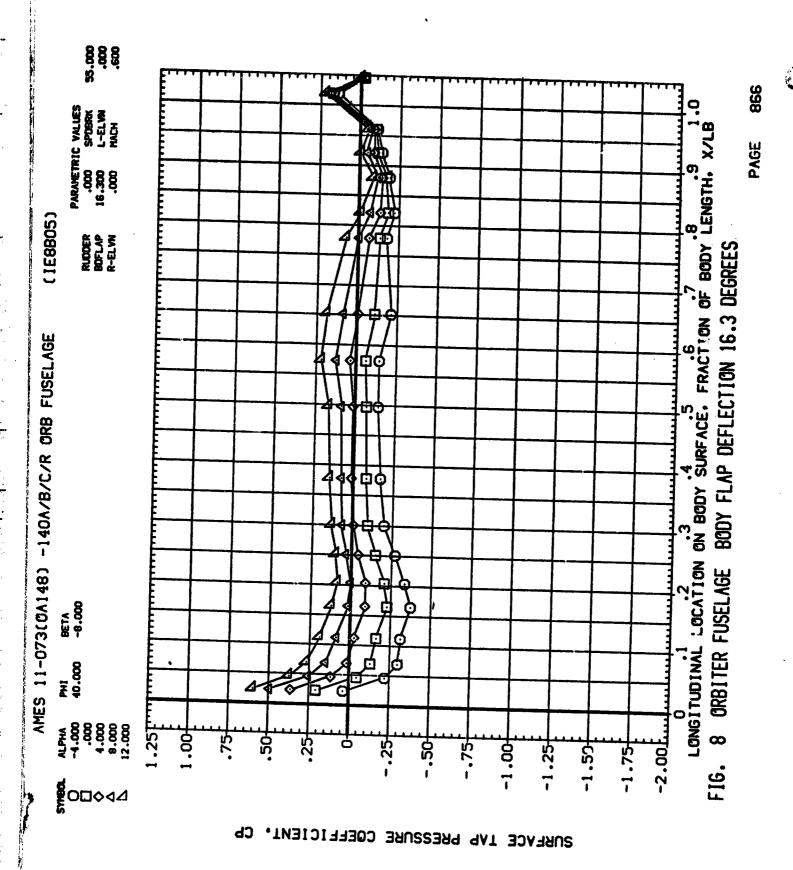
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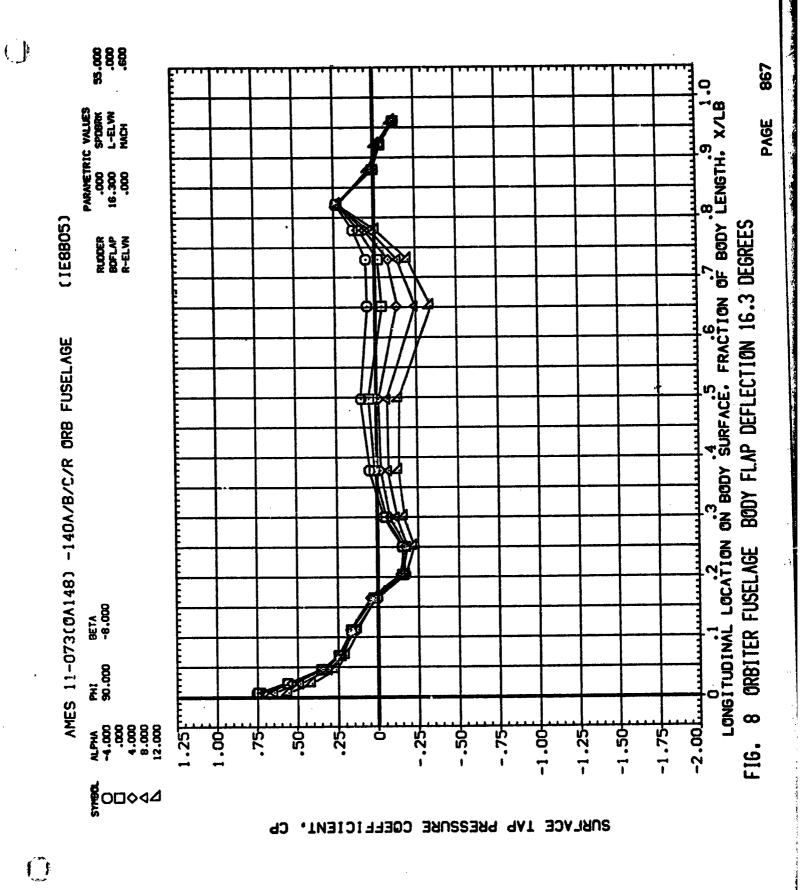


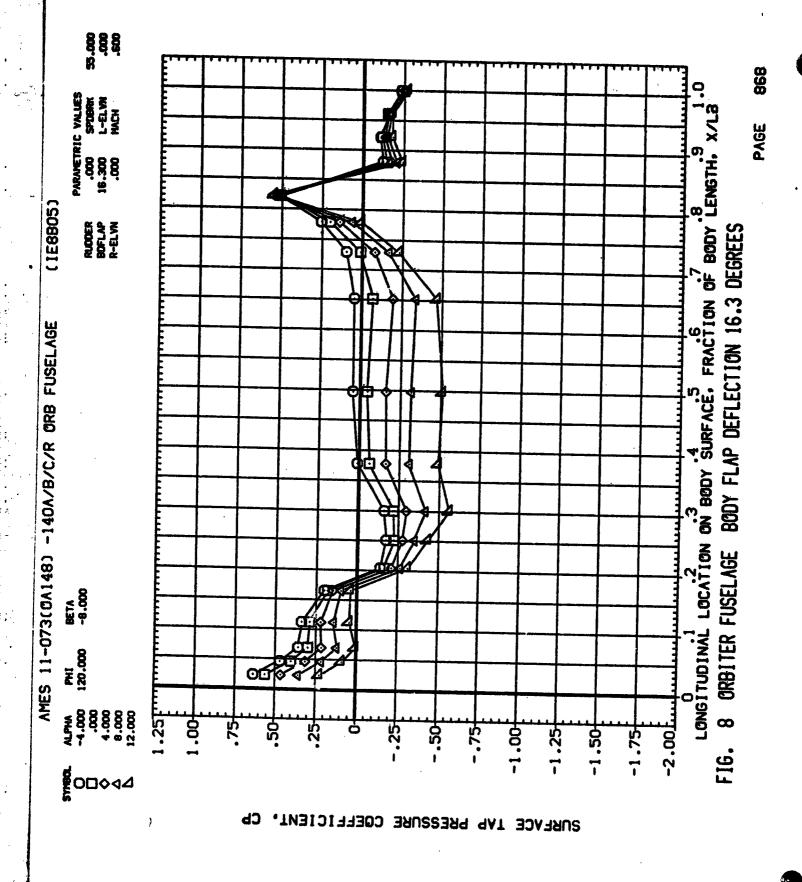
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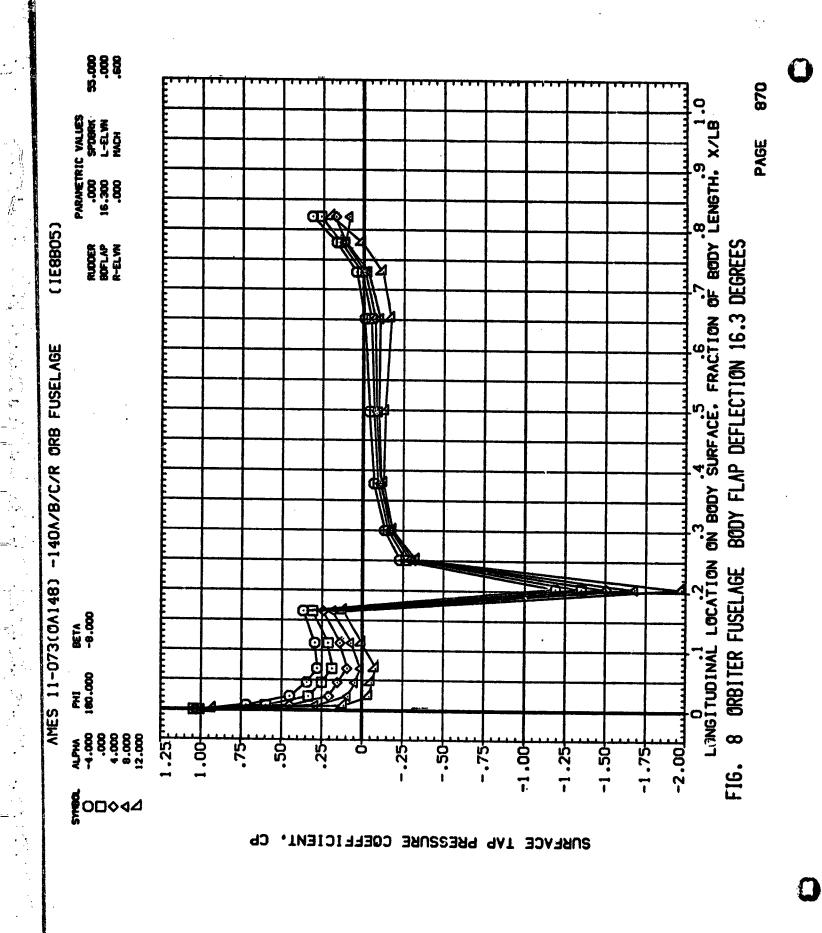


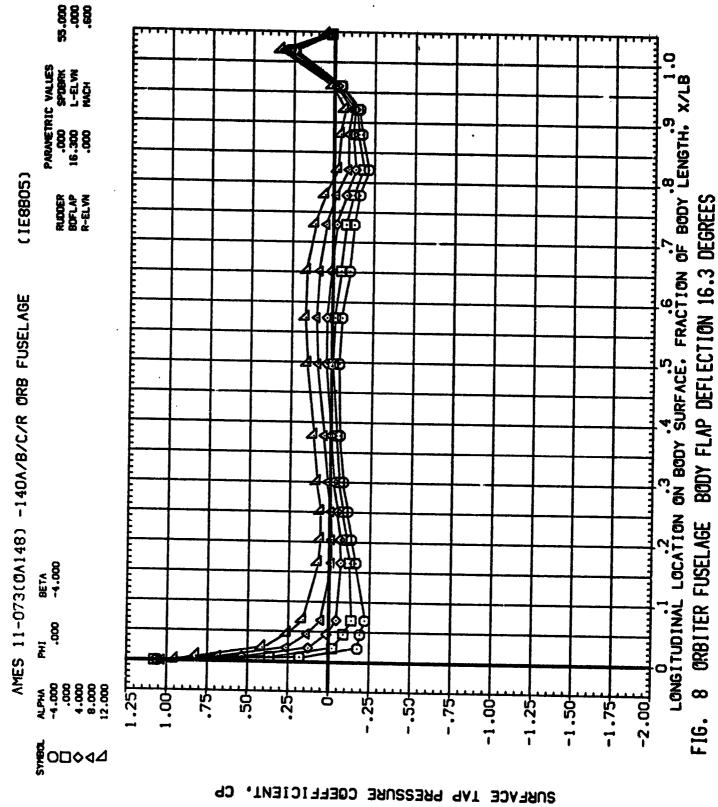




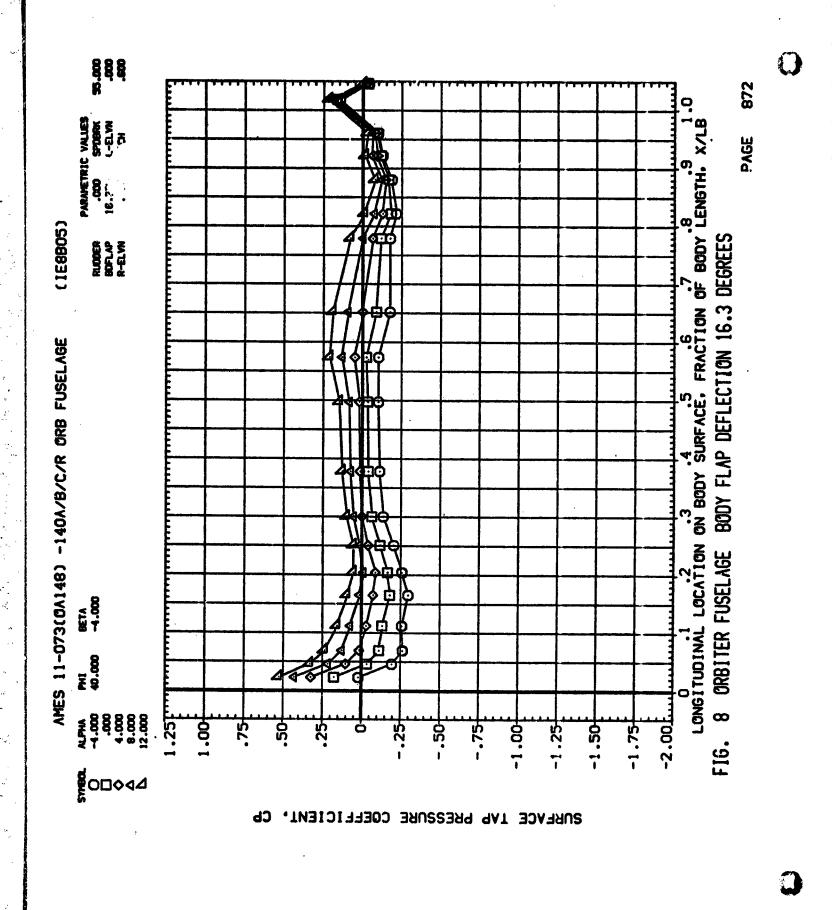


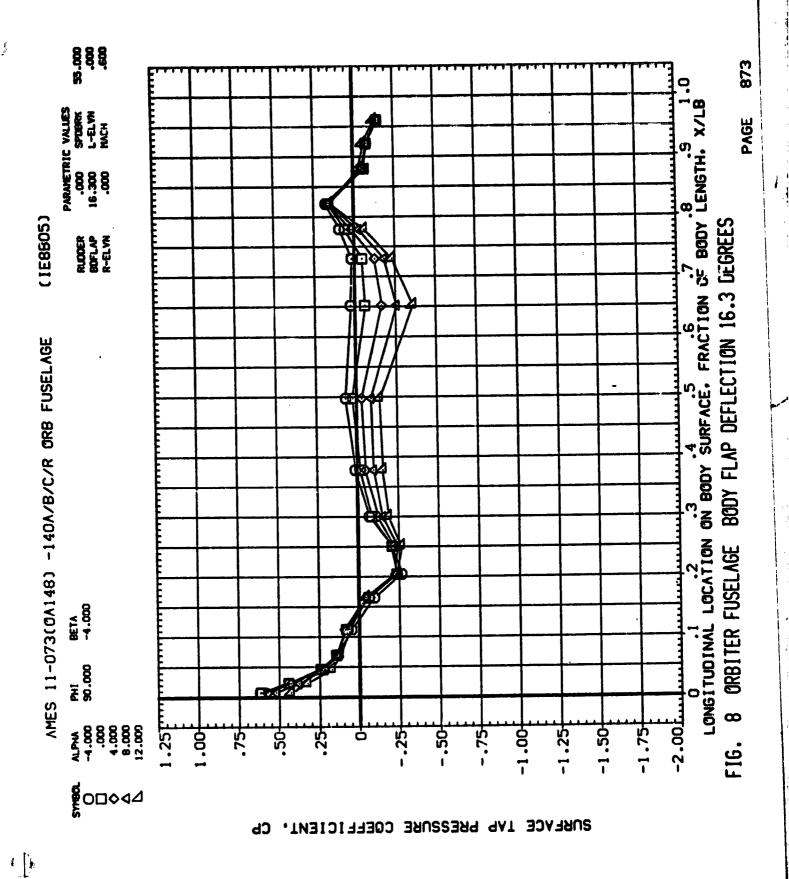
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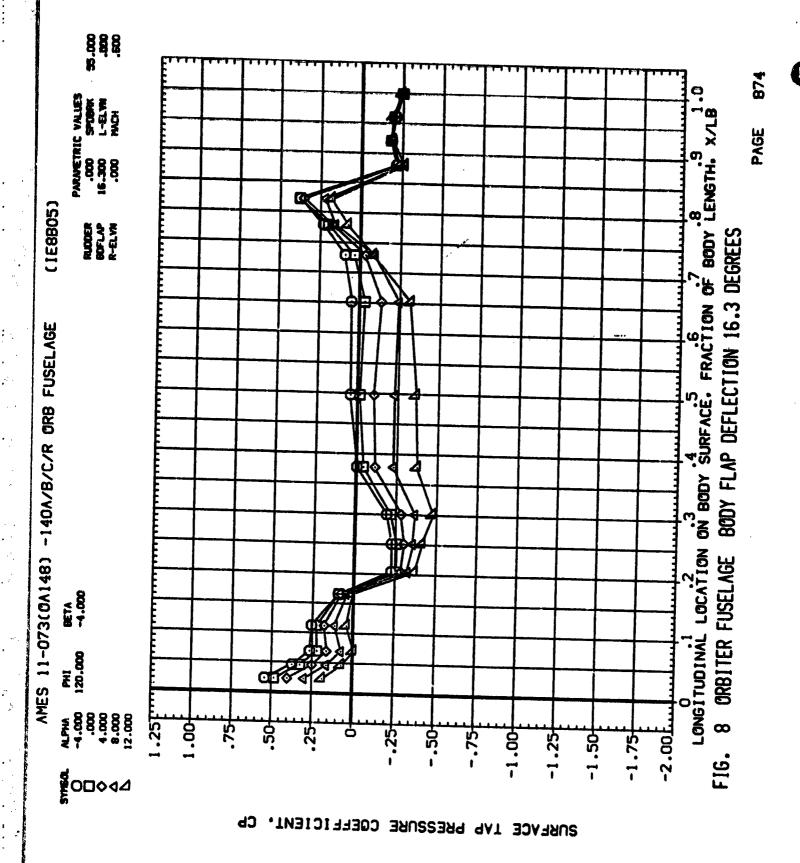




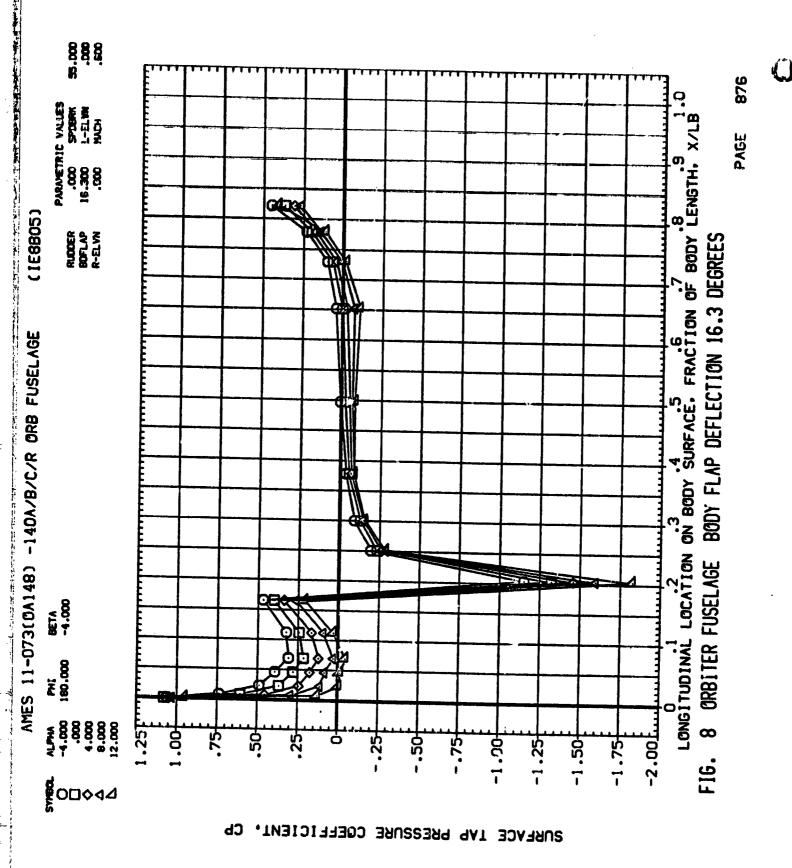
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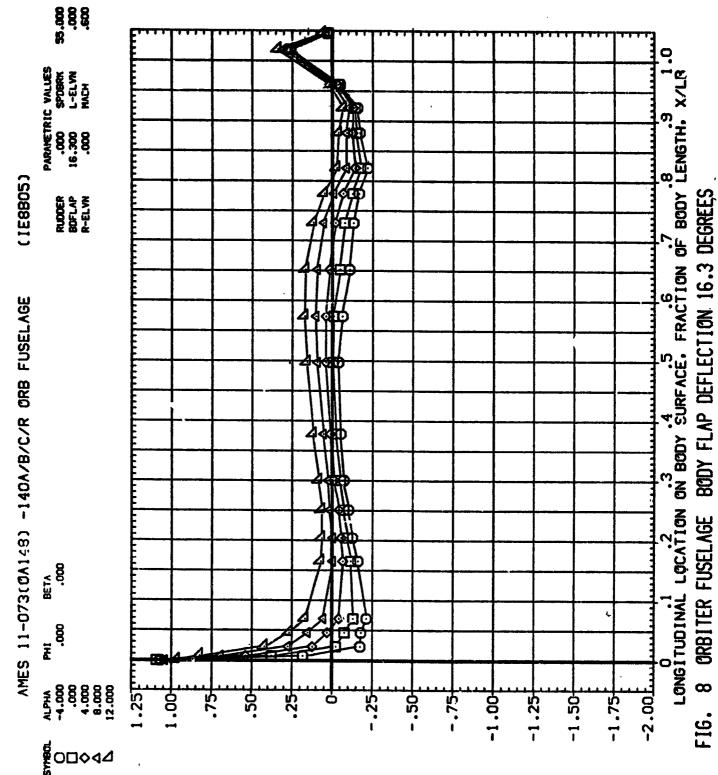




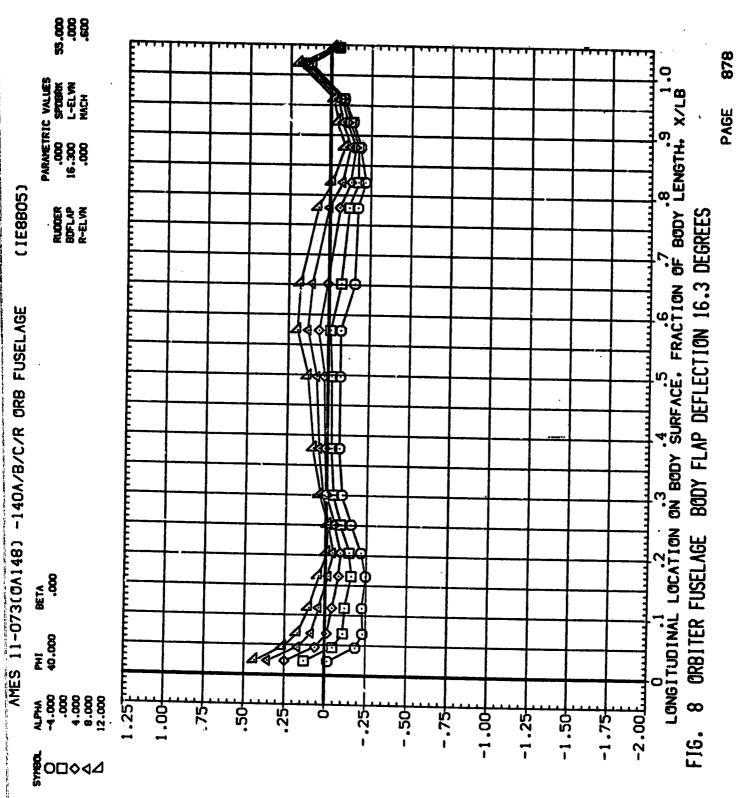


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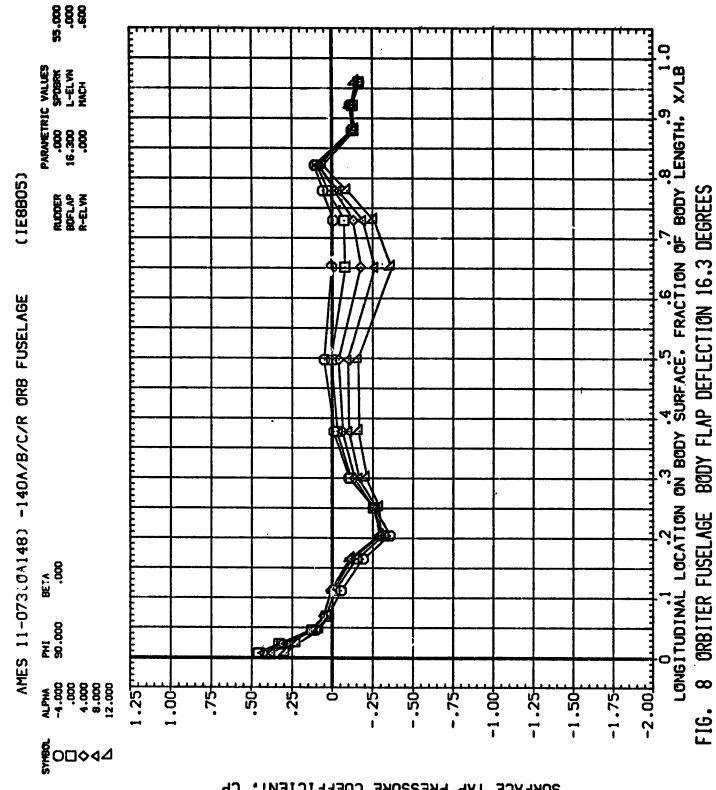


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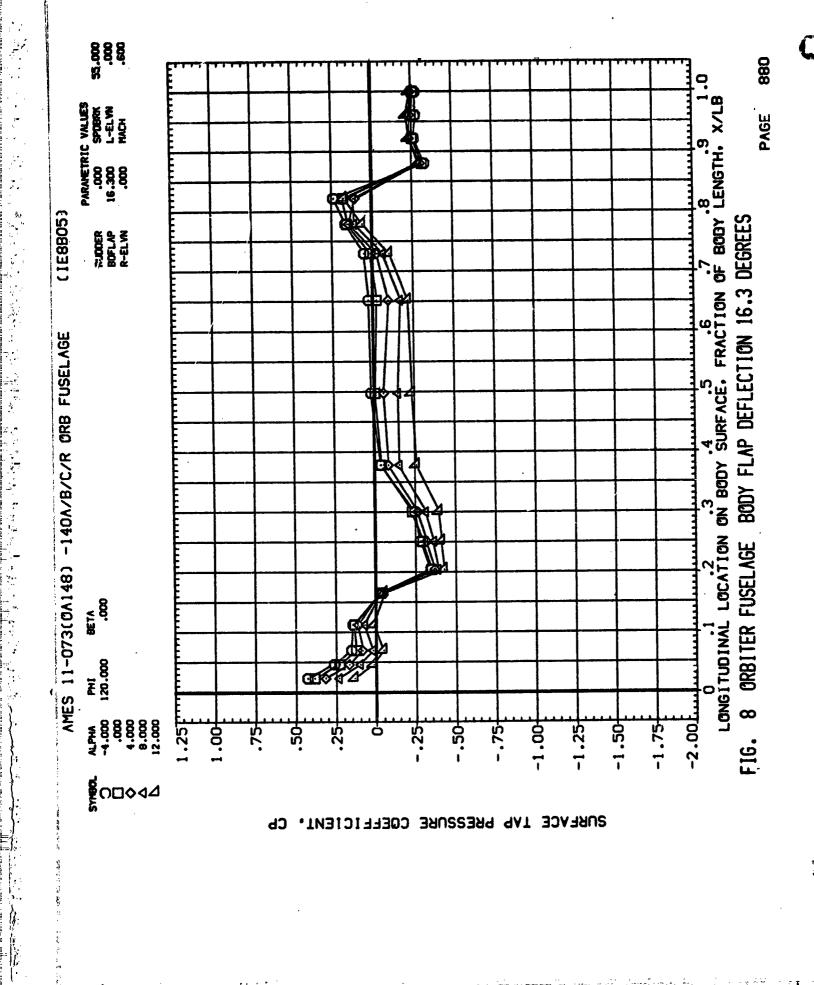


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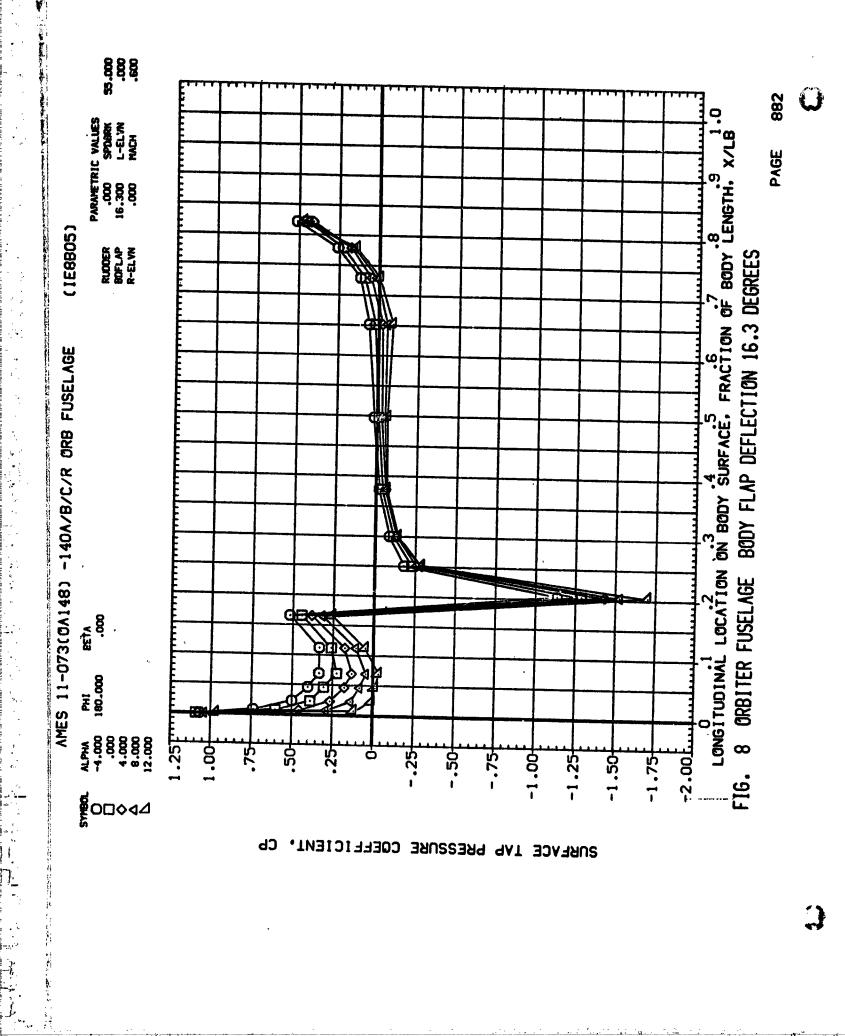
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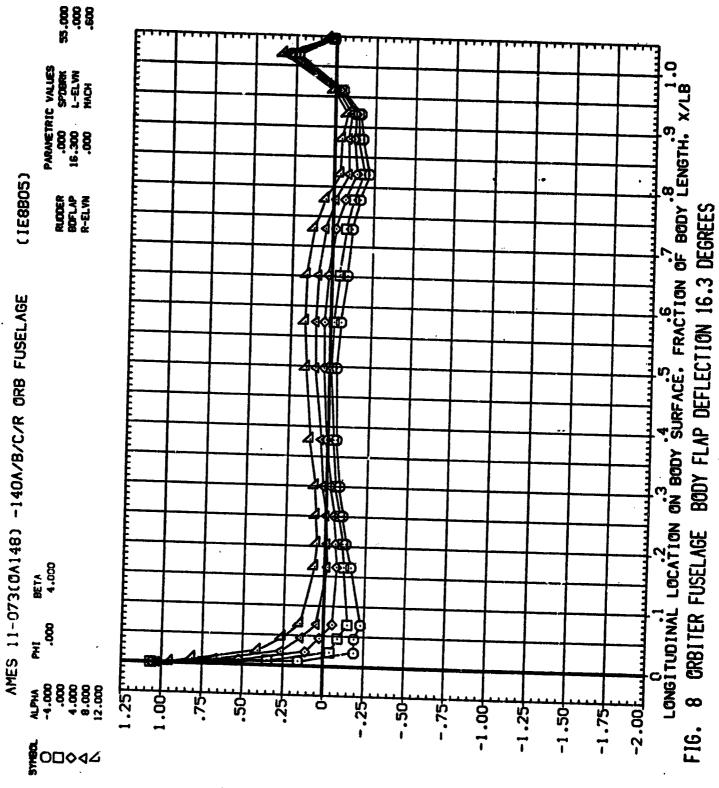


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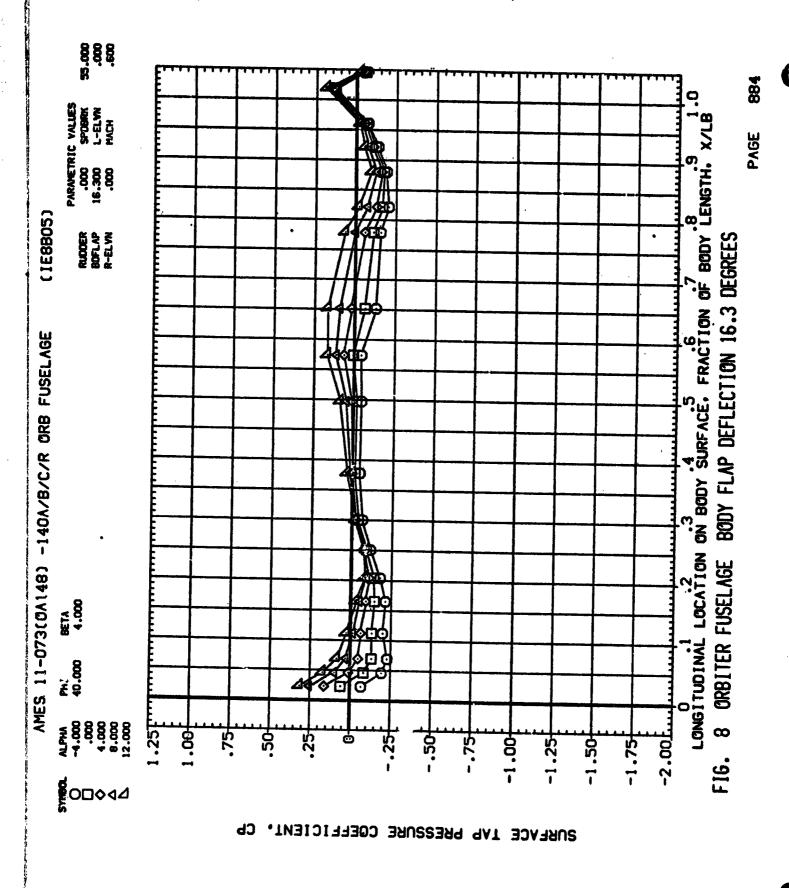


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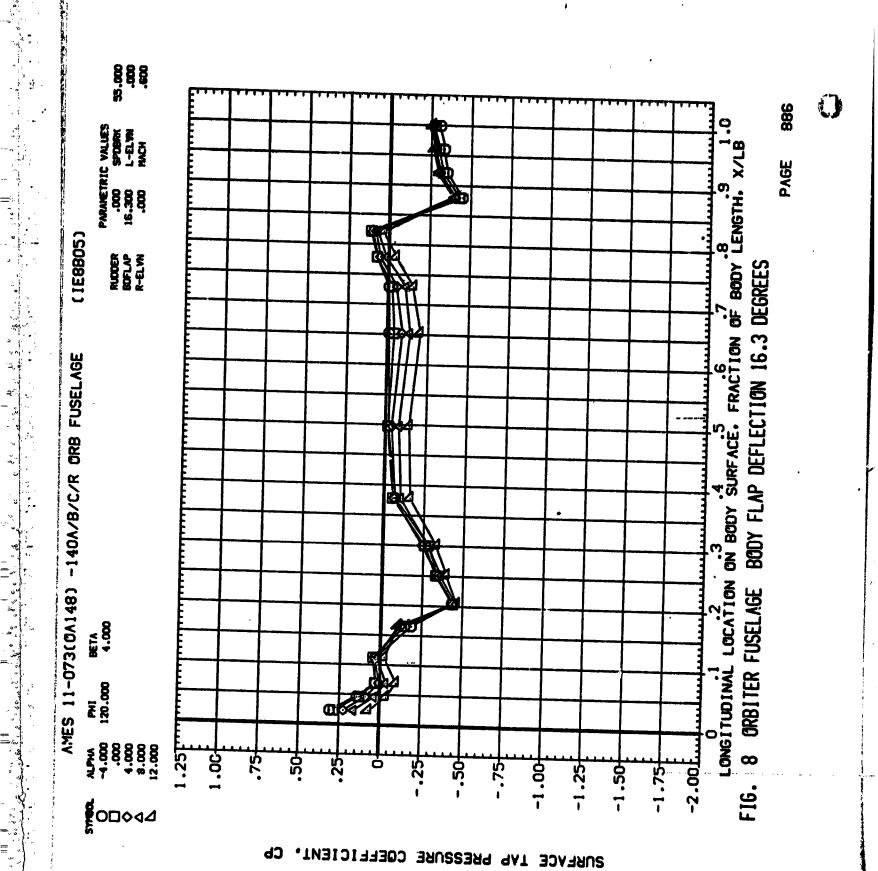




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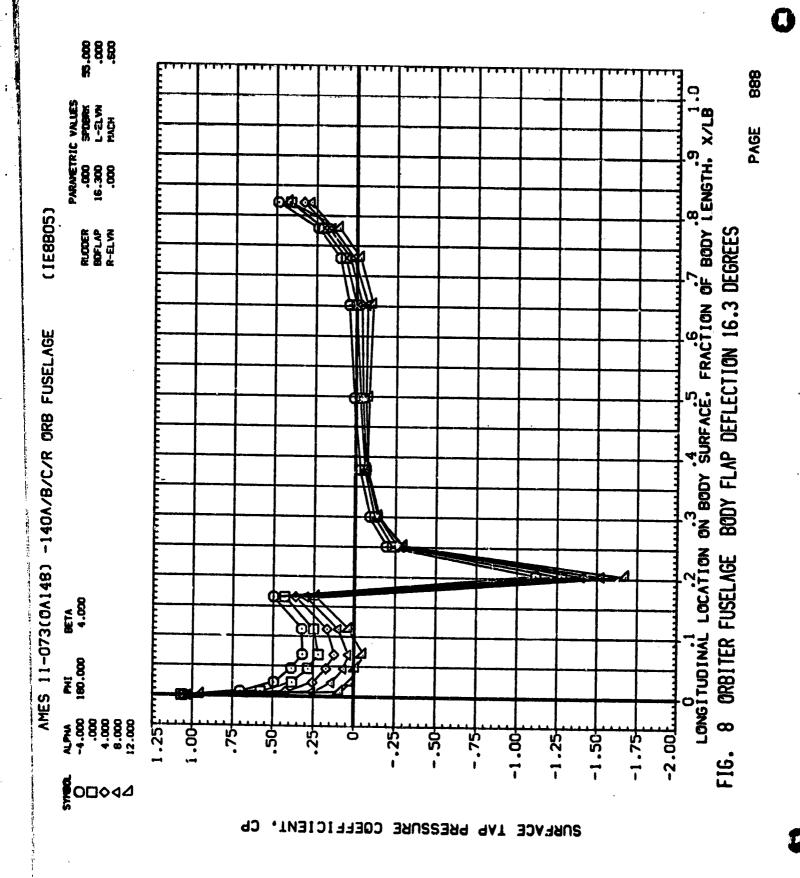


SURFACE TAP PRESSURE COEFFICIENT.

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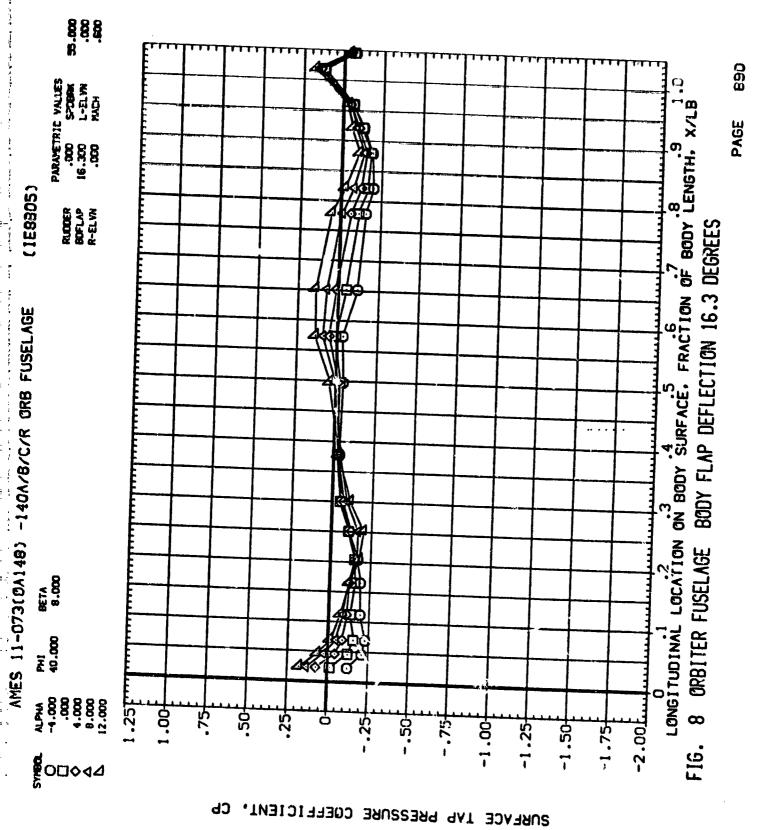
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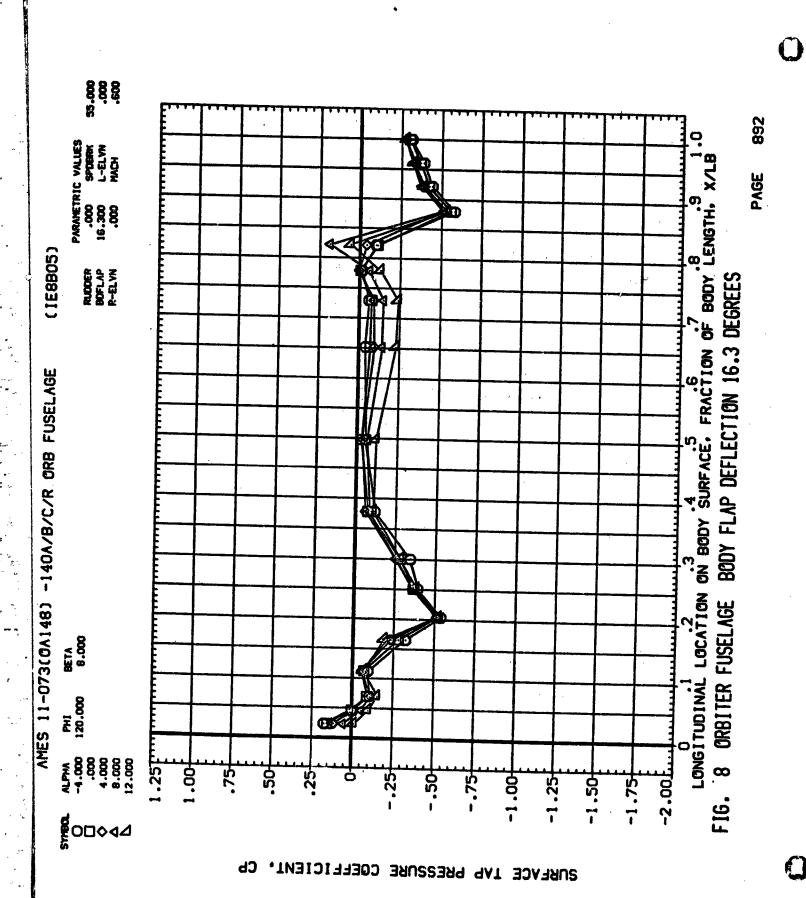
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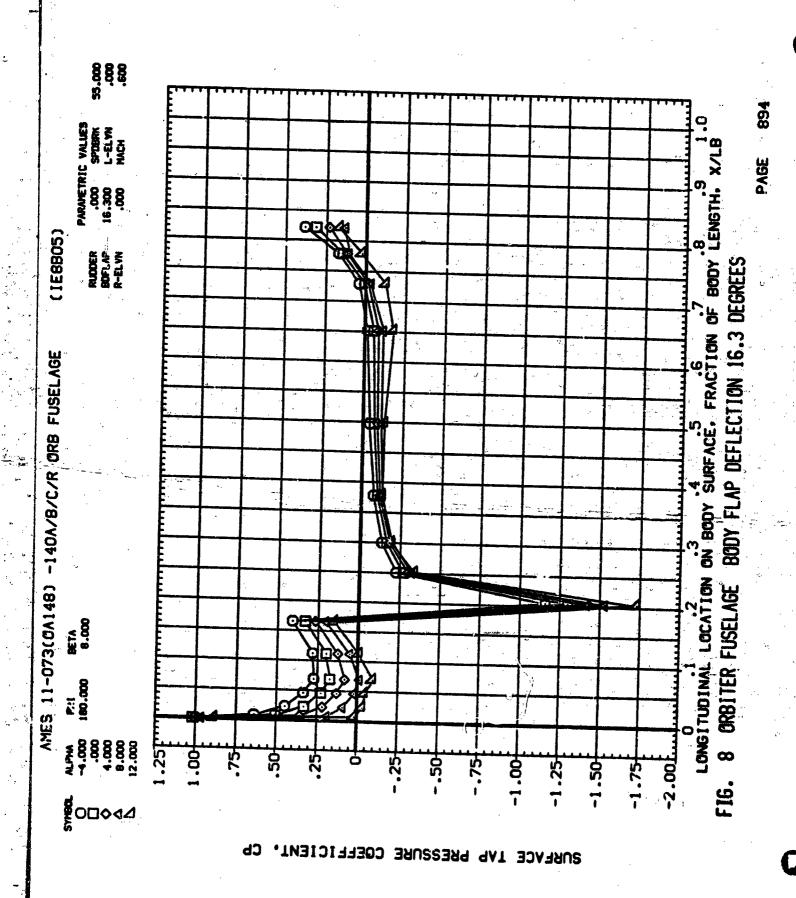
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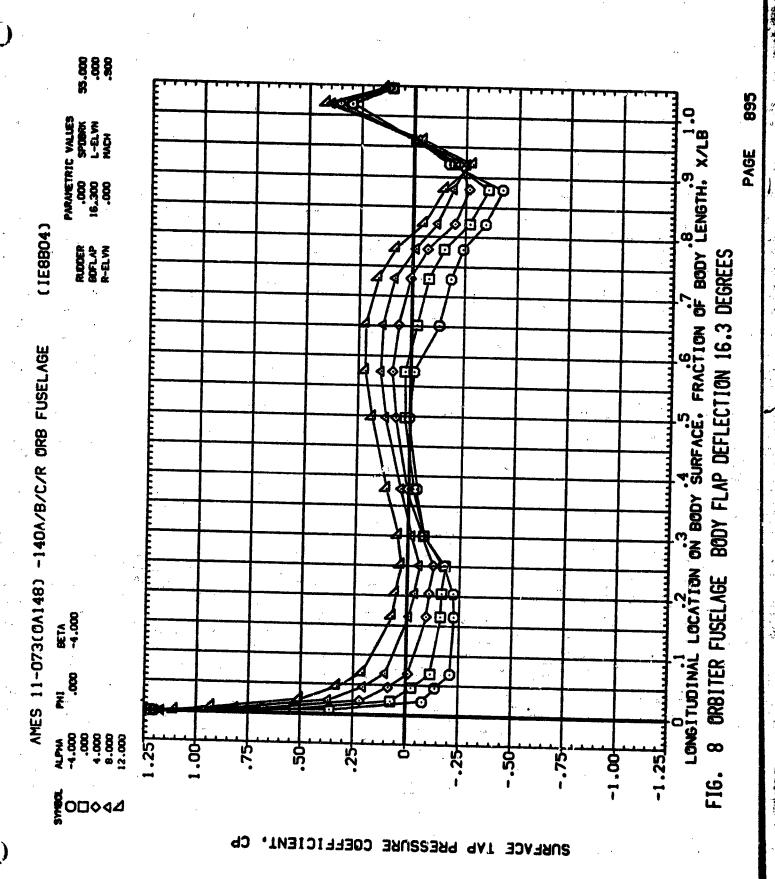


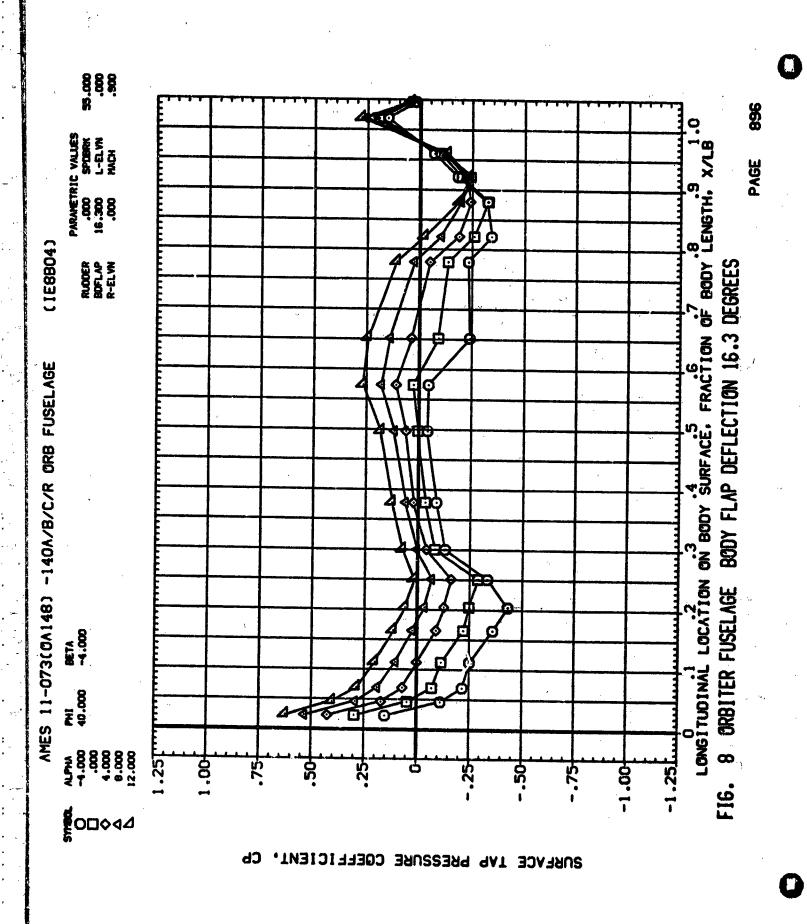
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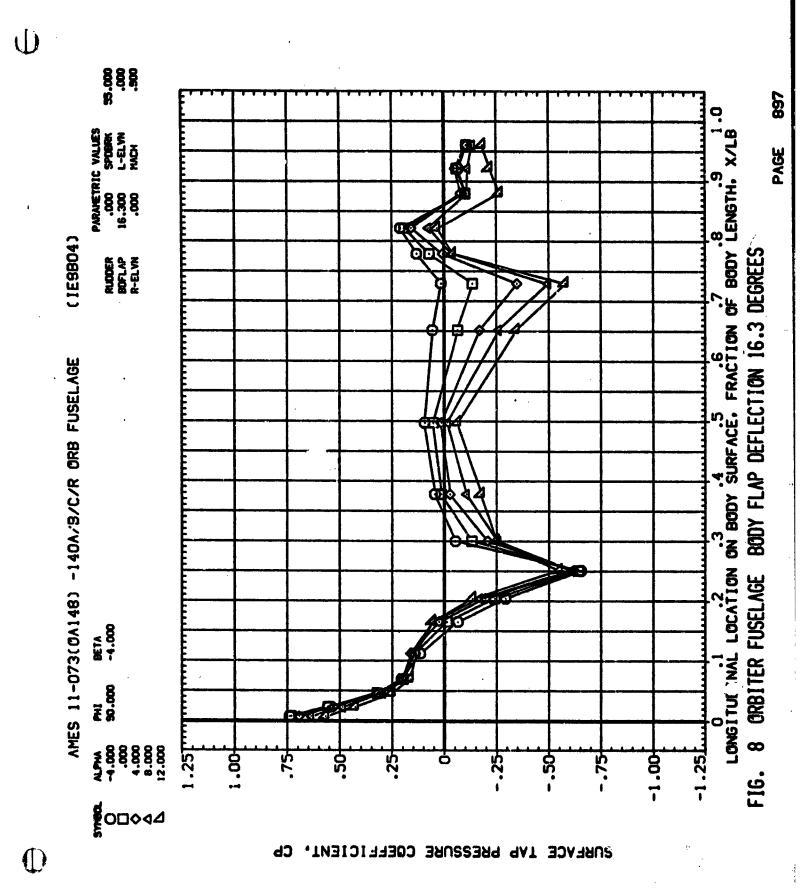


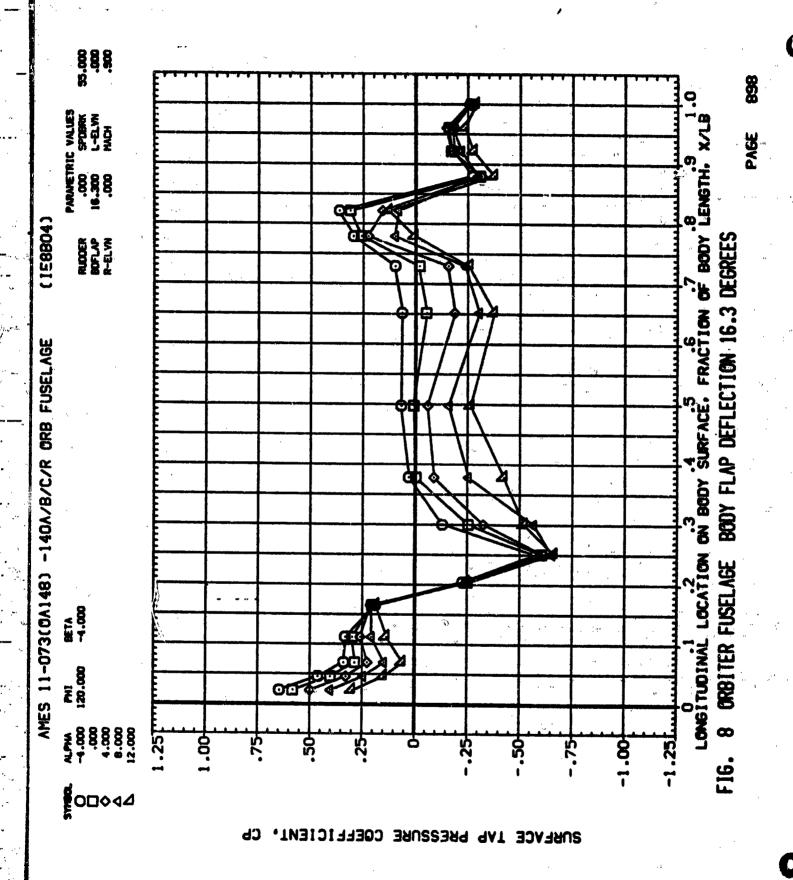
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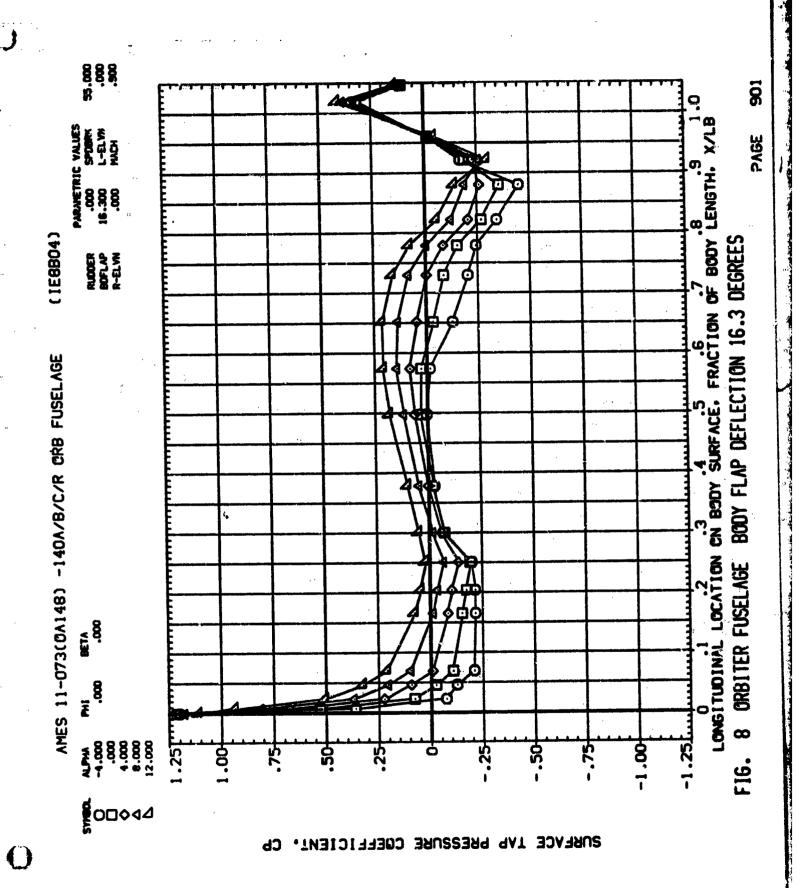




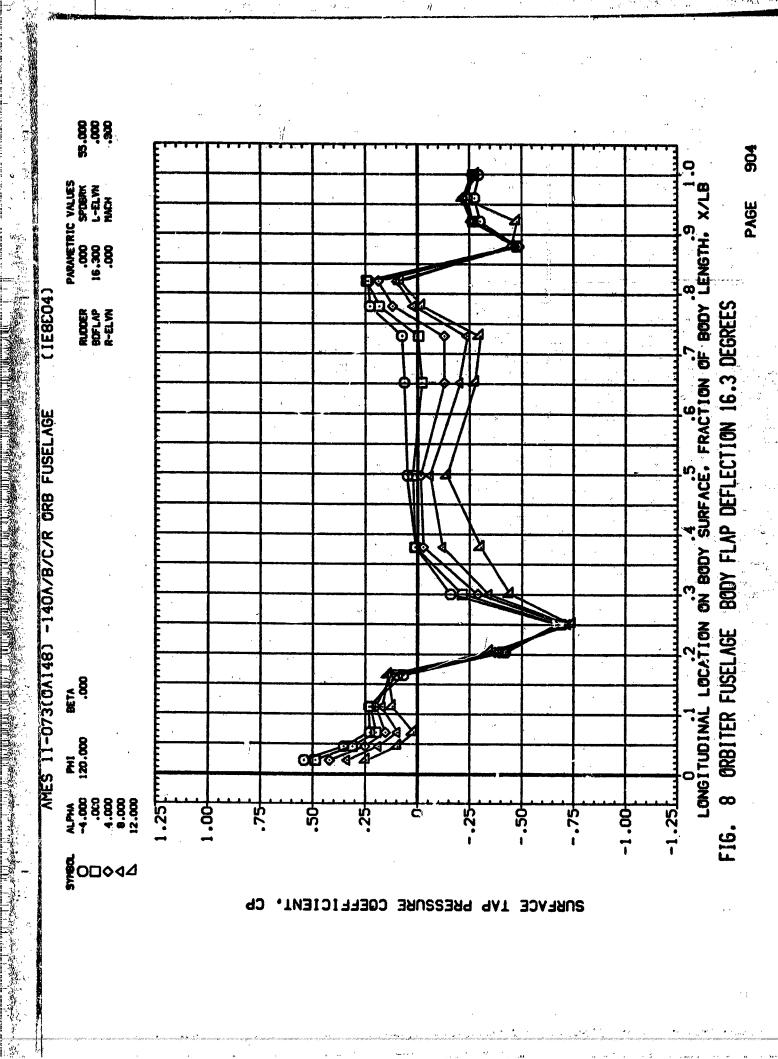


PRESSURE COEFFICIENT,

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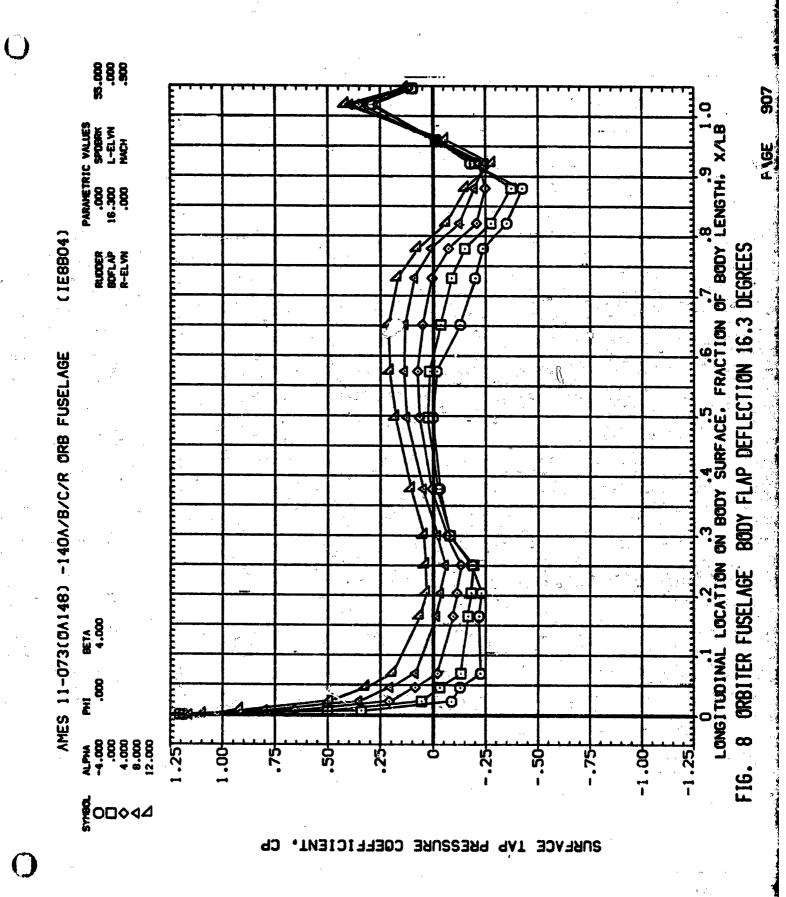


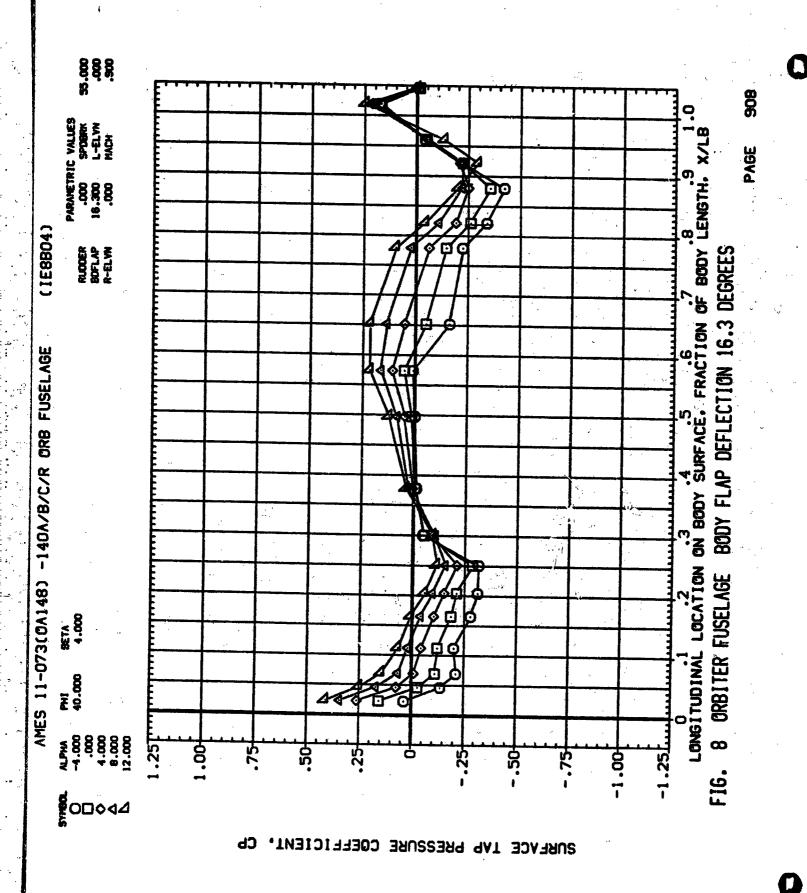
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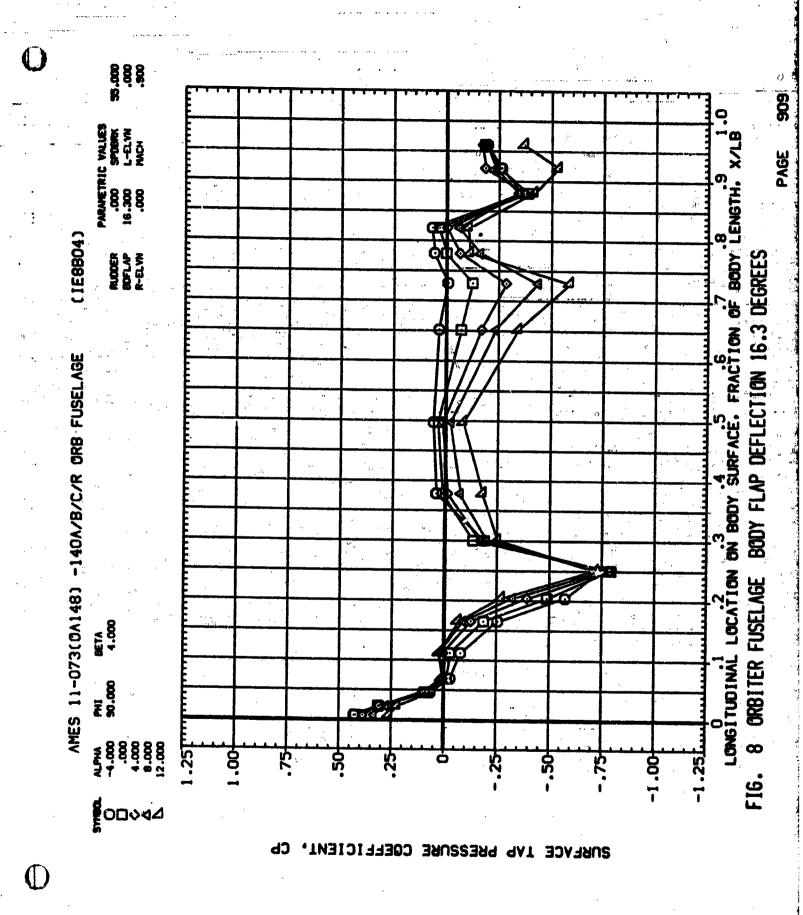
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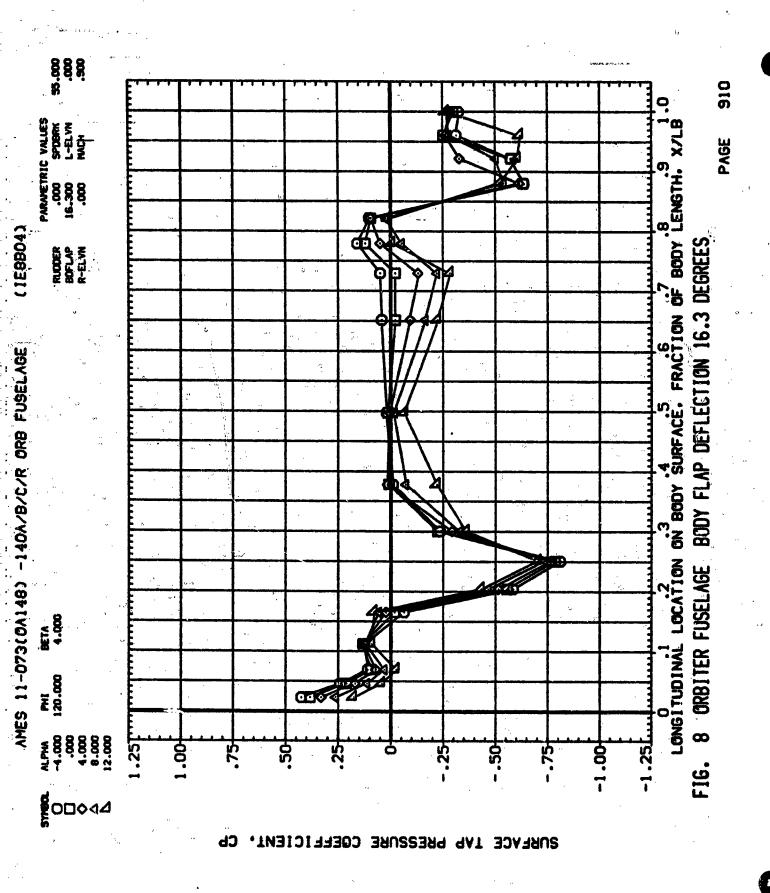
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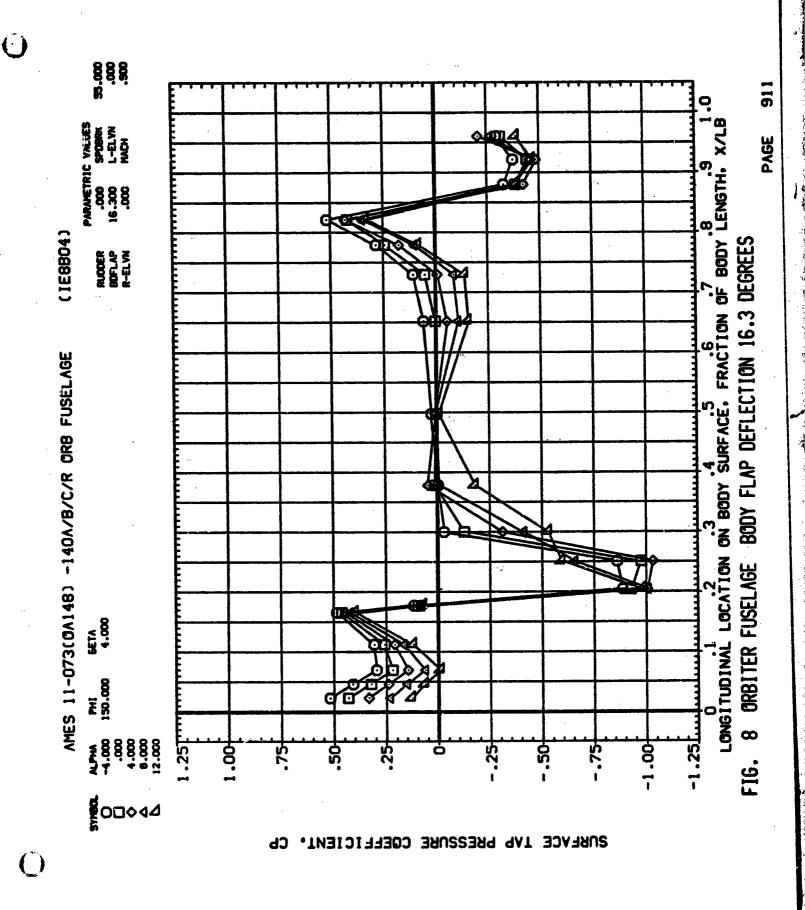
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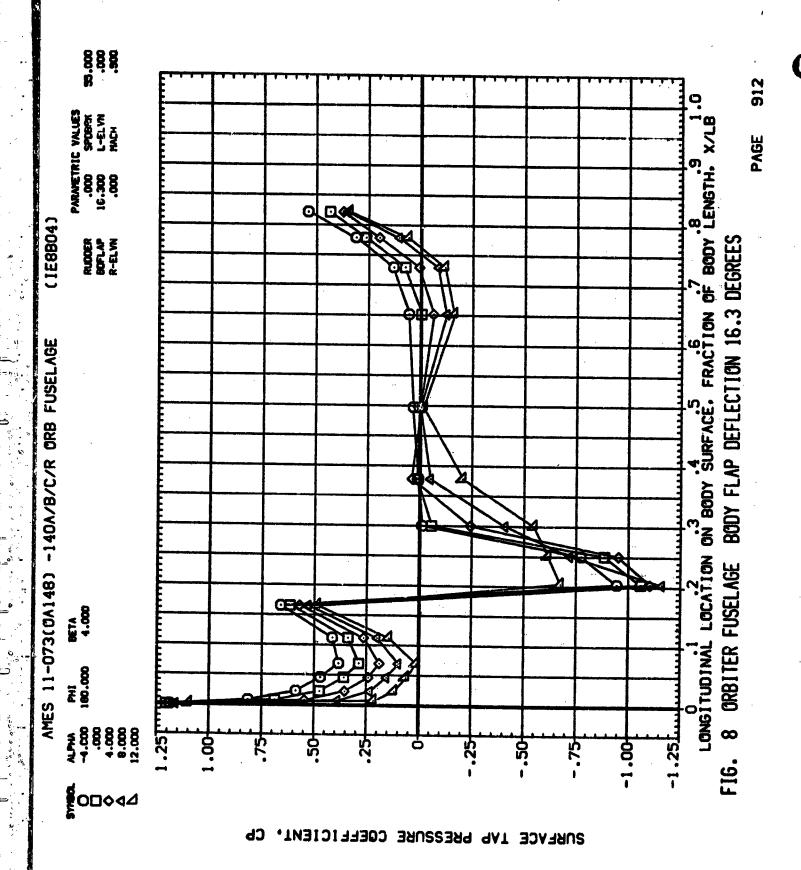


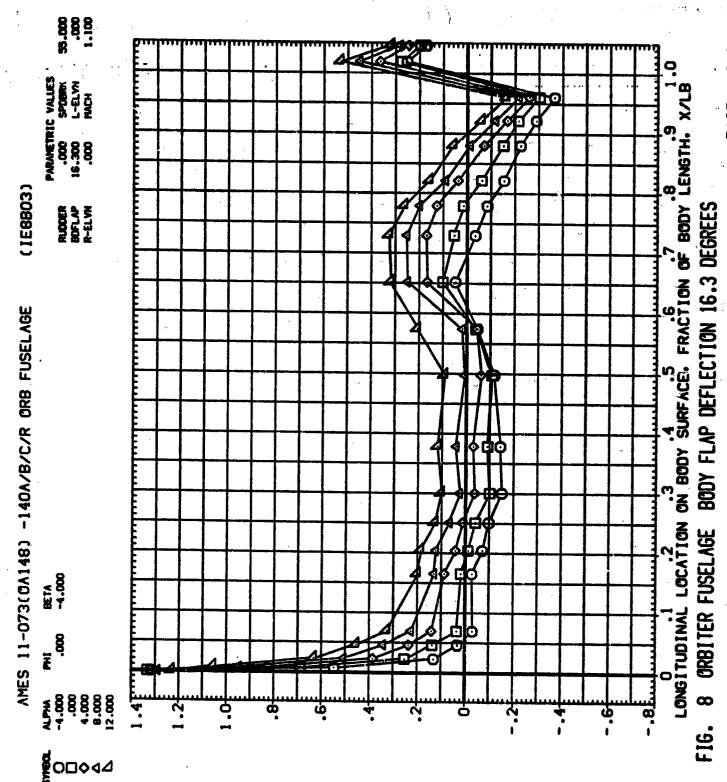






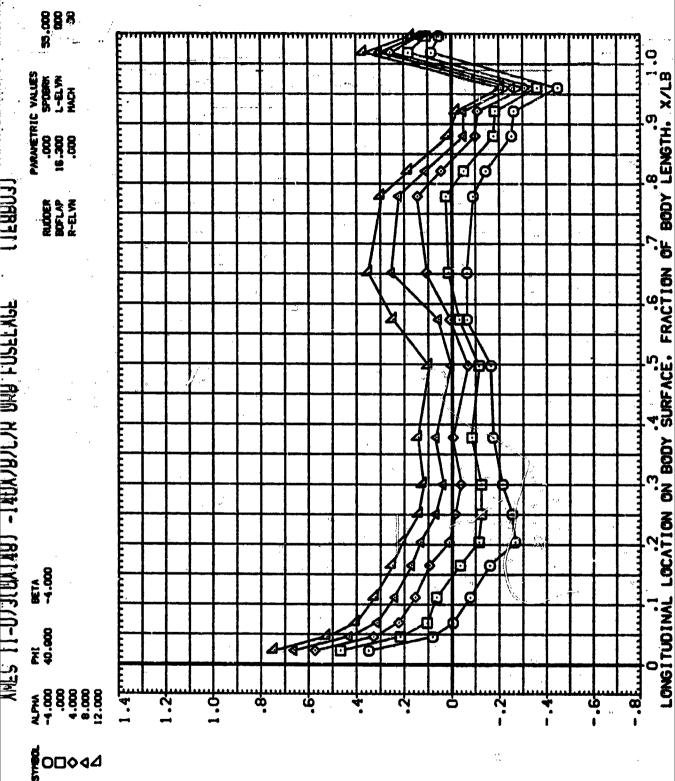


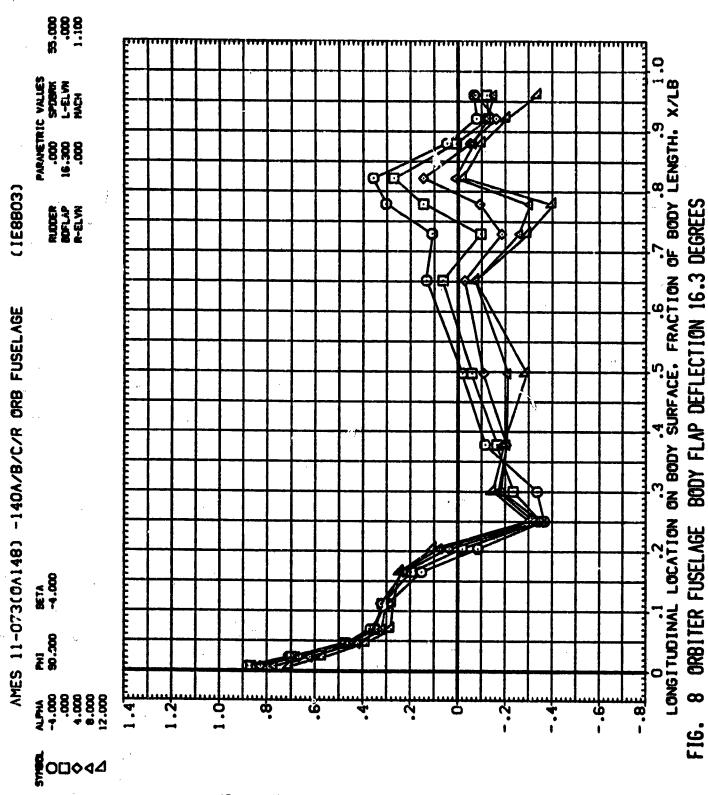




SURFACE TAP PRESSURE COEFFICIENT, C

SURFACE TAP PRESSURE COEFFICIENT, CP





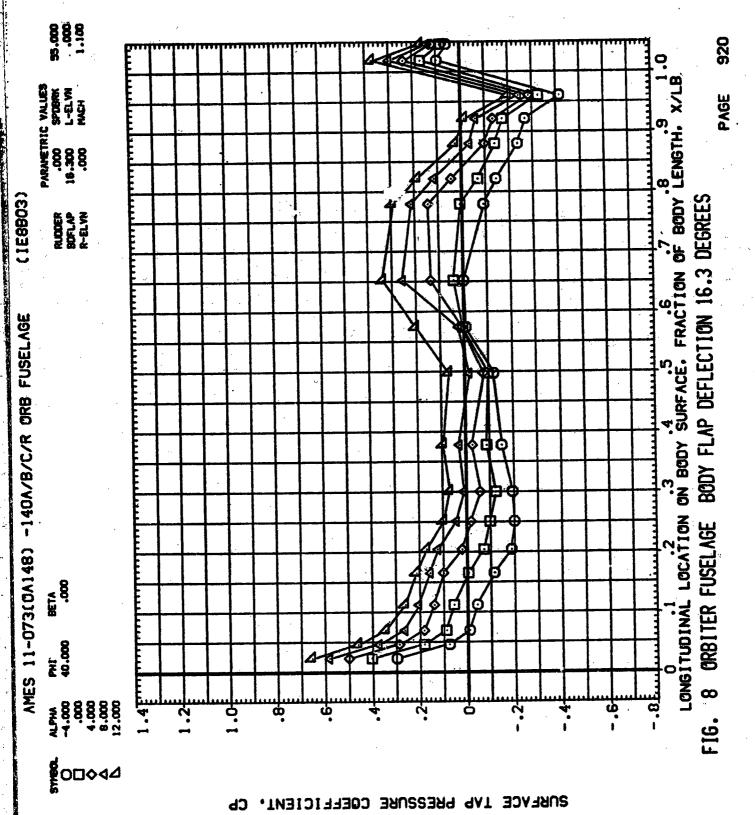
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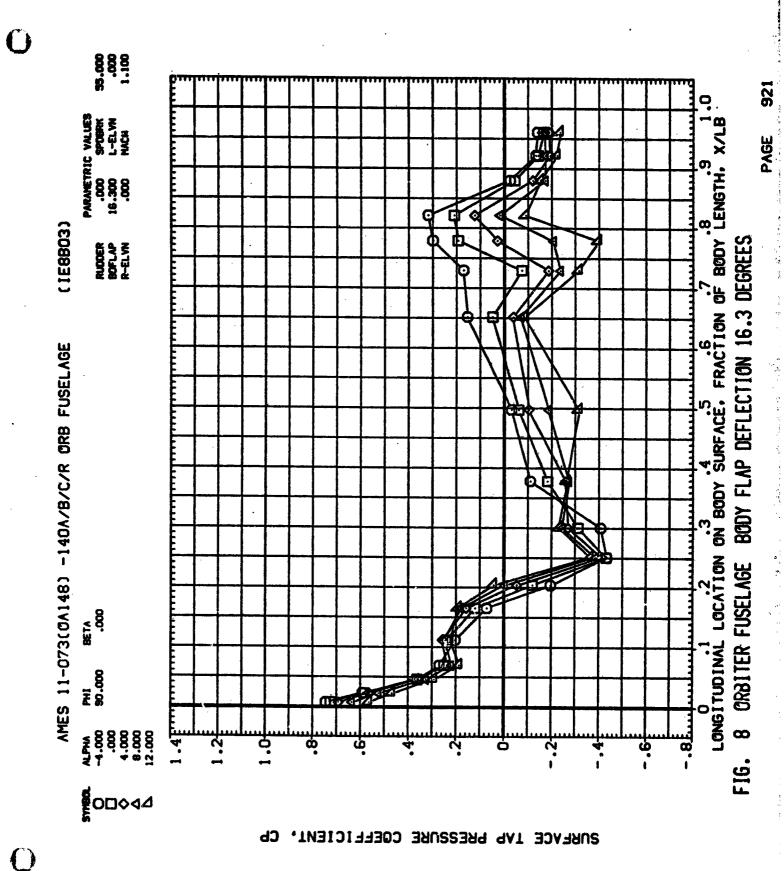
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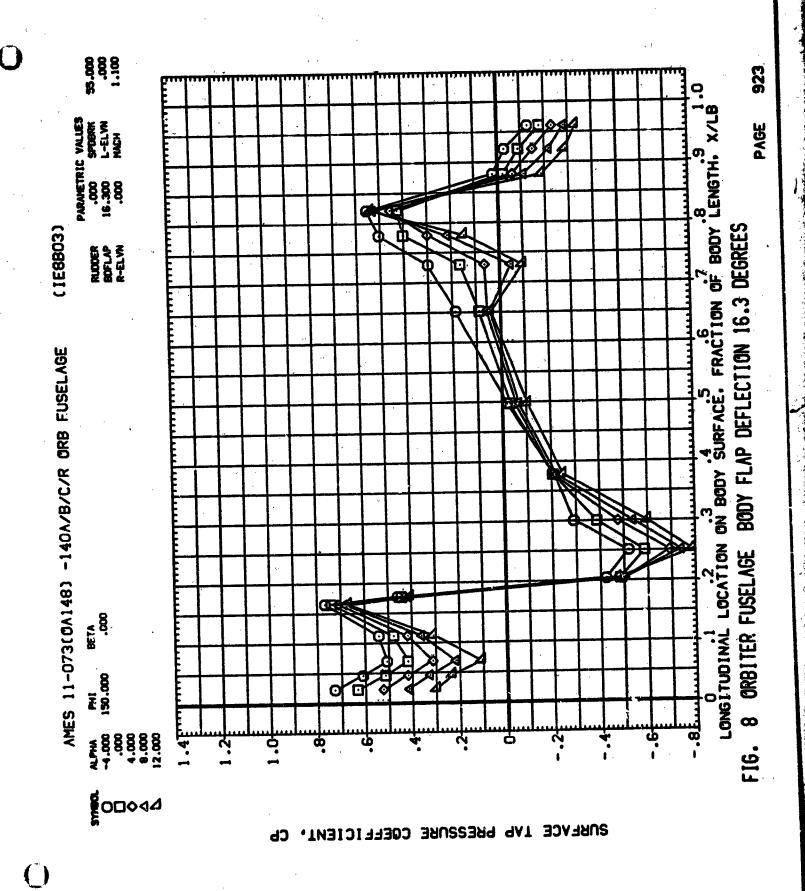
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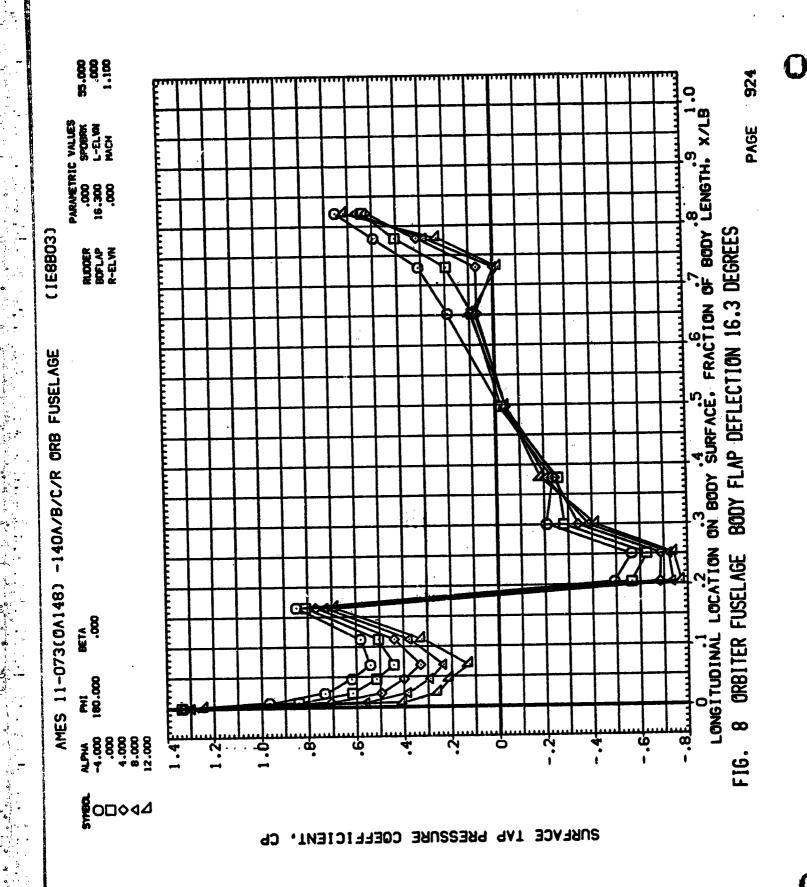
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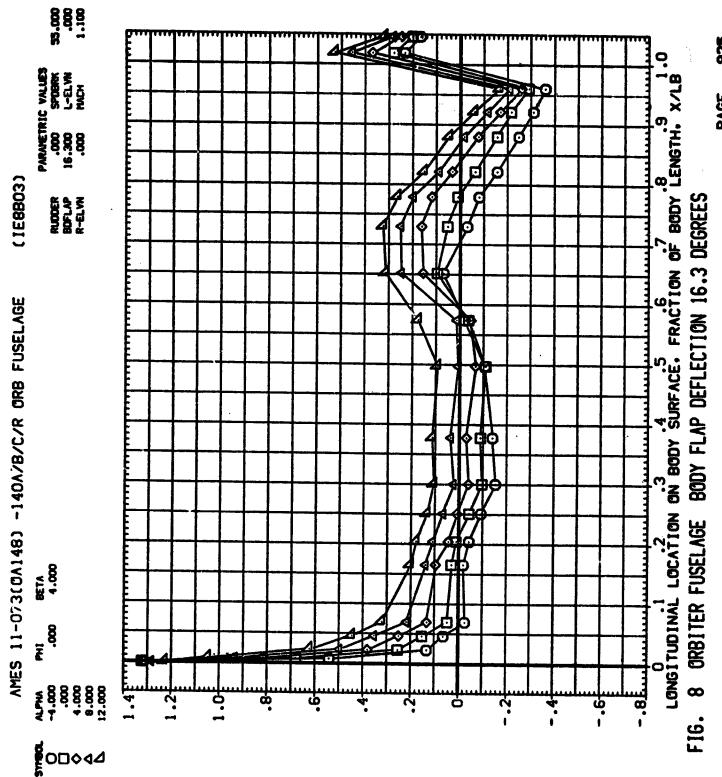


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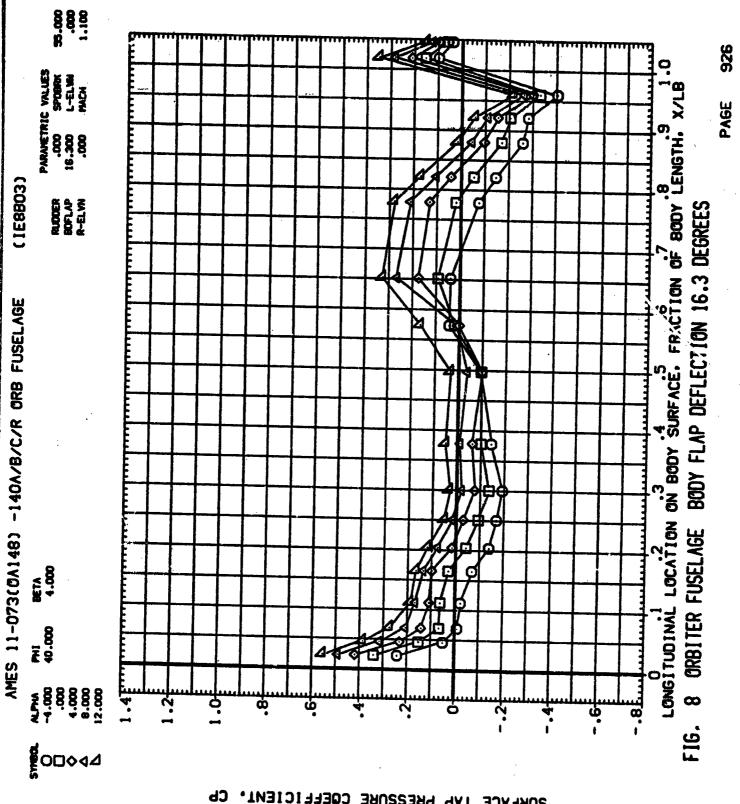




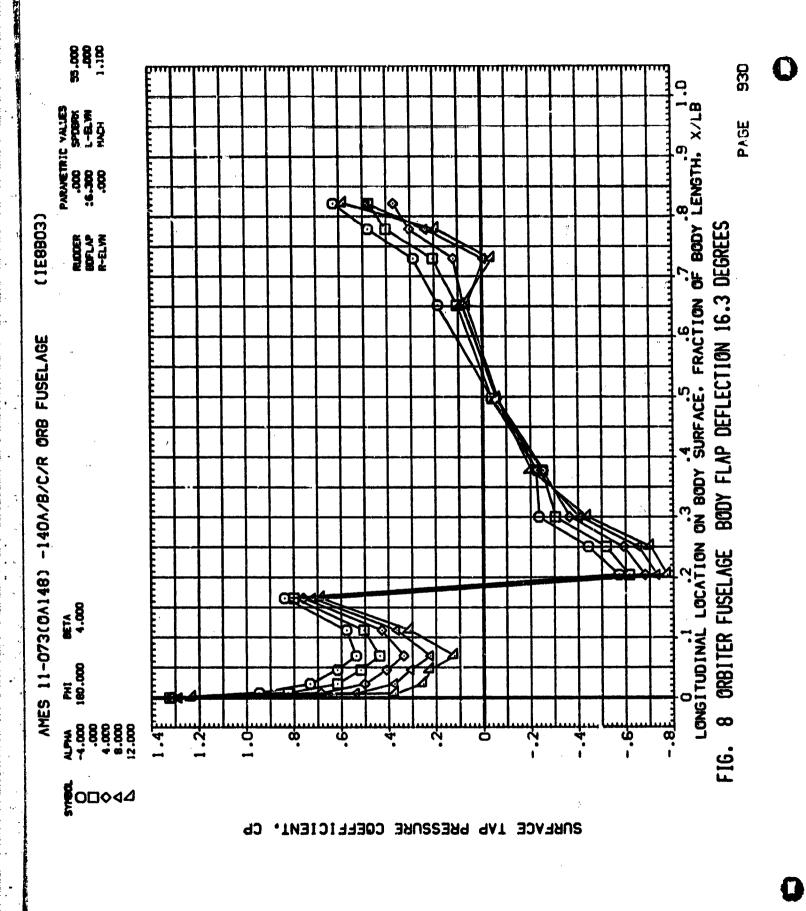


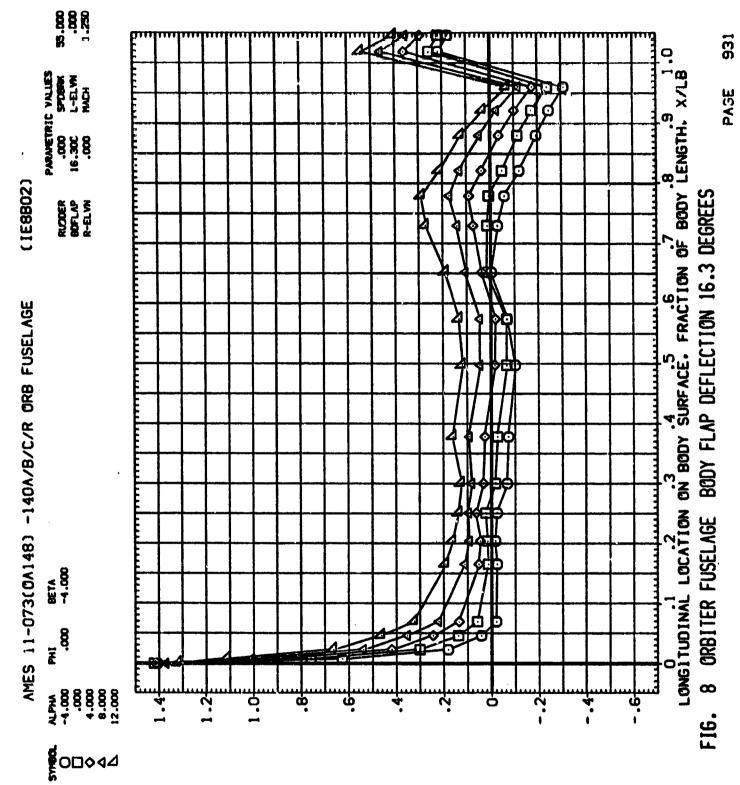


SURFACE TAP PRESSURE COEFFICIENT,



SURFACE TAP PRESSURE COEFFICIENT.

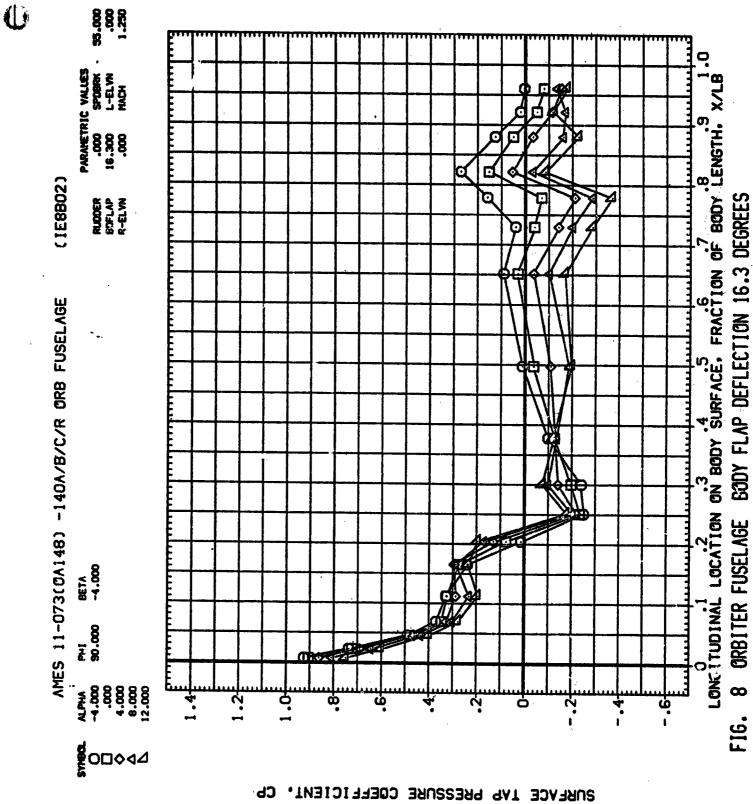




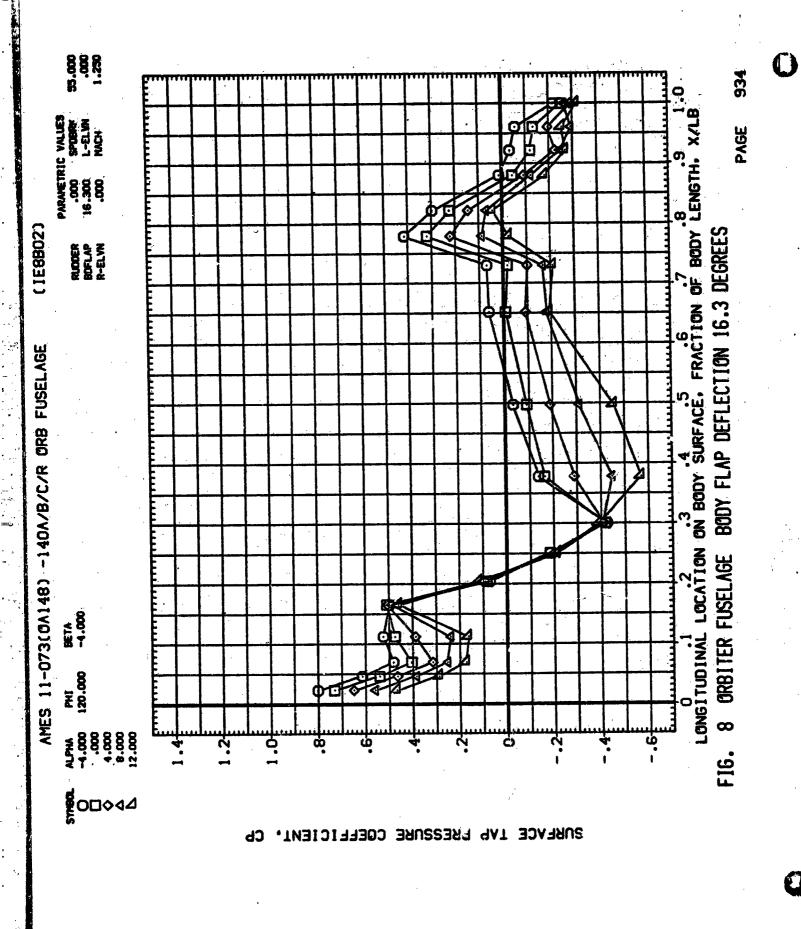
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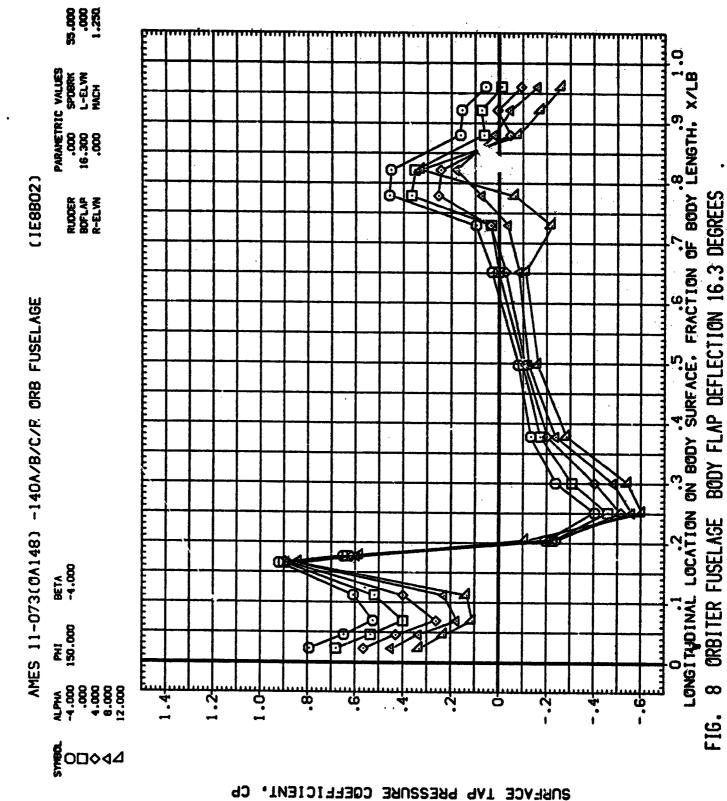
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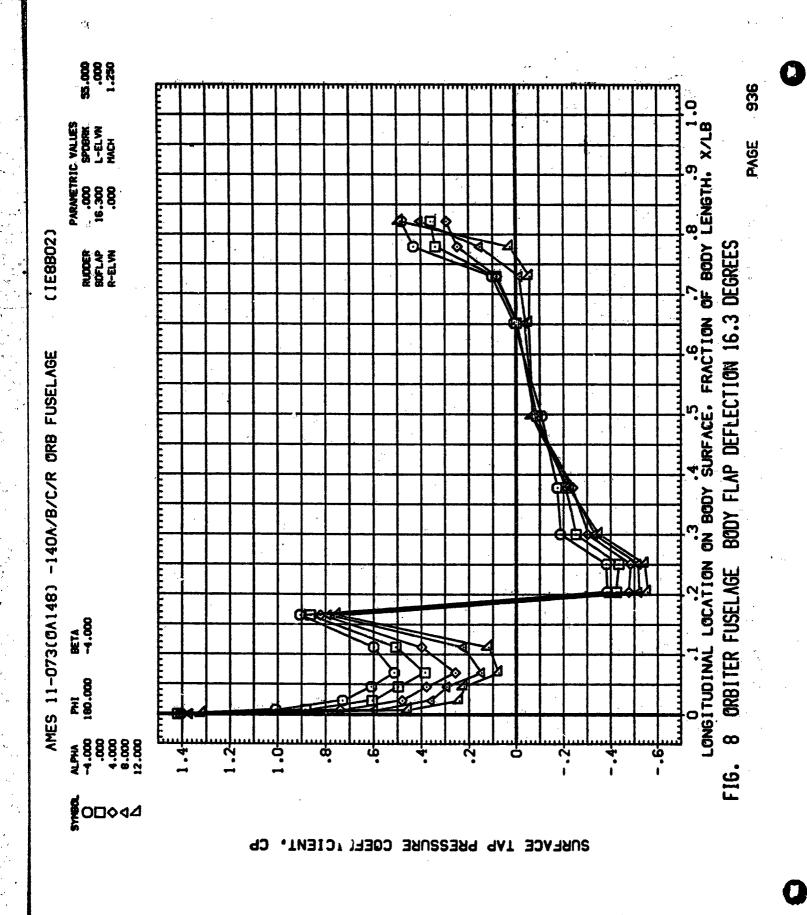
8 ORBITER FUSELAGE BODY FLAP DEFLECTION 16.3 DEGREES PARAFETRIC VALLES
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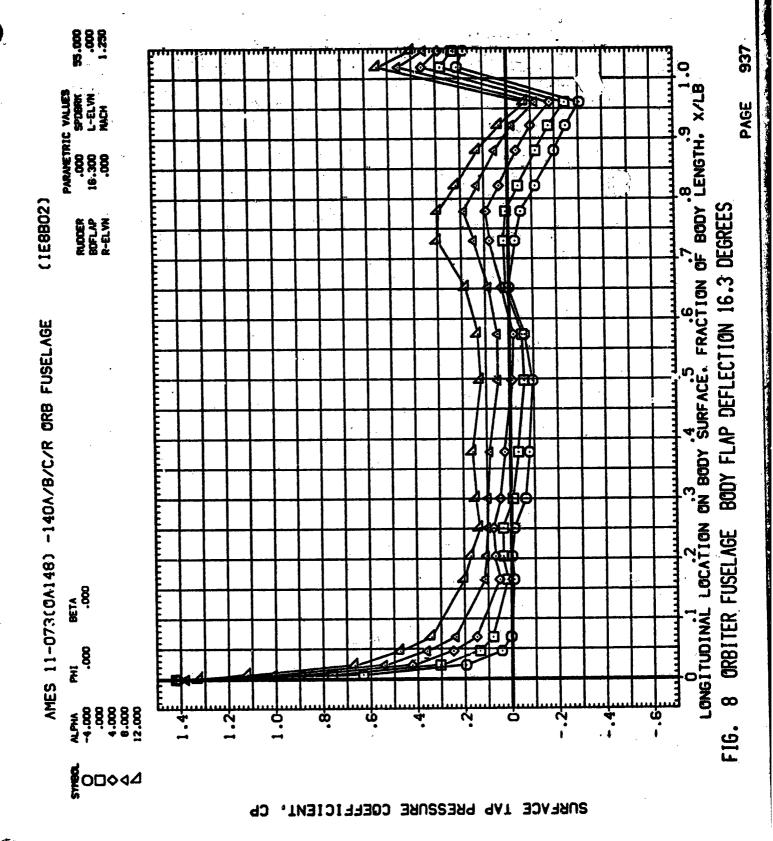


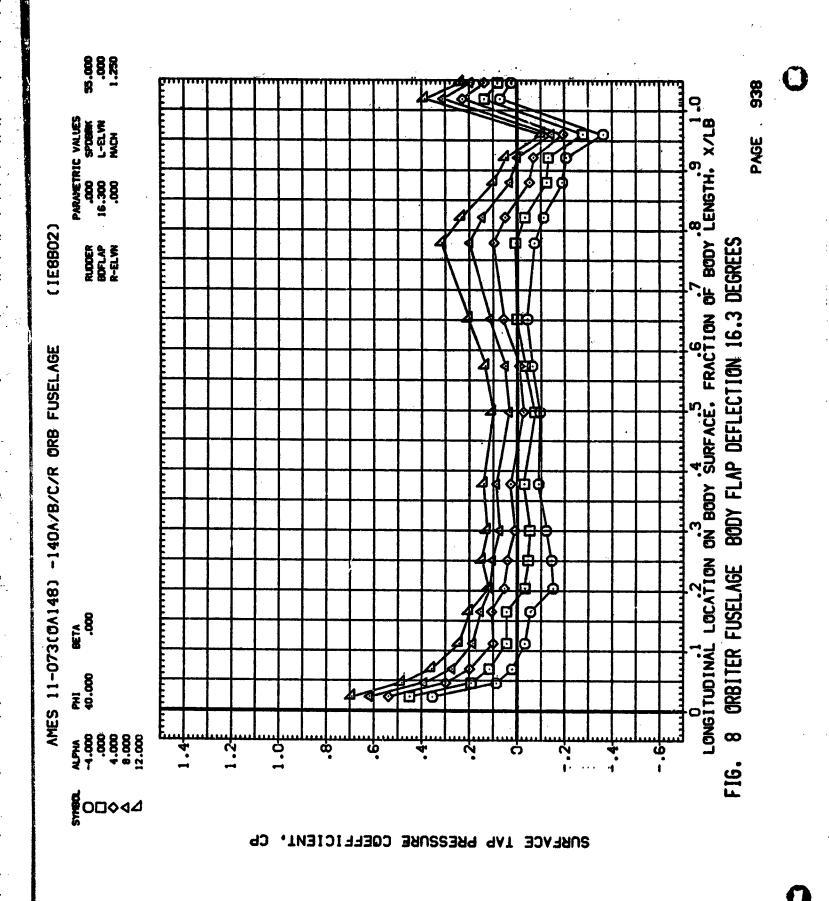
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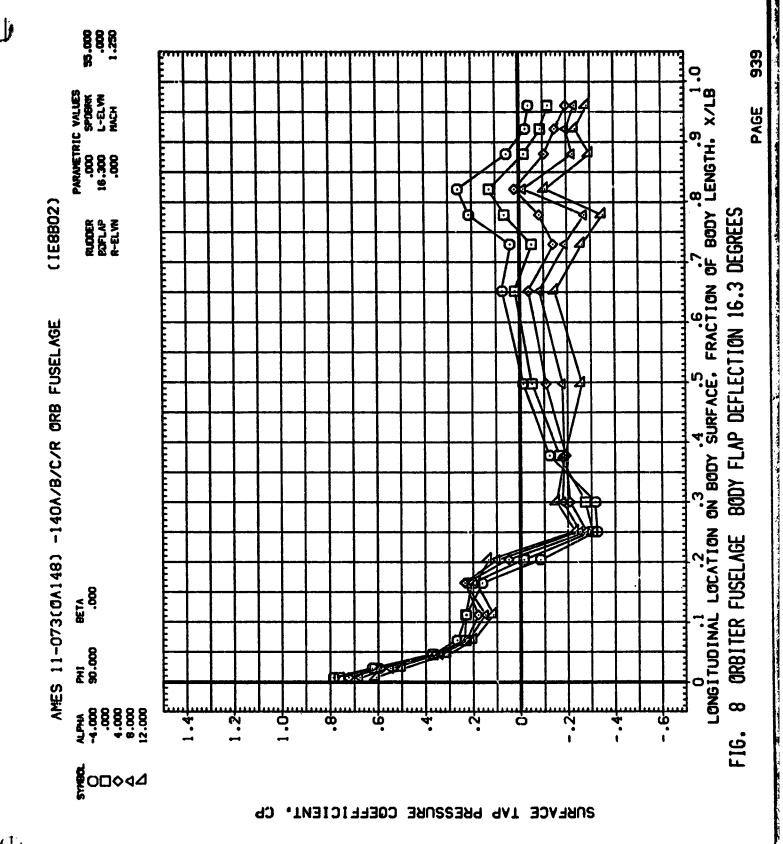


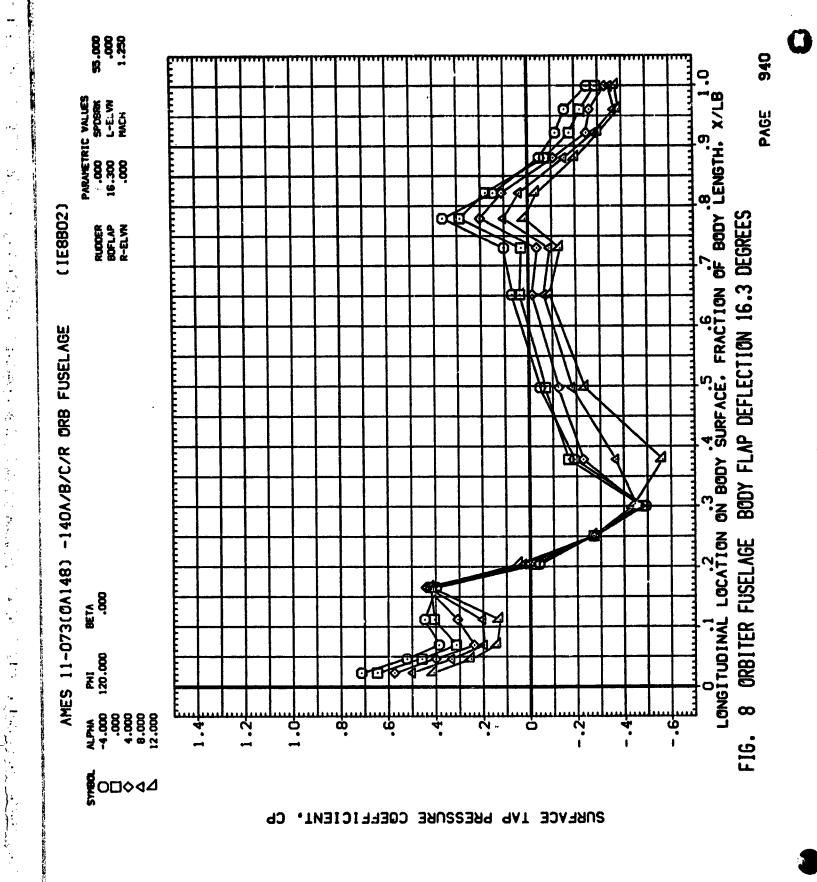






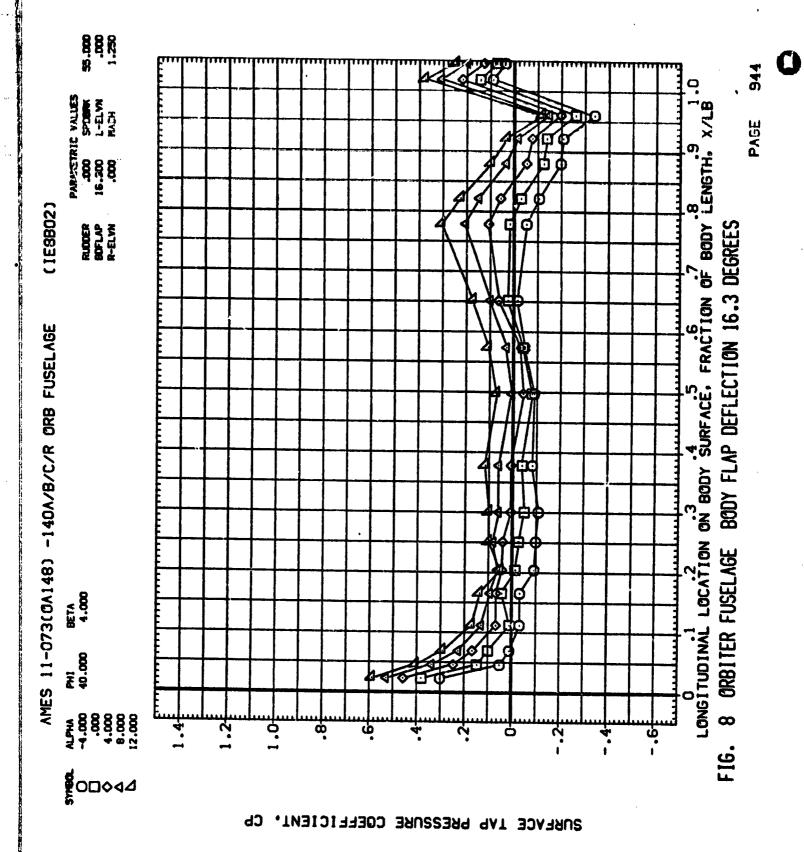






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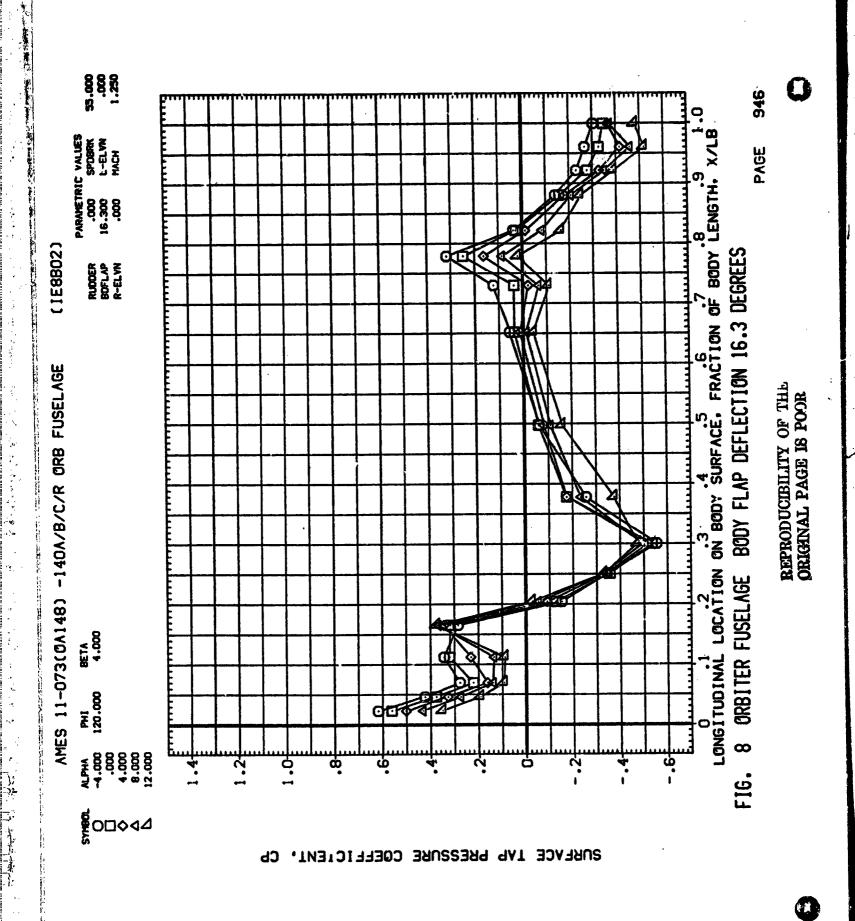
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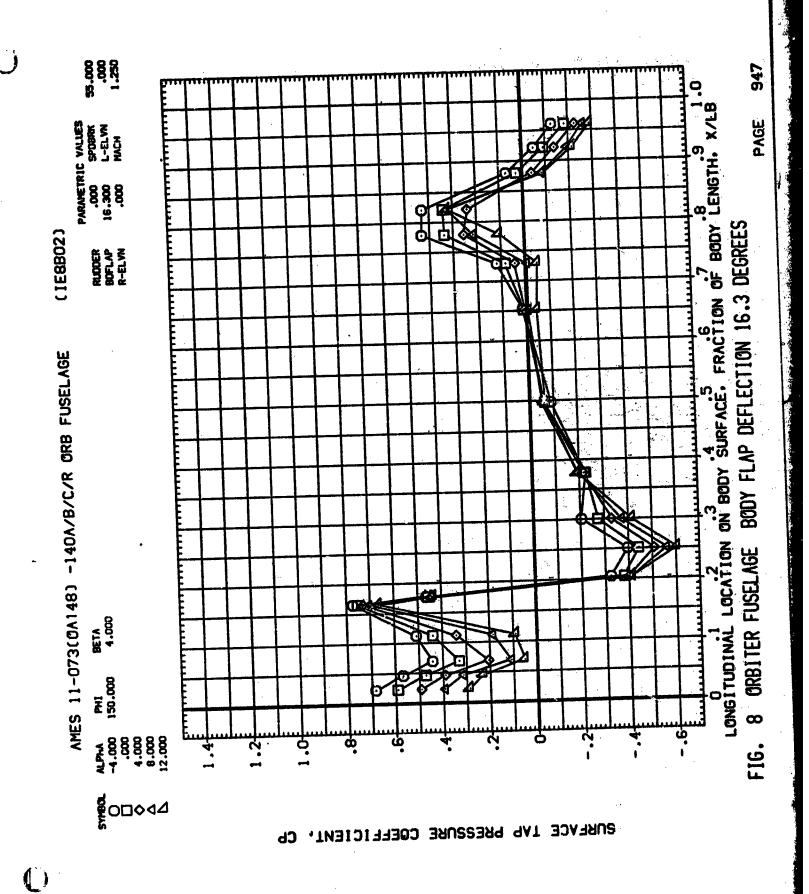
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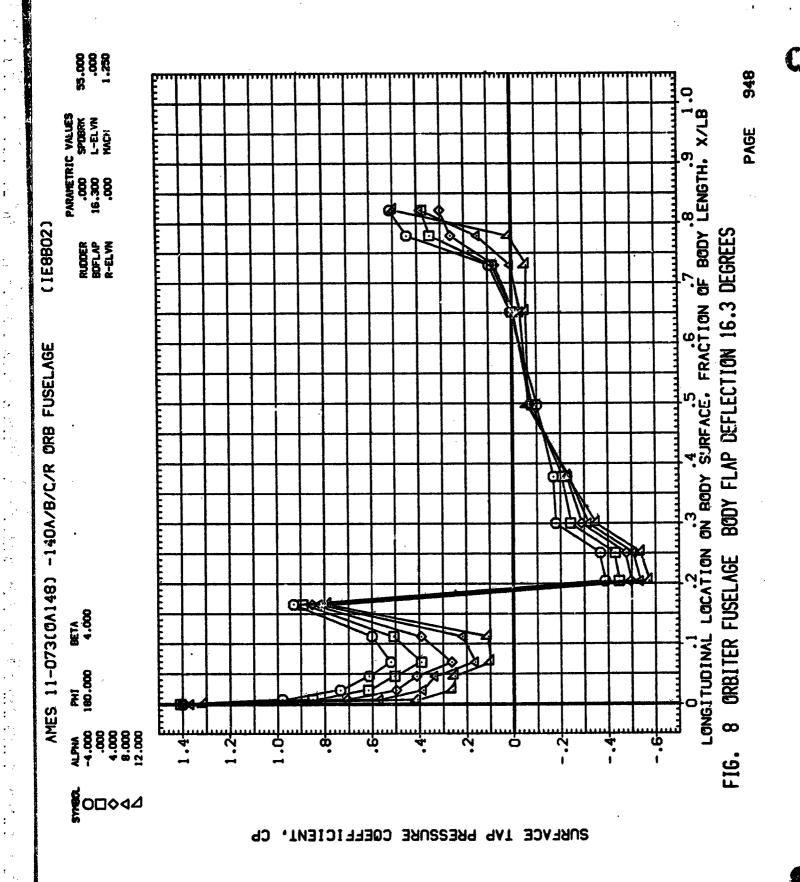
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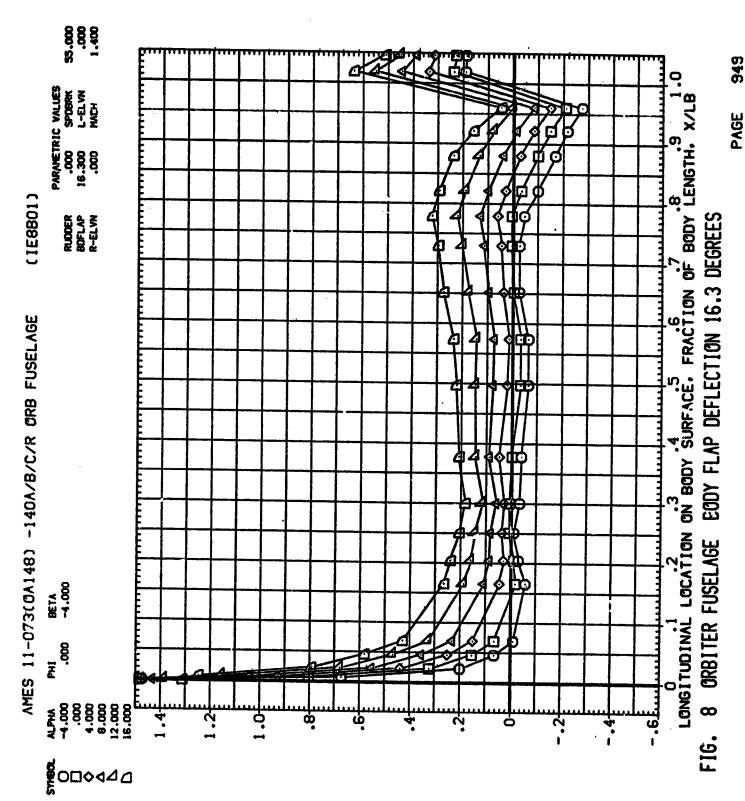
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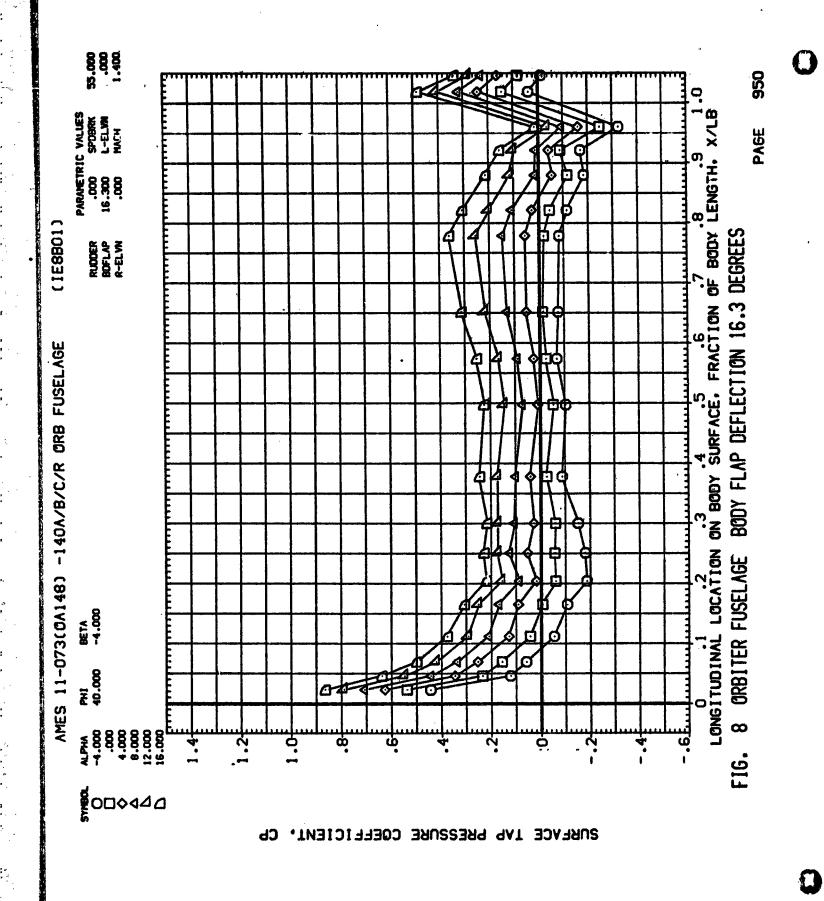




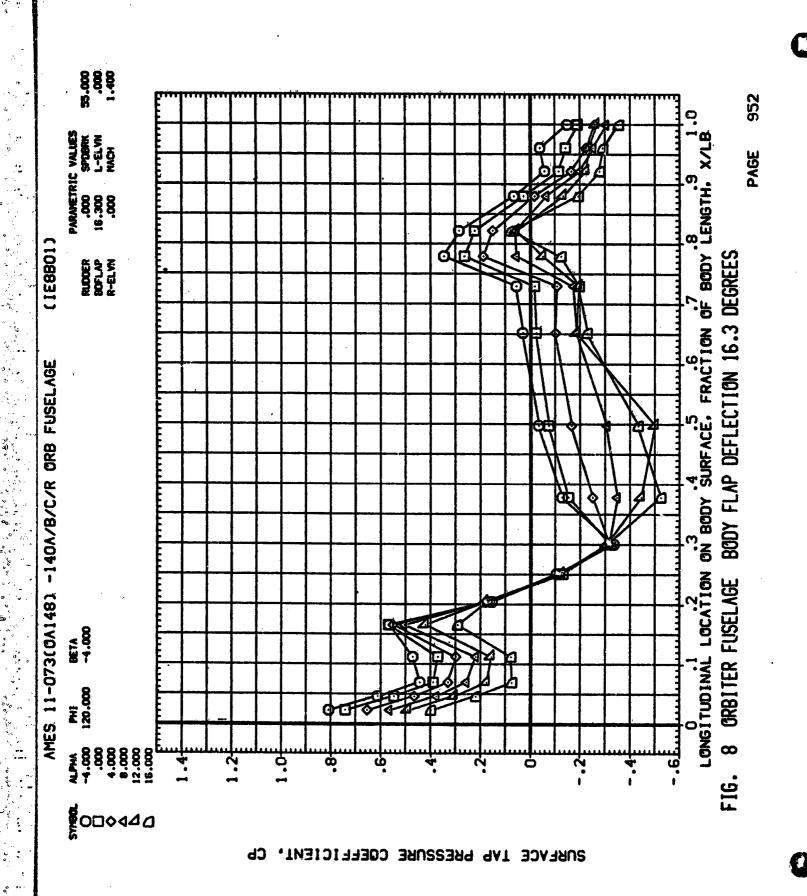


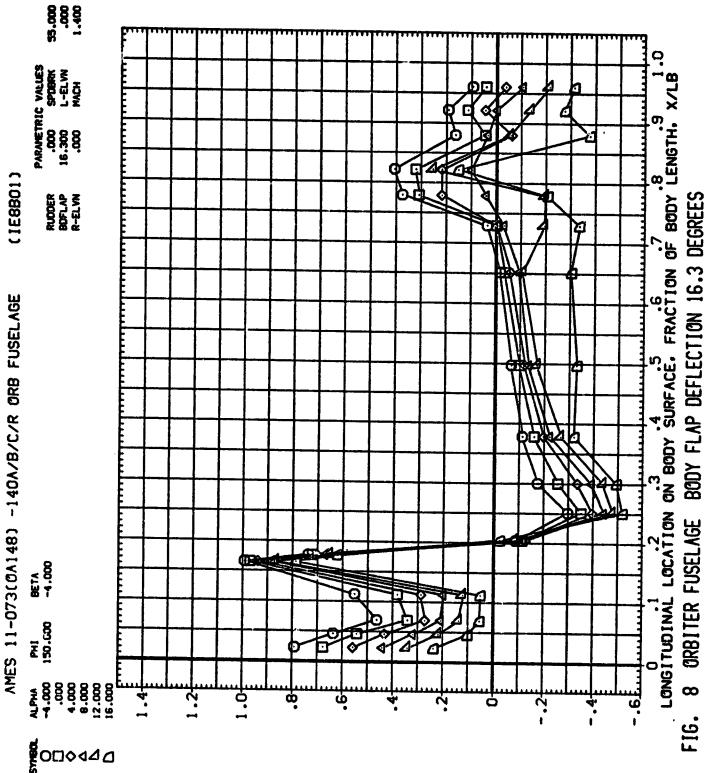


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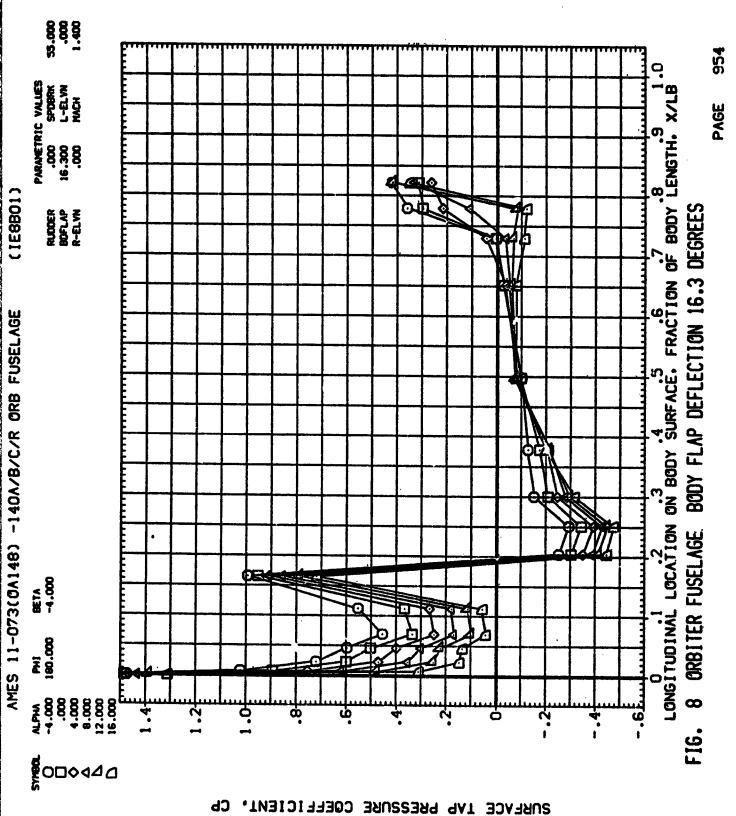


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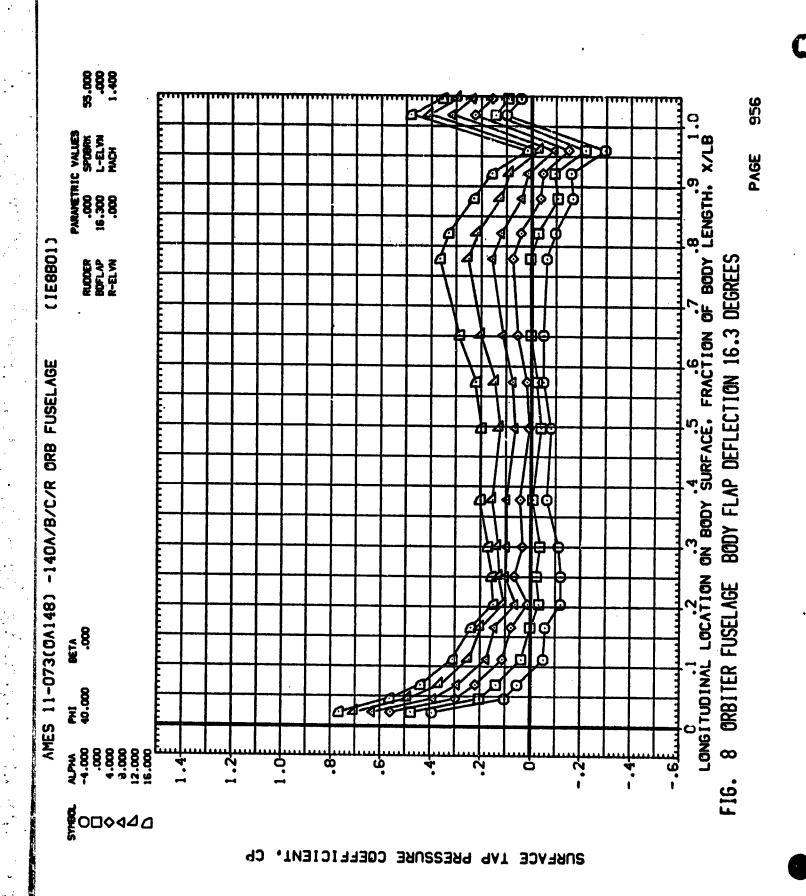
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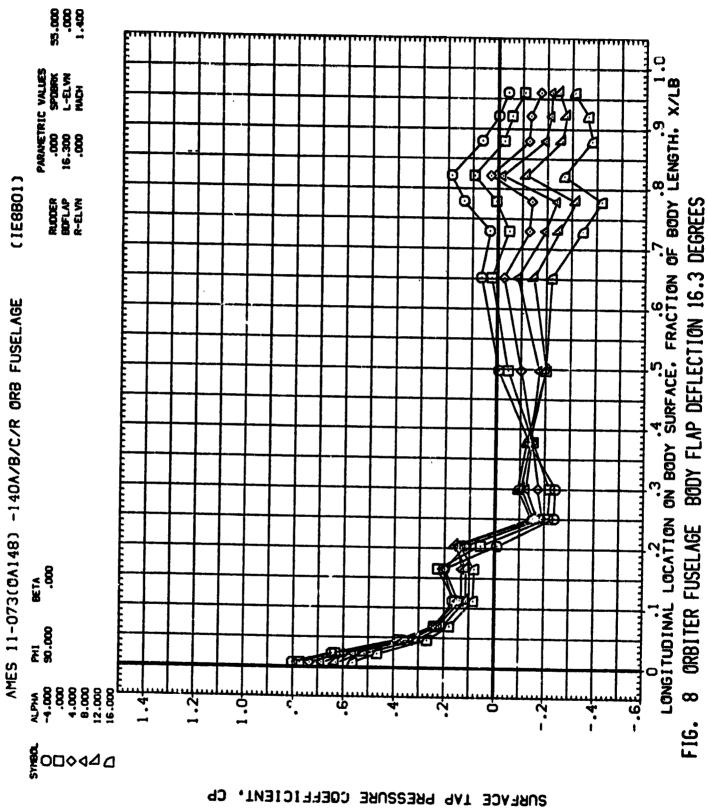
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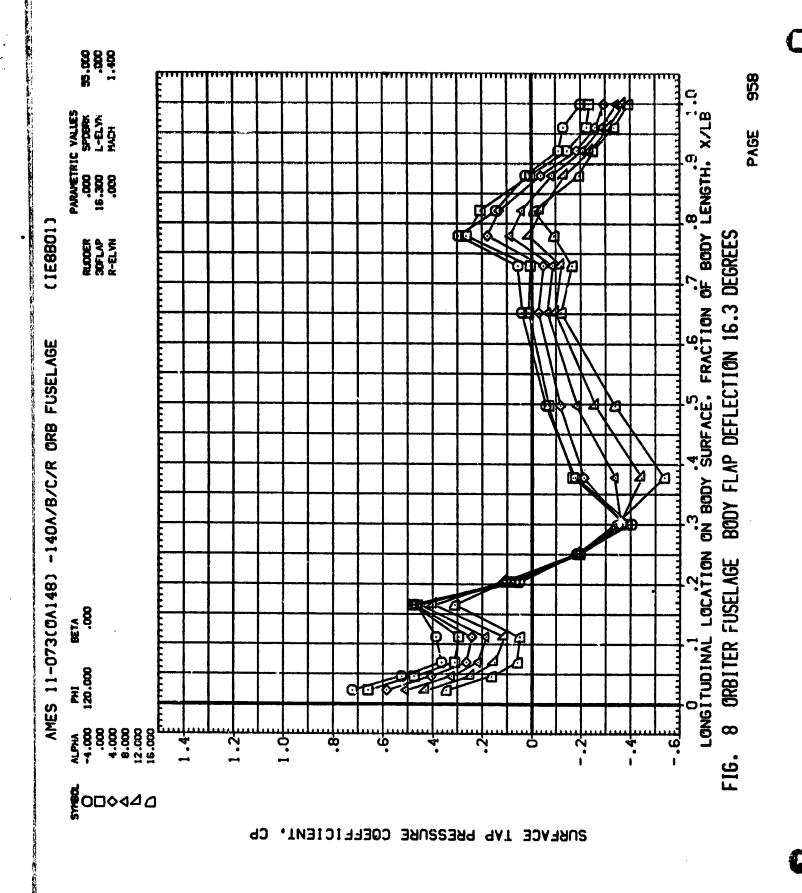
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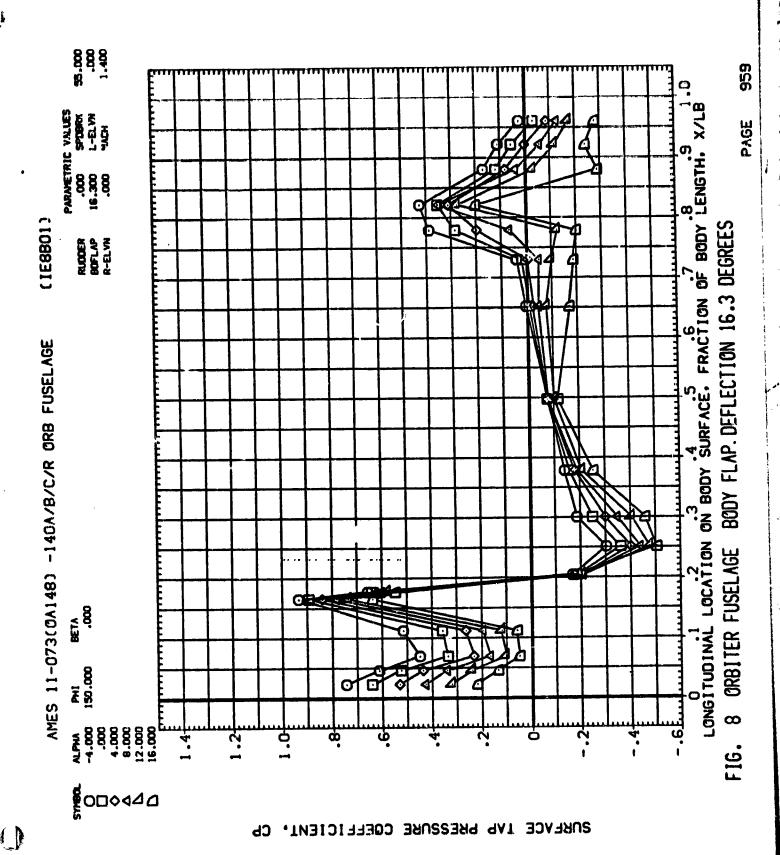
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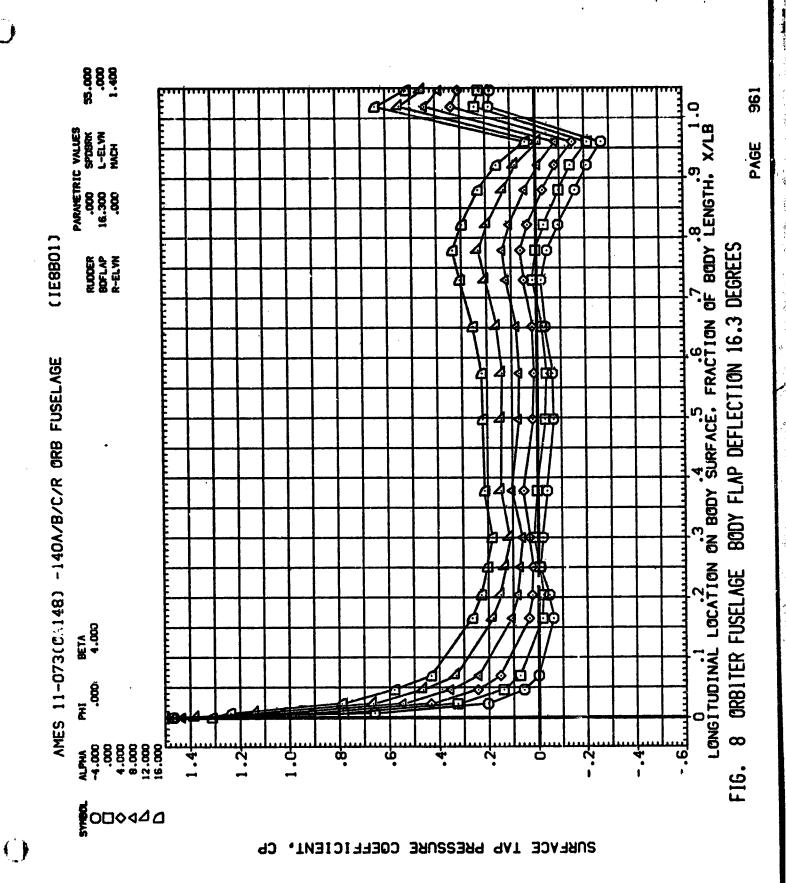
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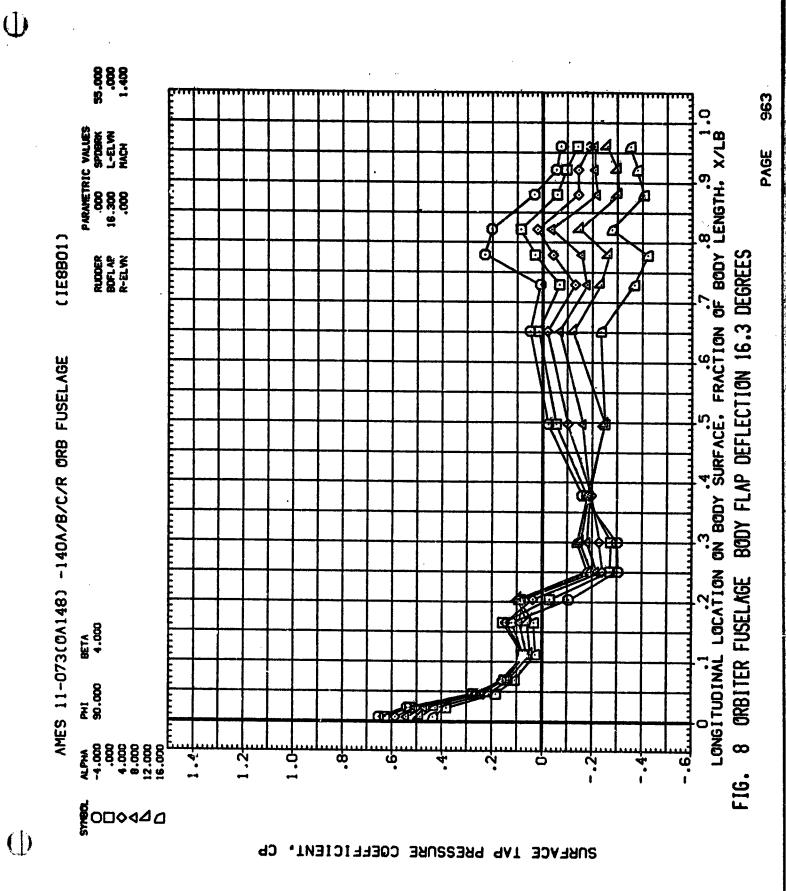


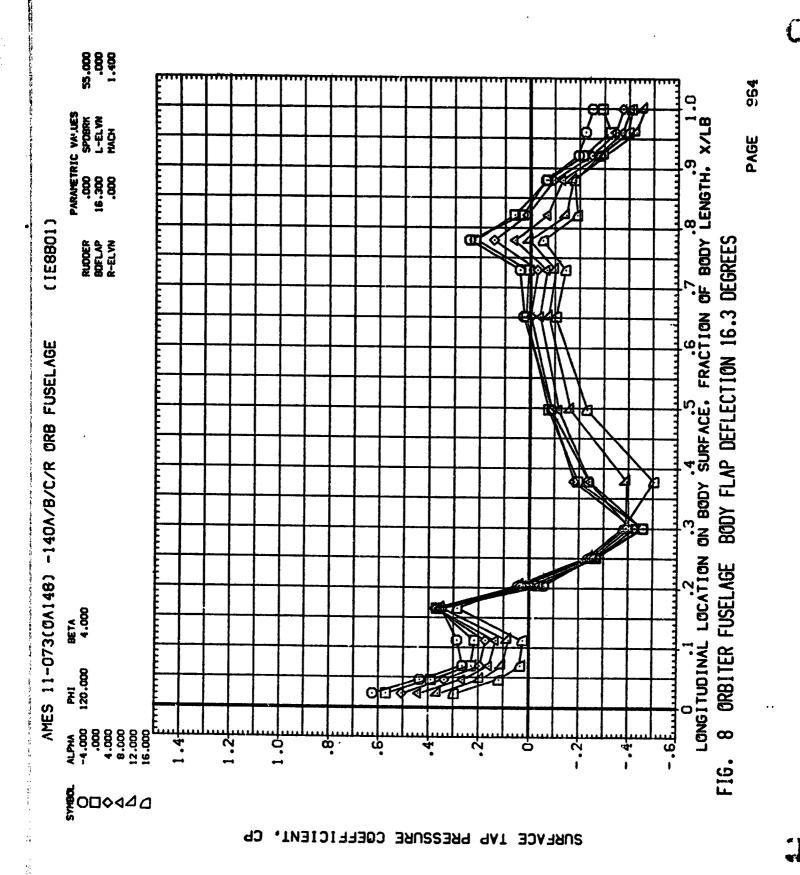
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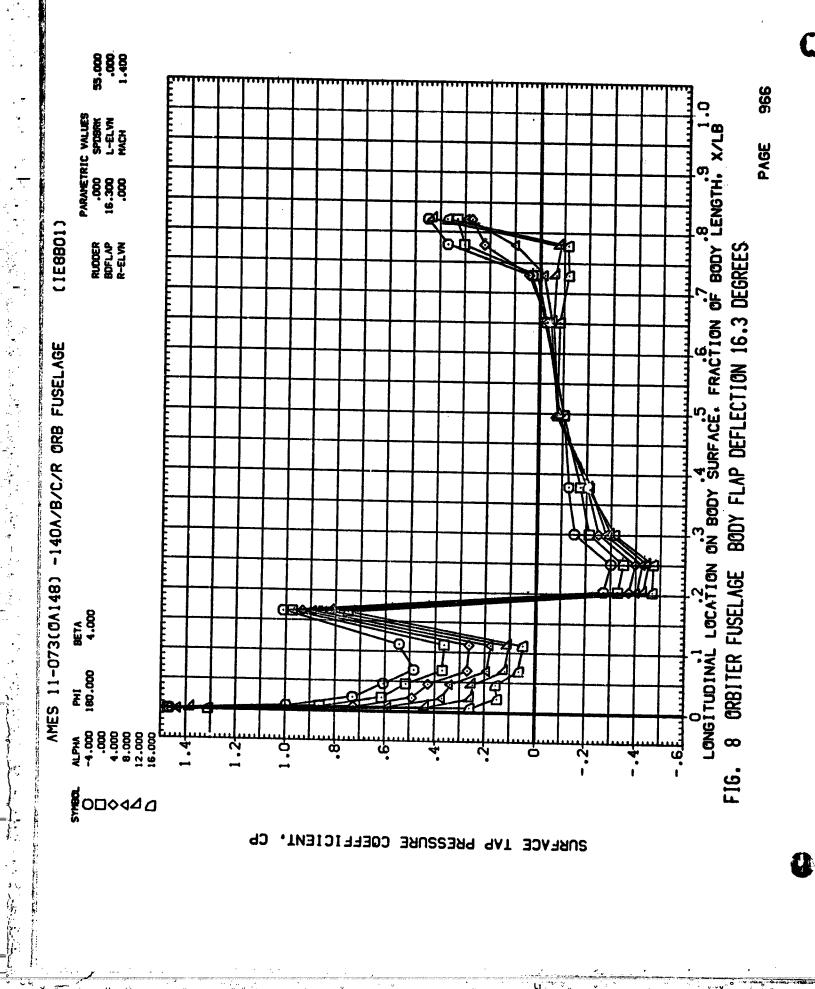
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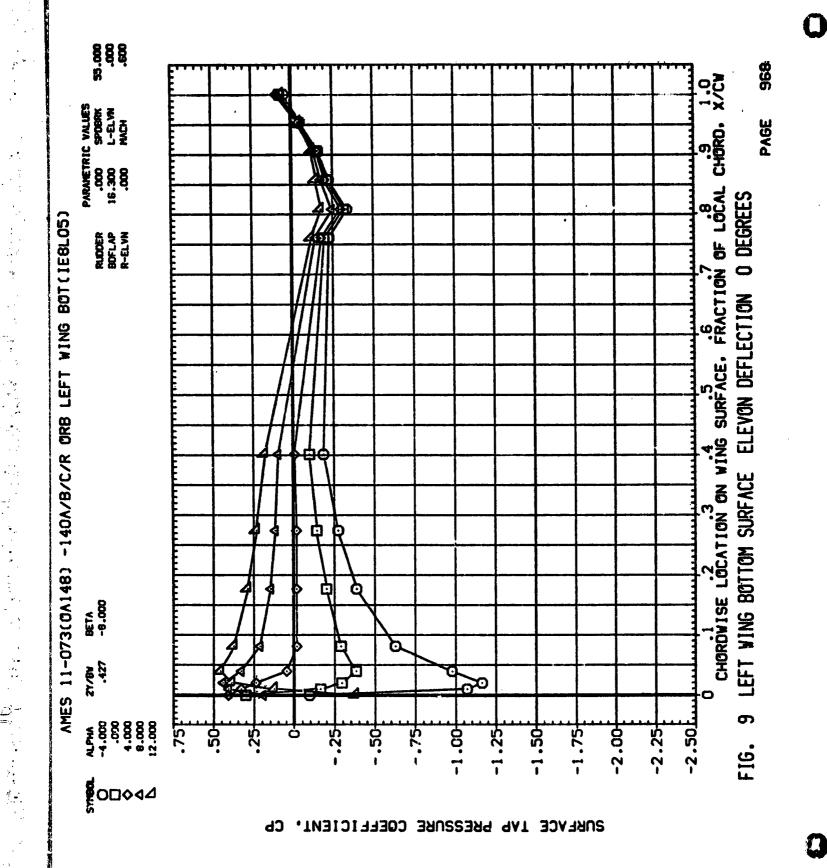
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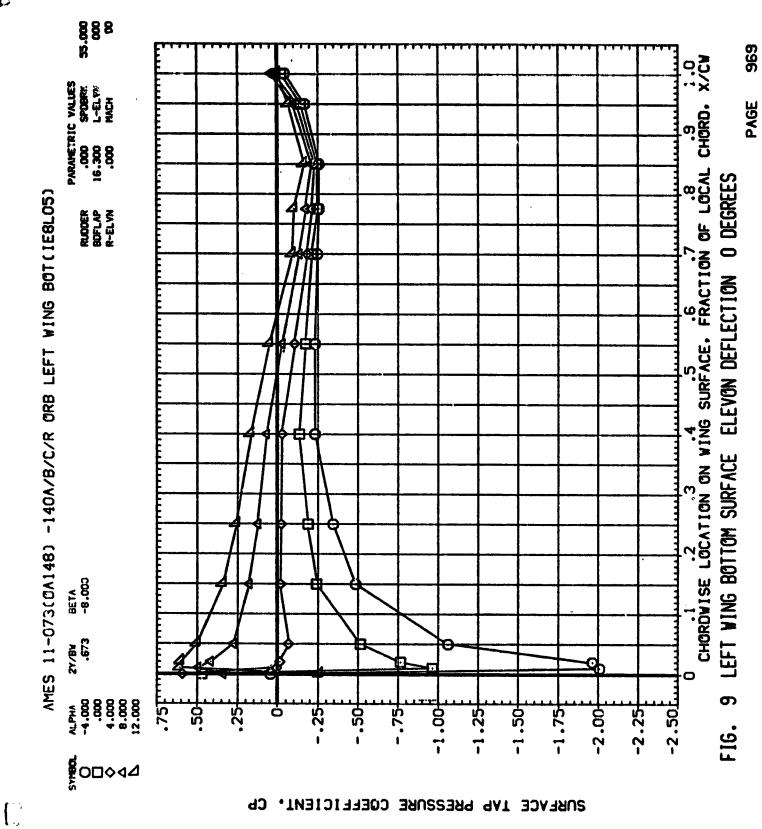
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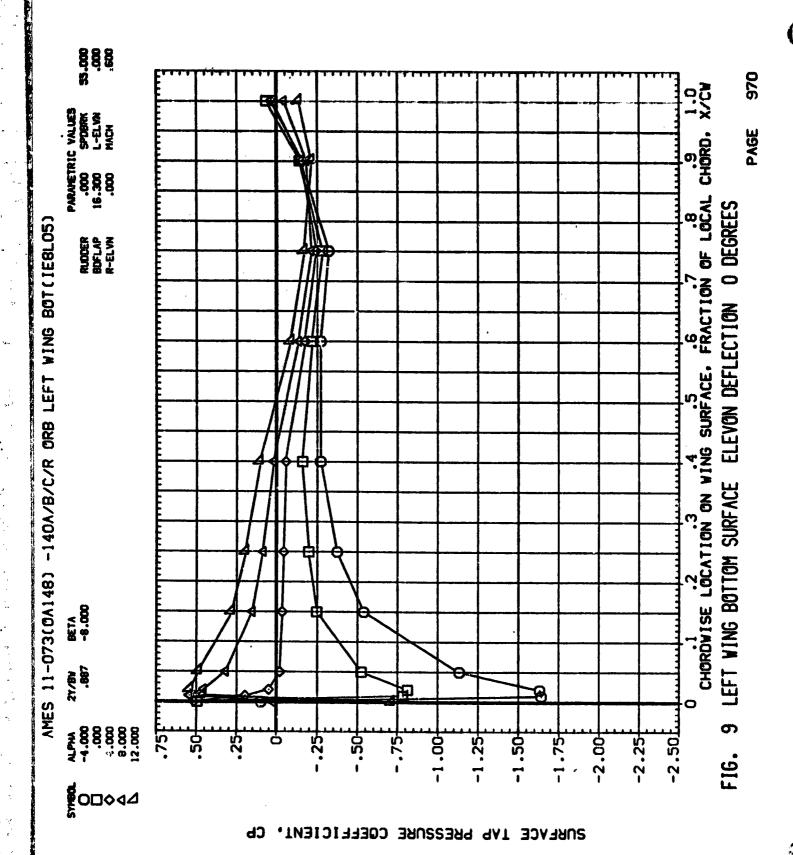
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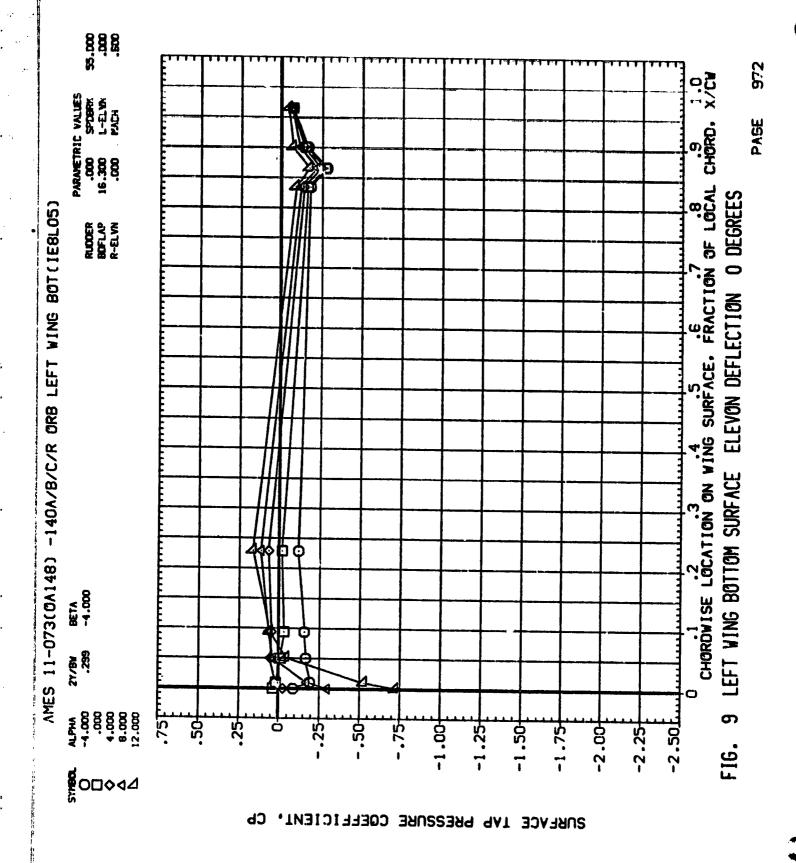


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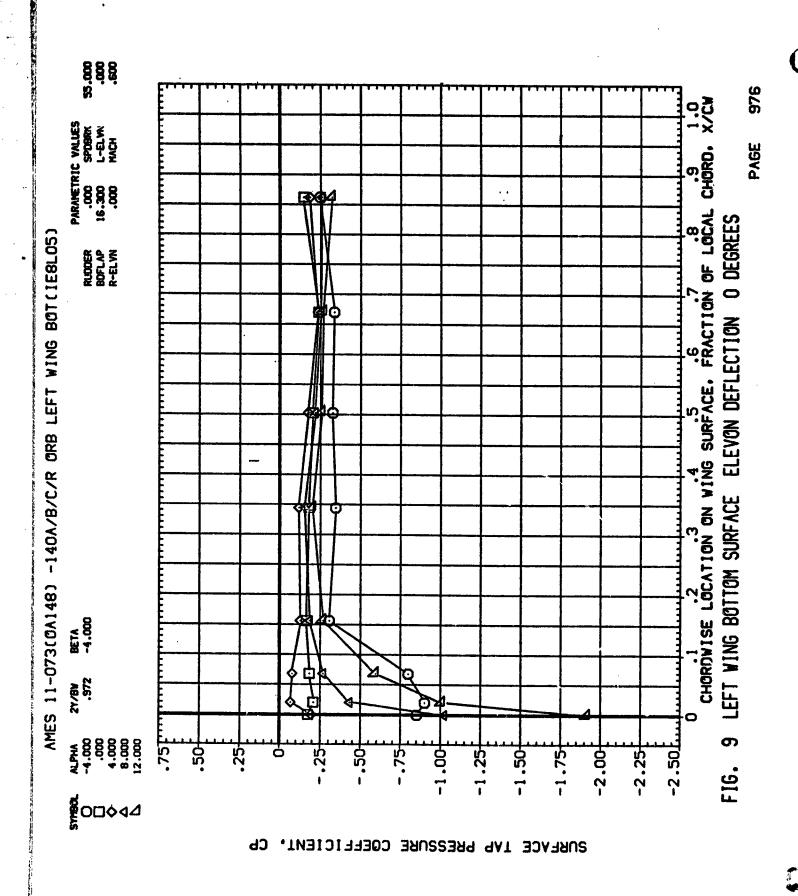


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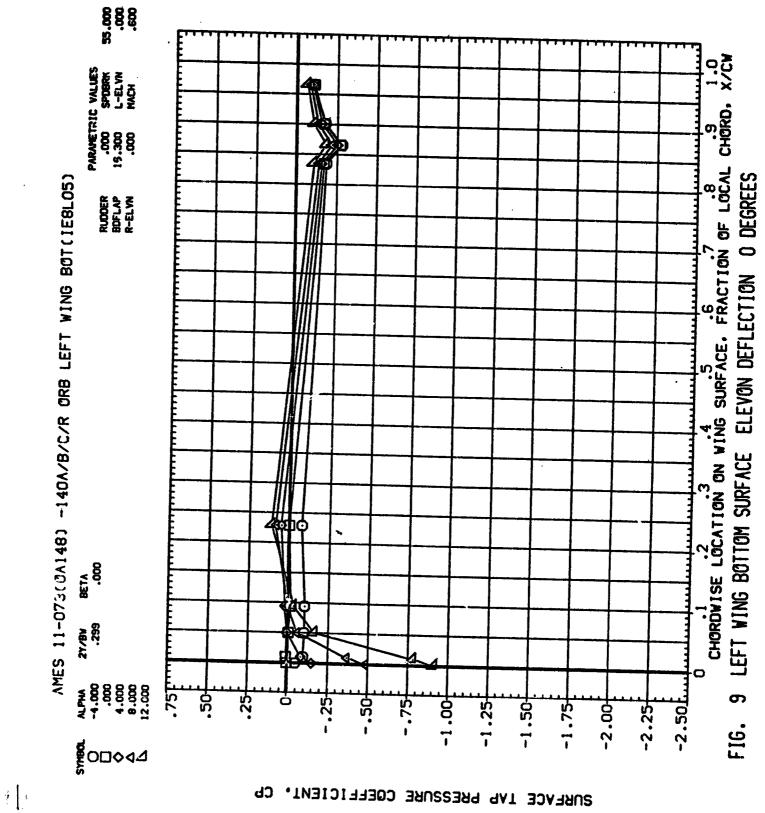
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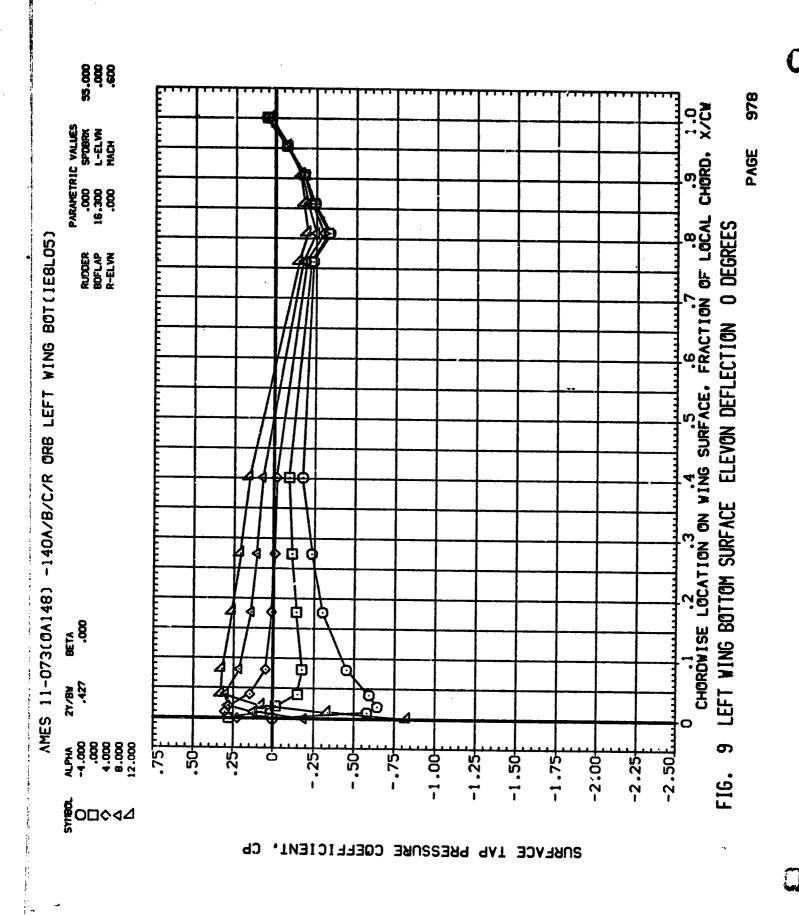
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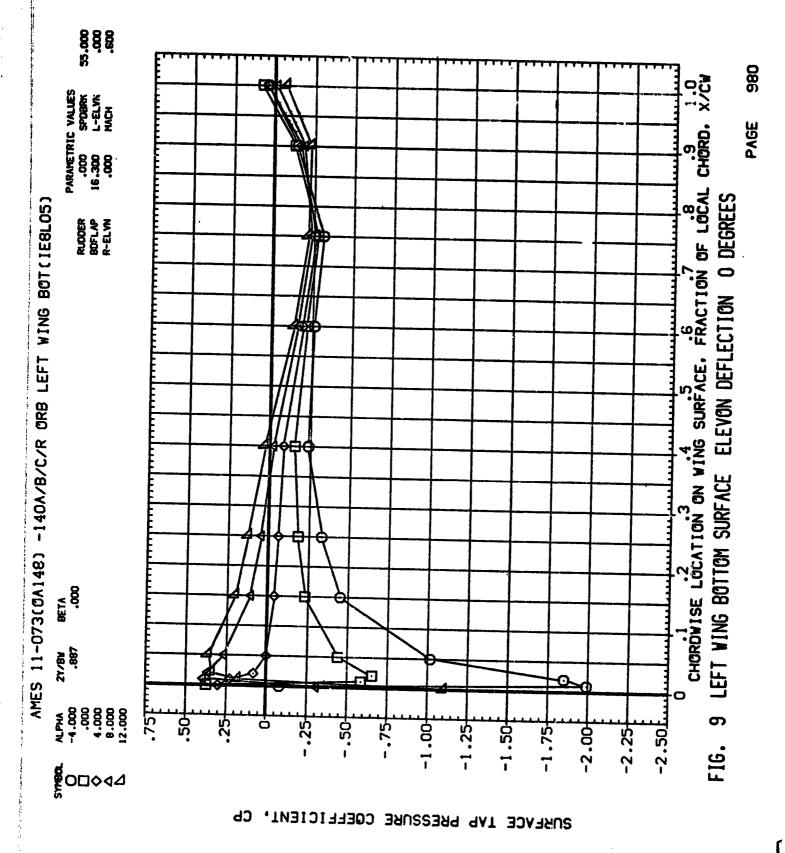
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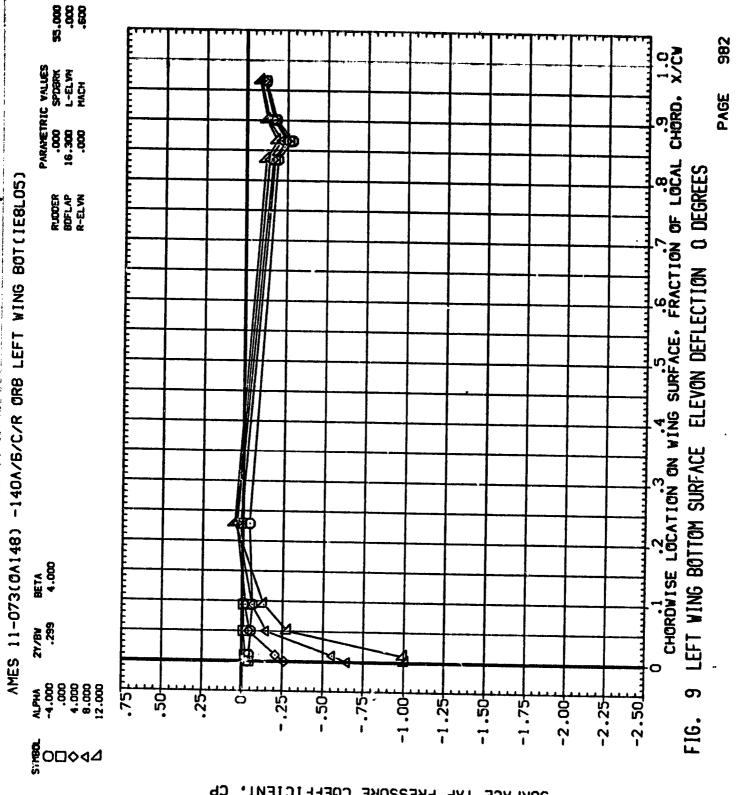
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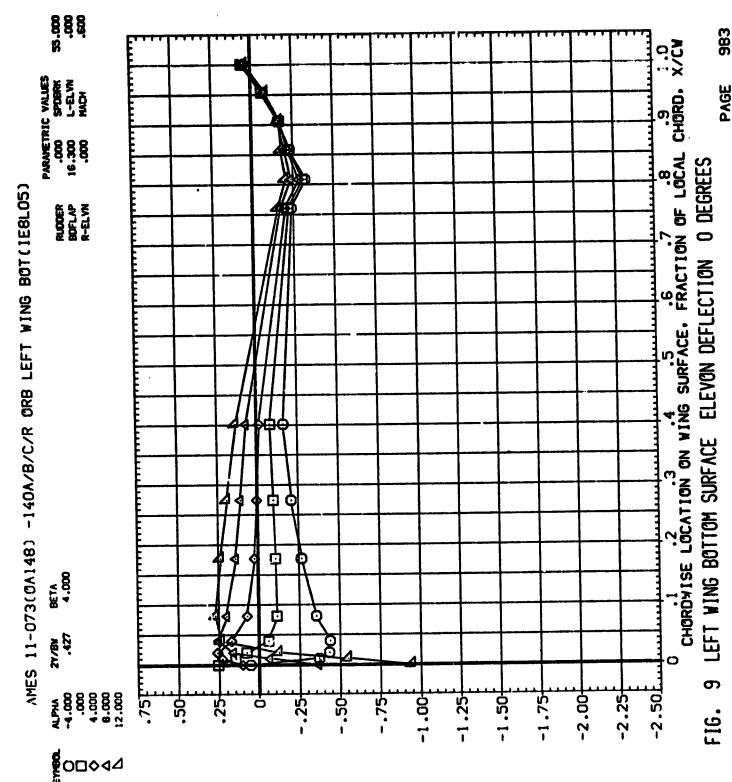


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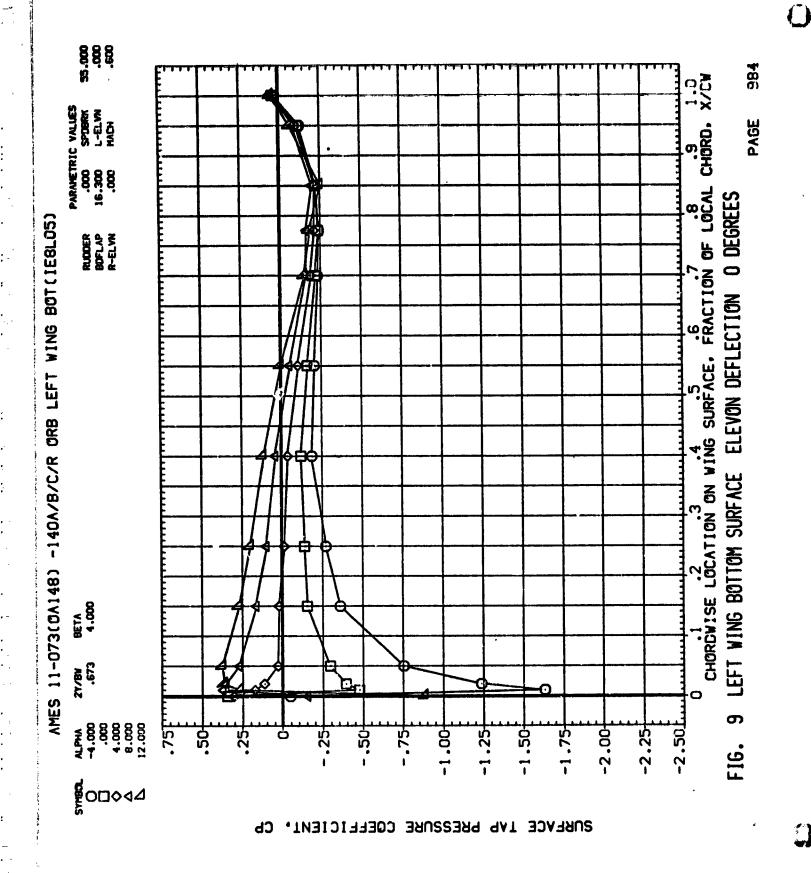


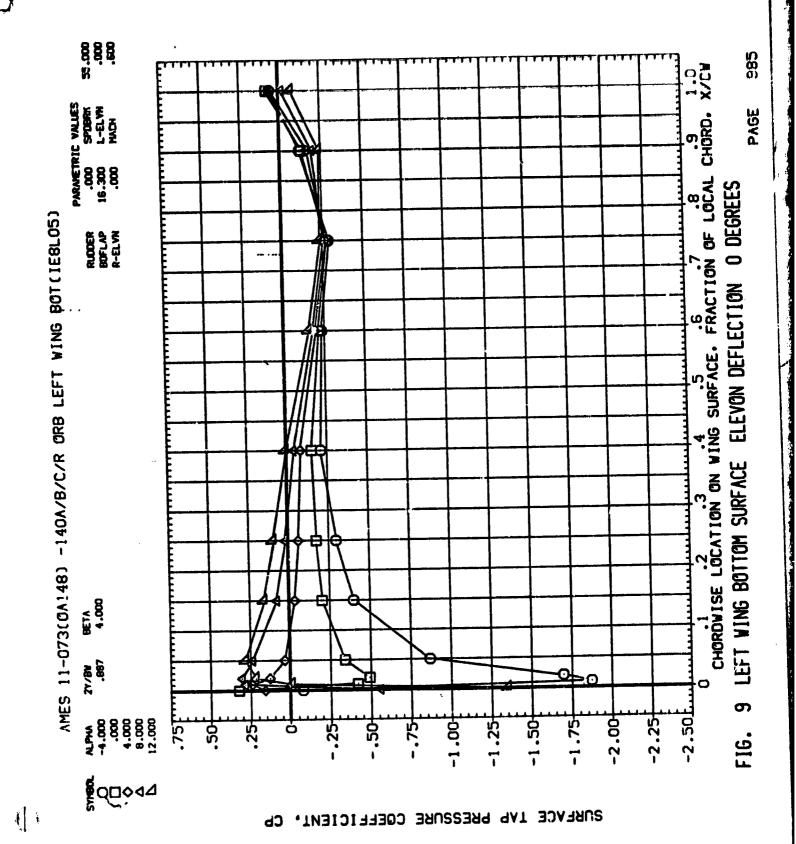
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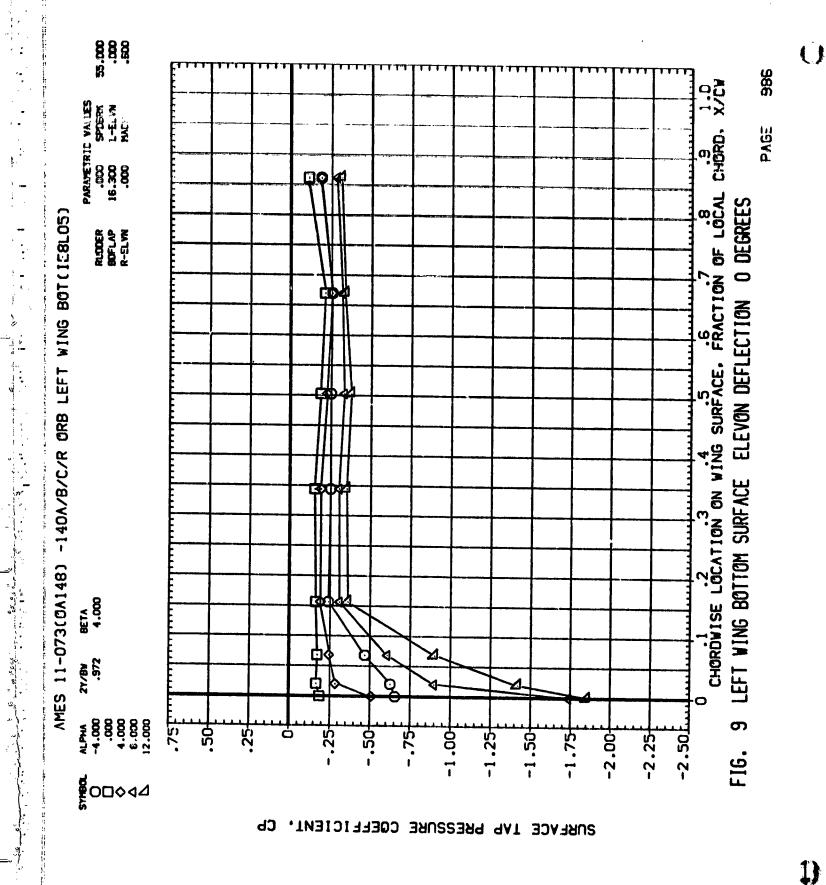


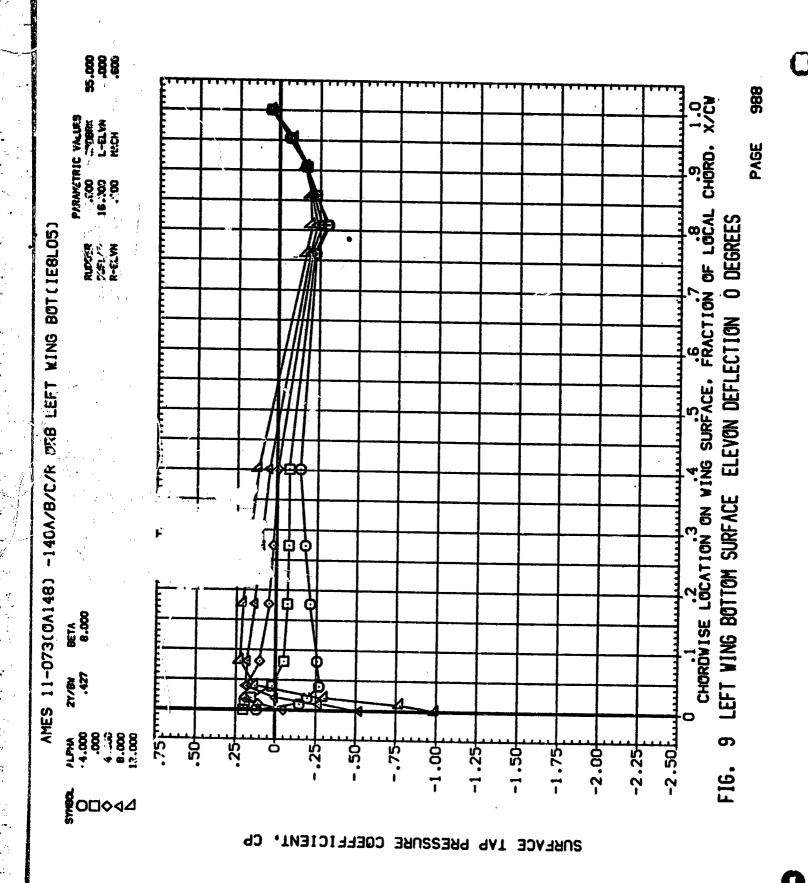
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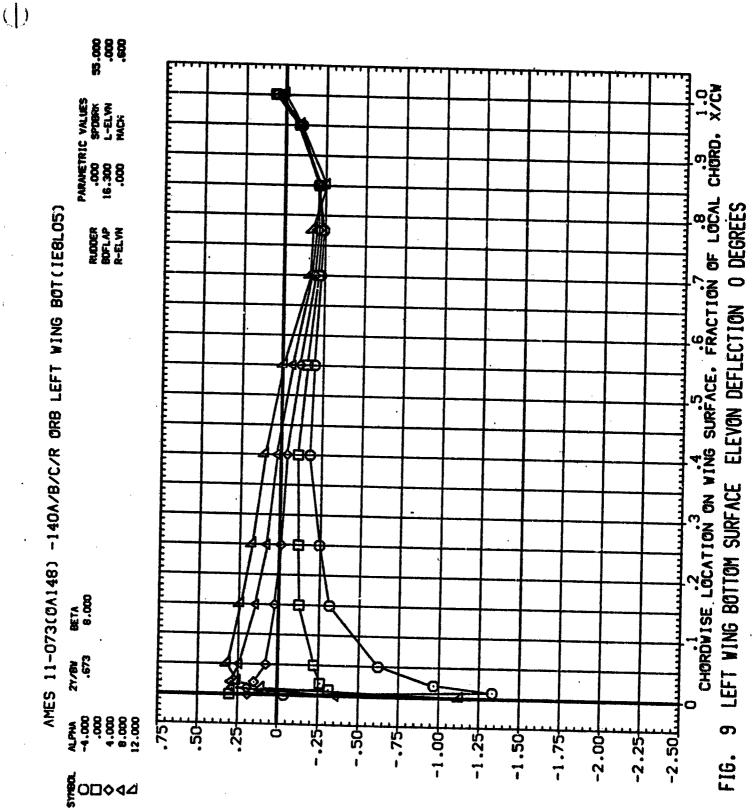
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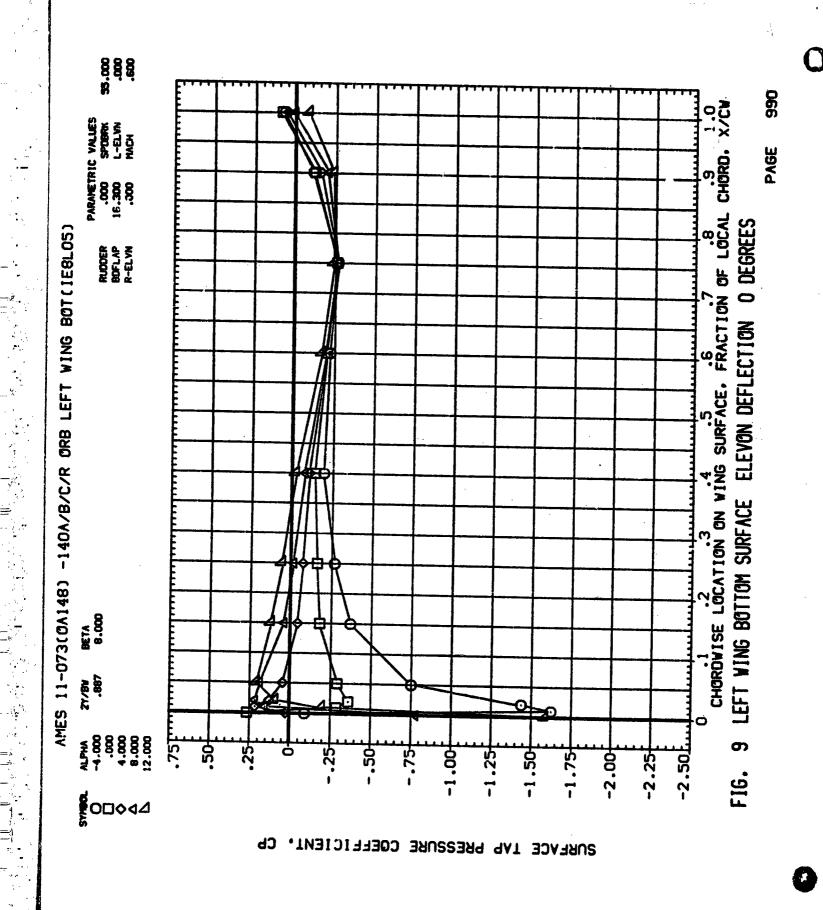


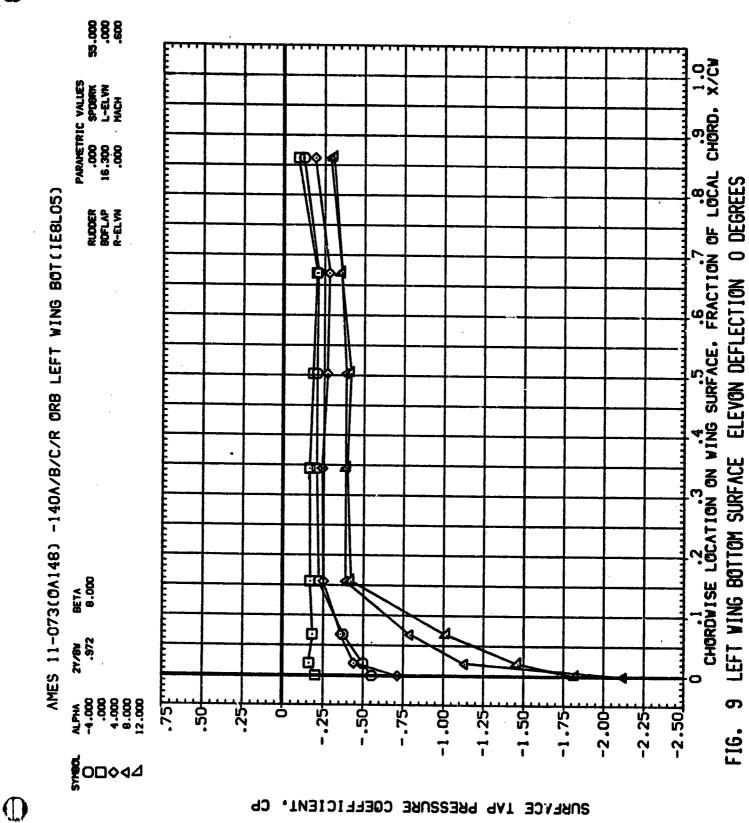


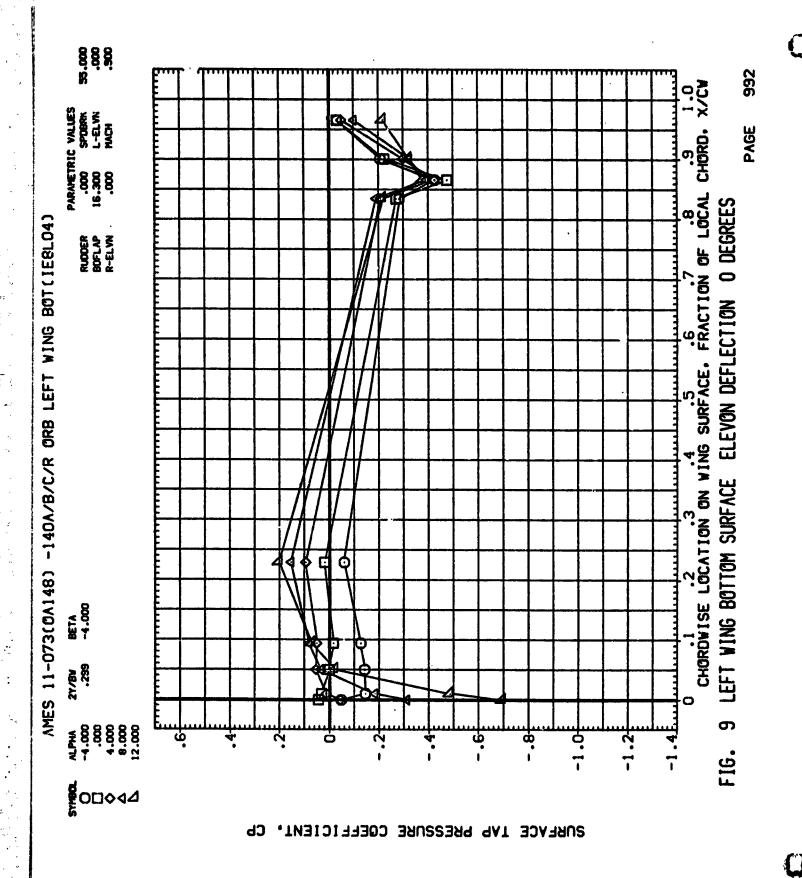












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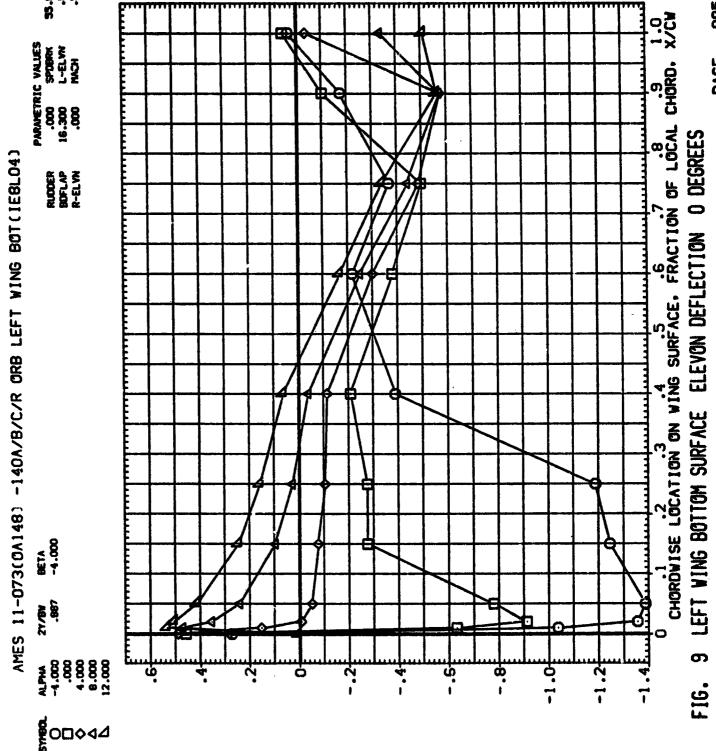
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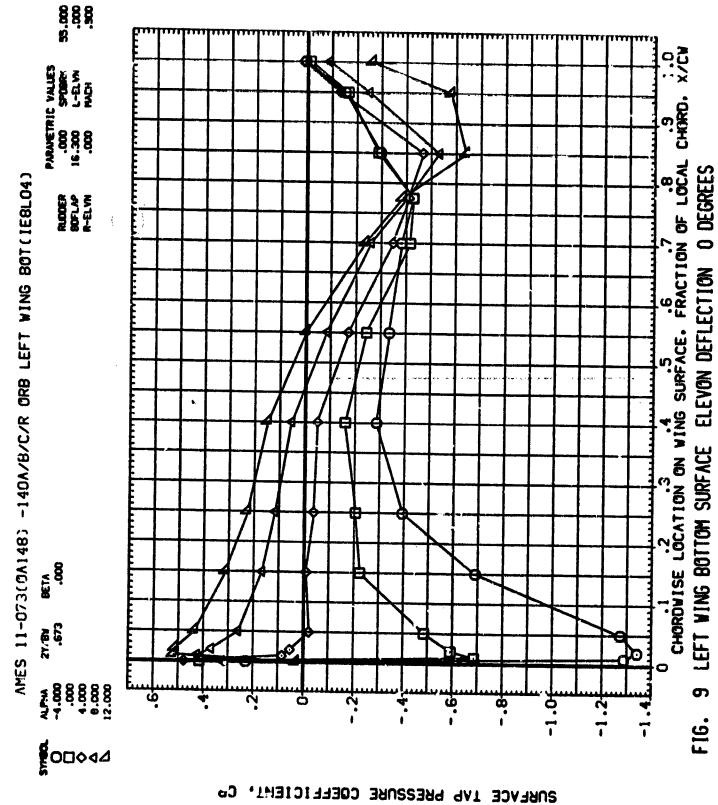
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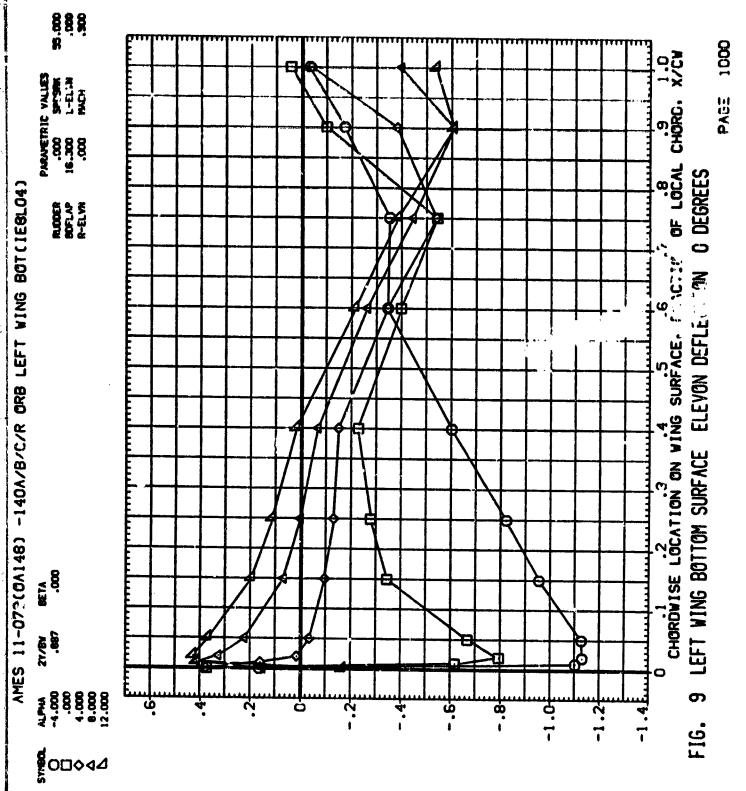
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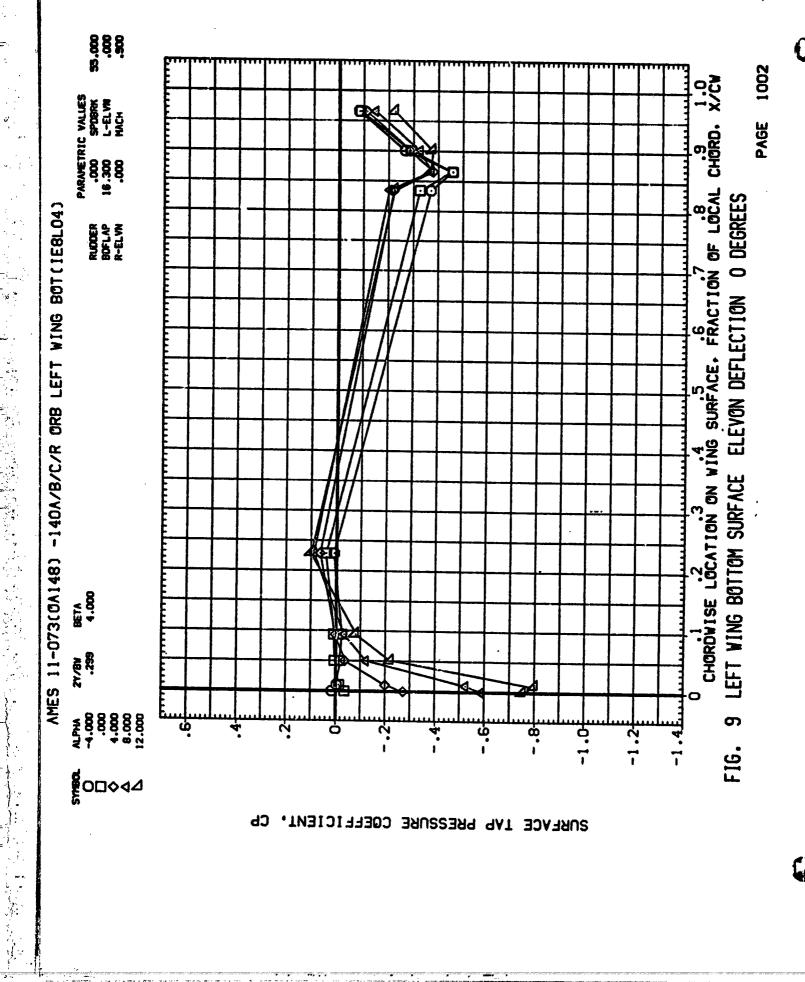


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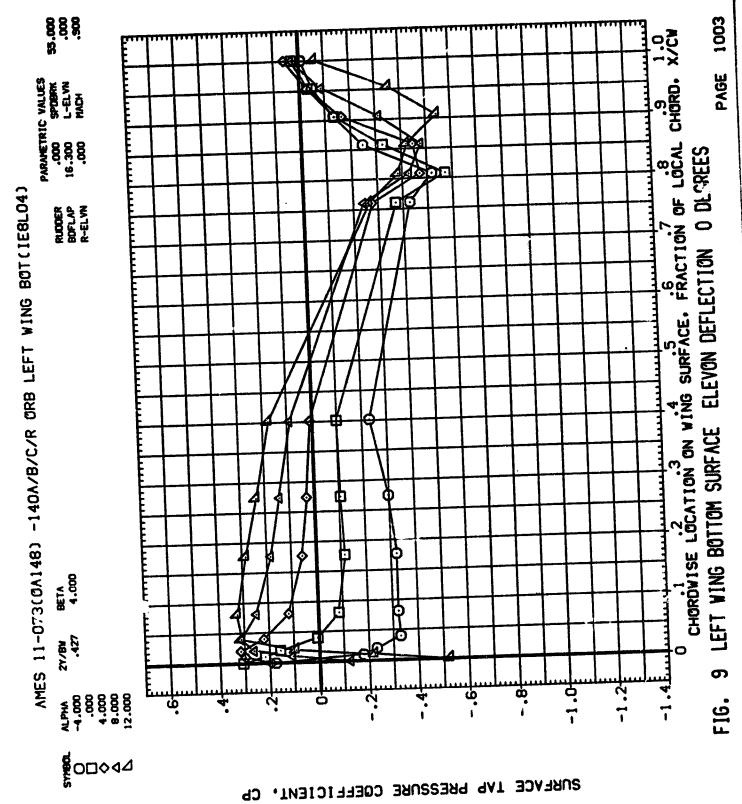
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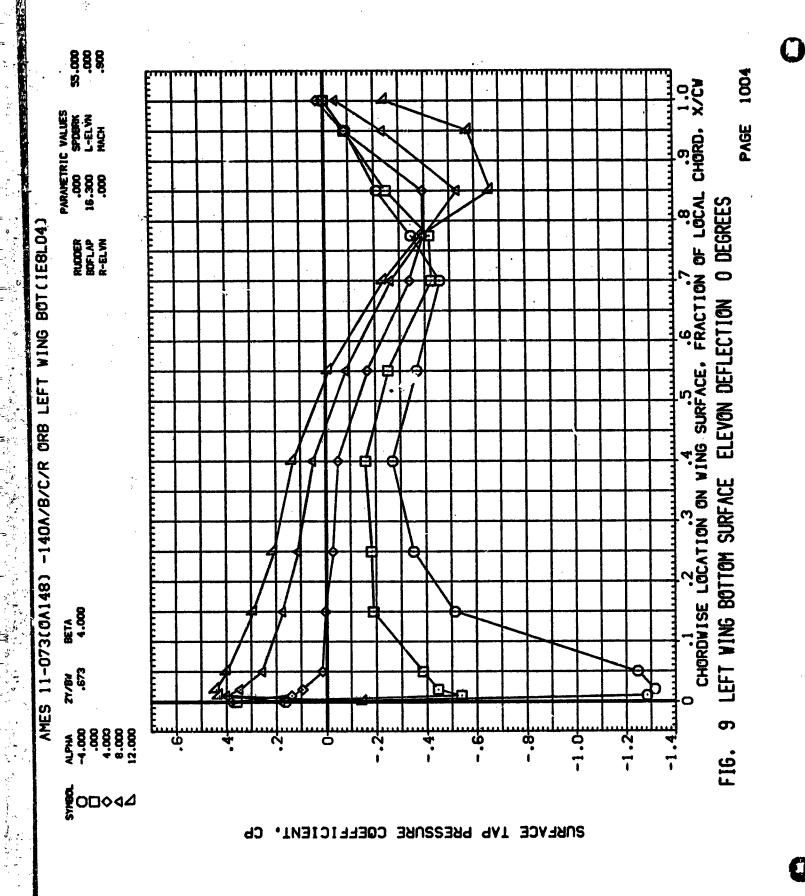
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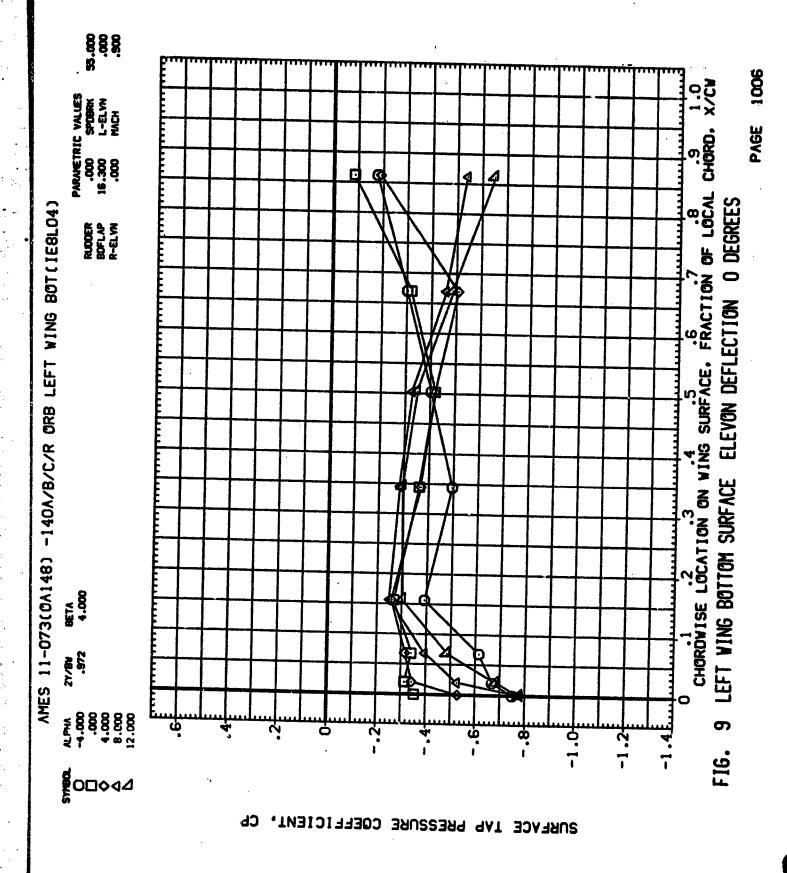


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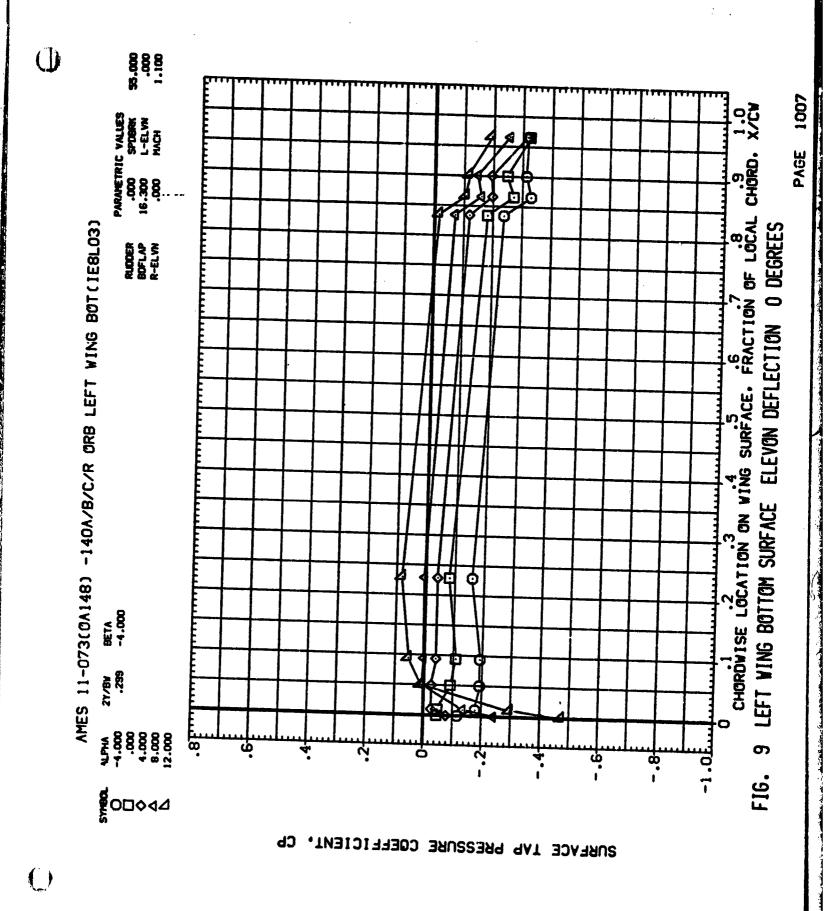
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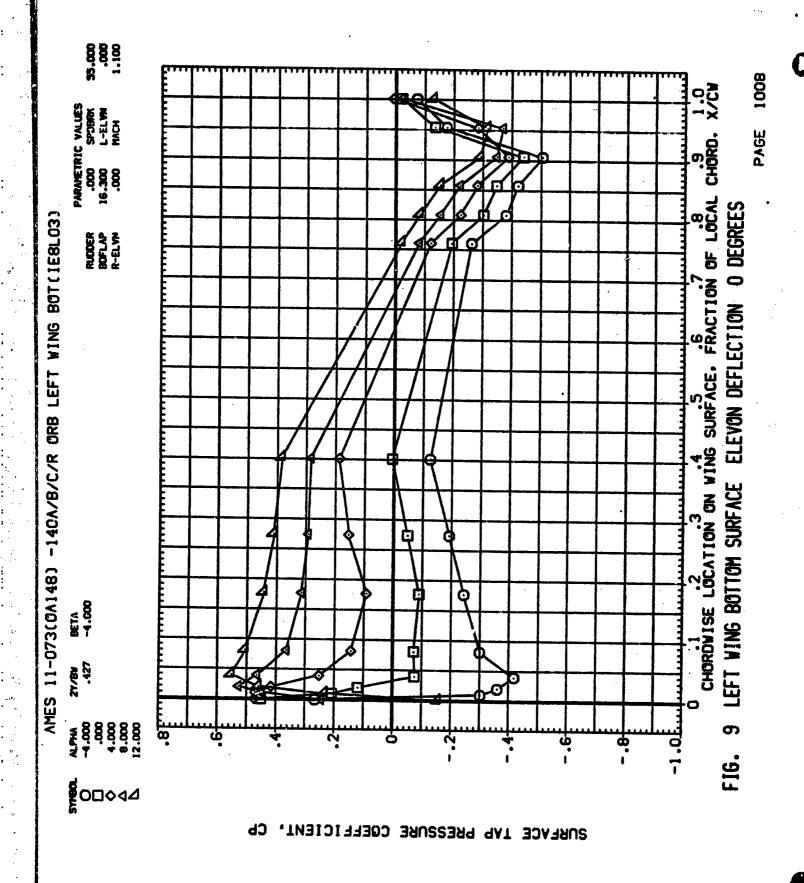
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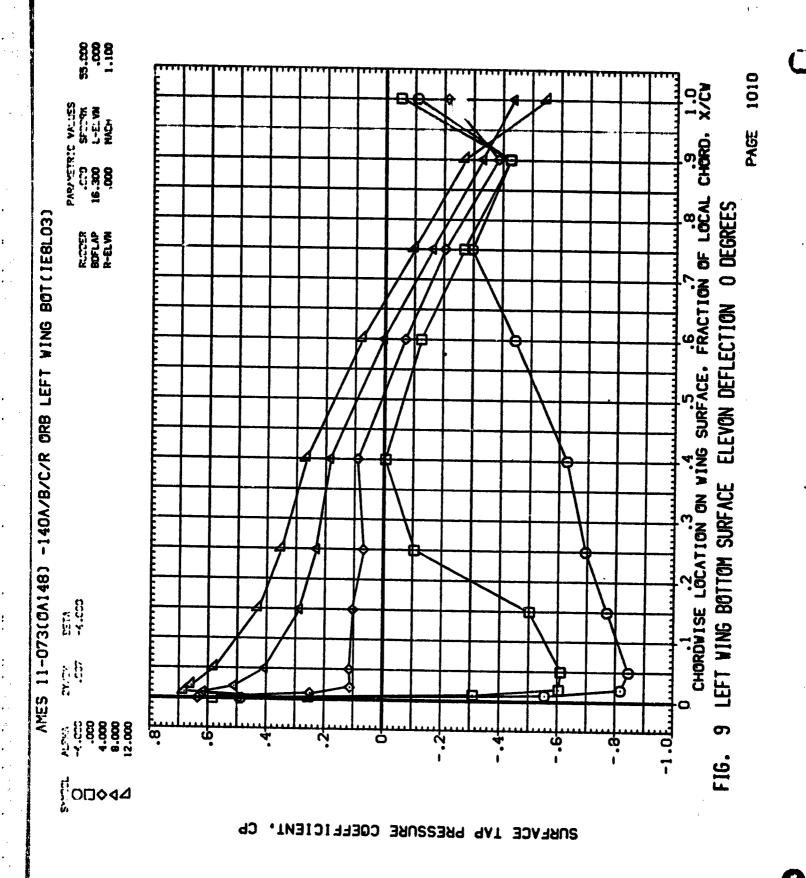


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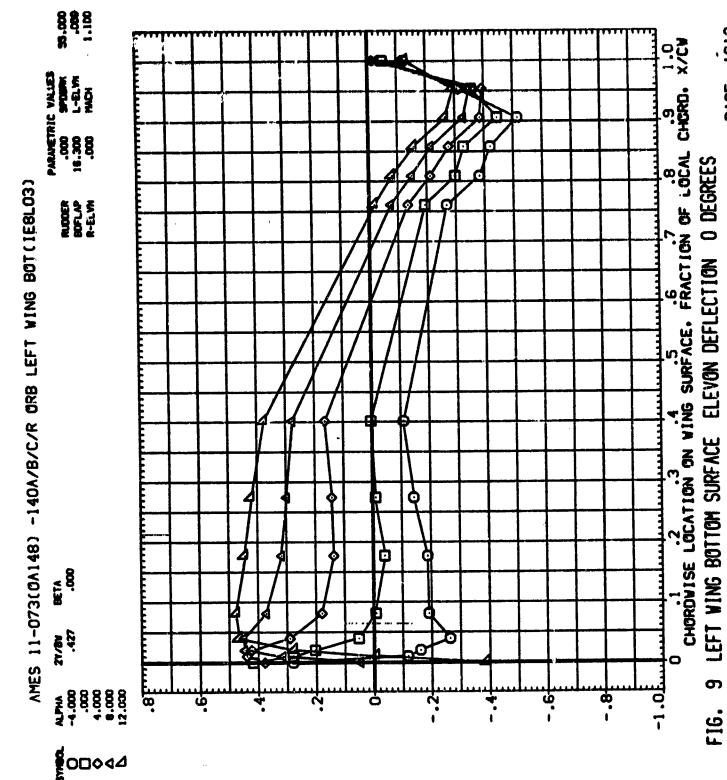
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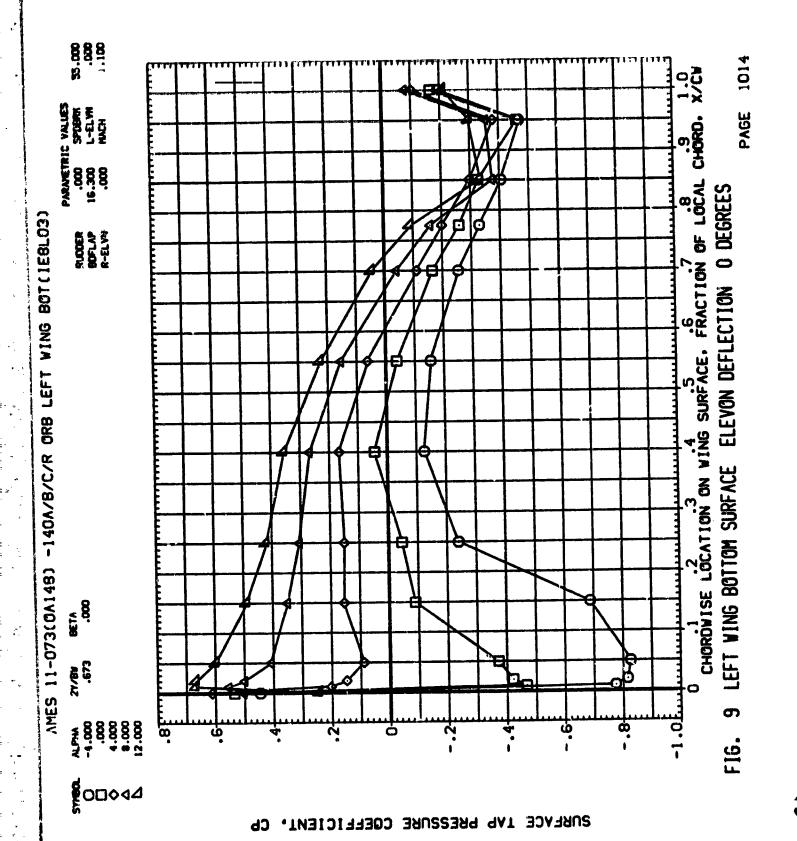
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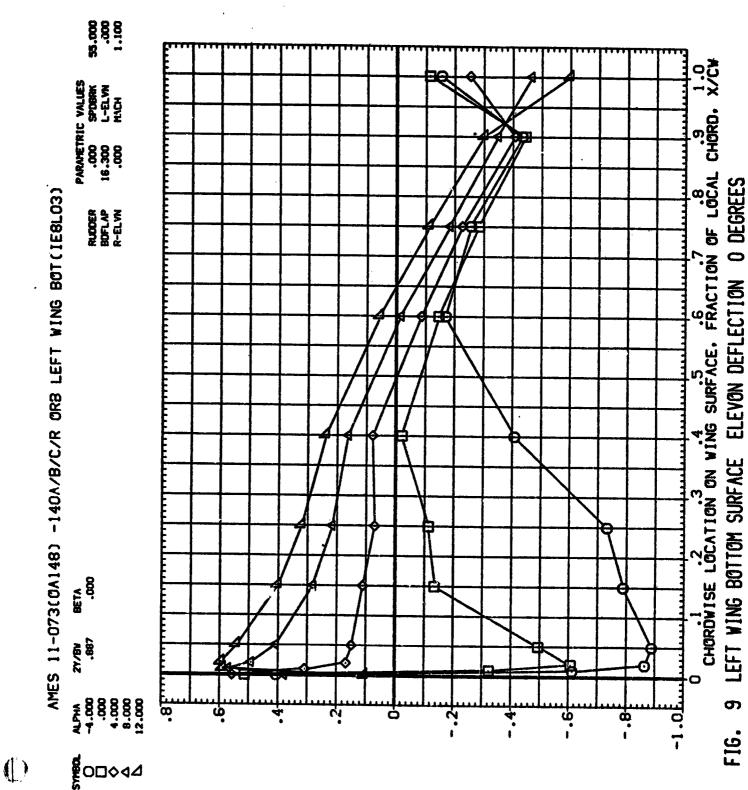
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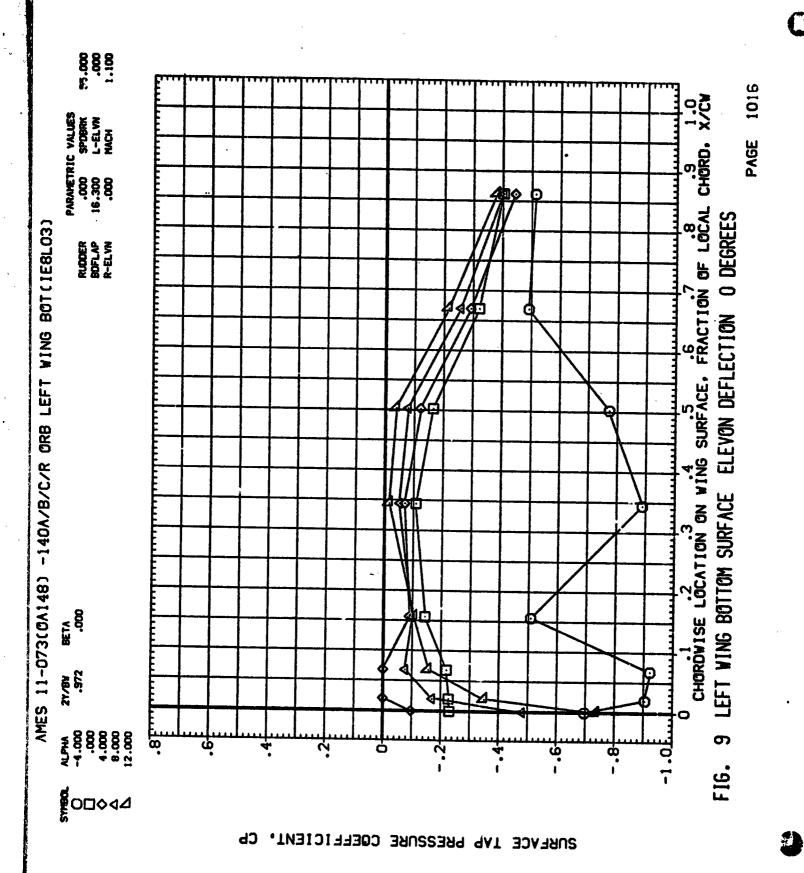


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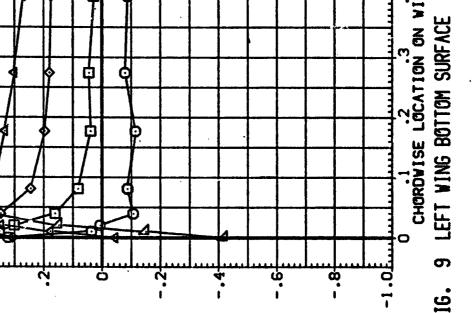


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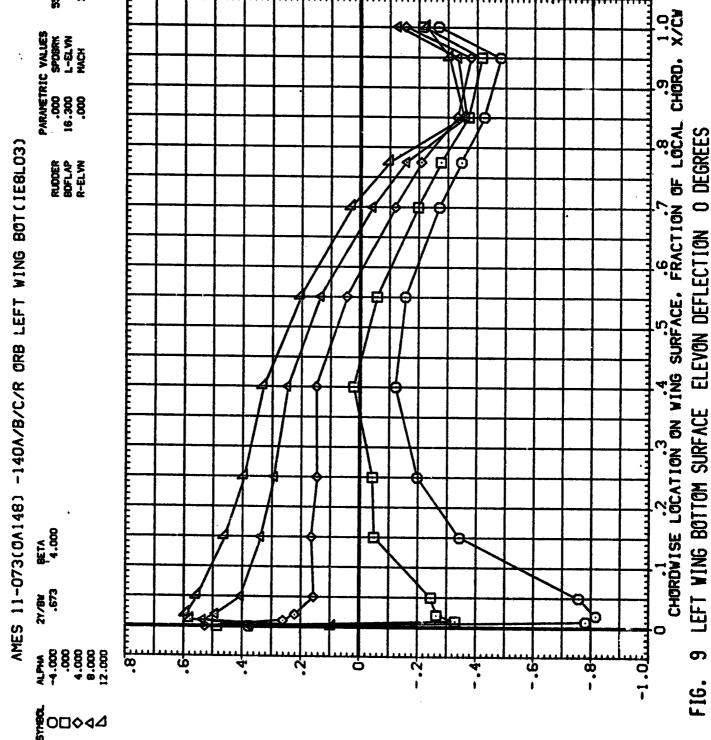


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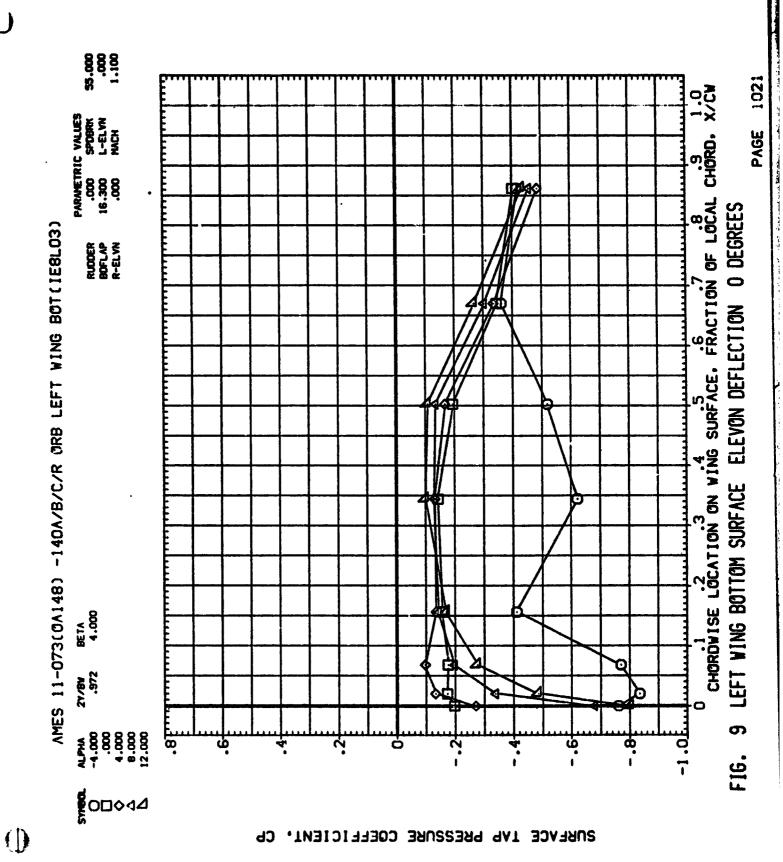


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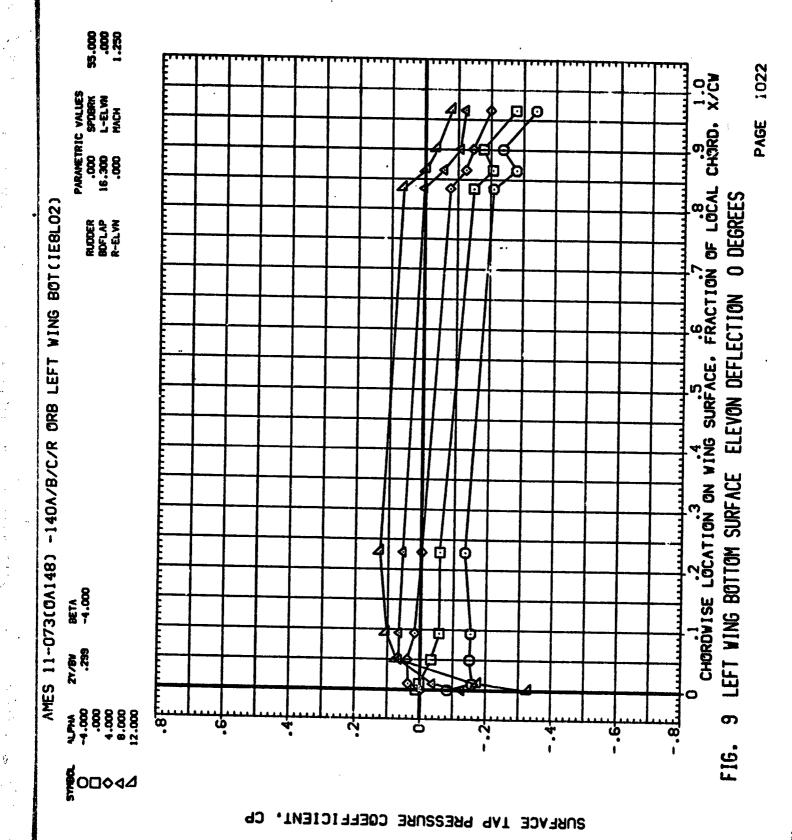
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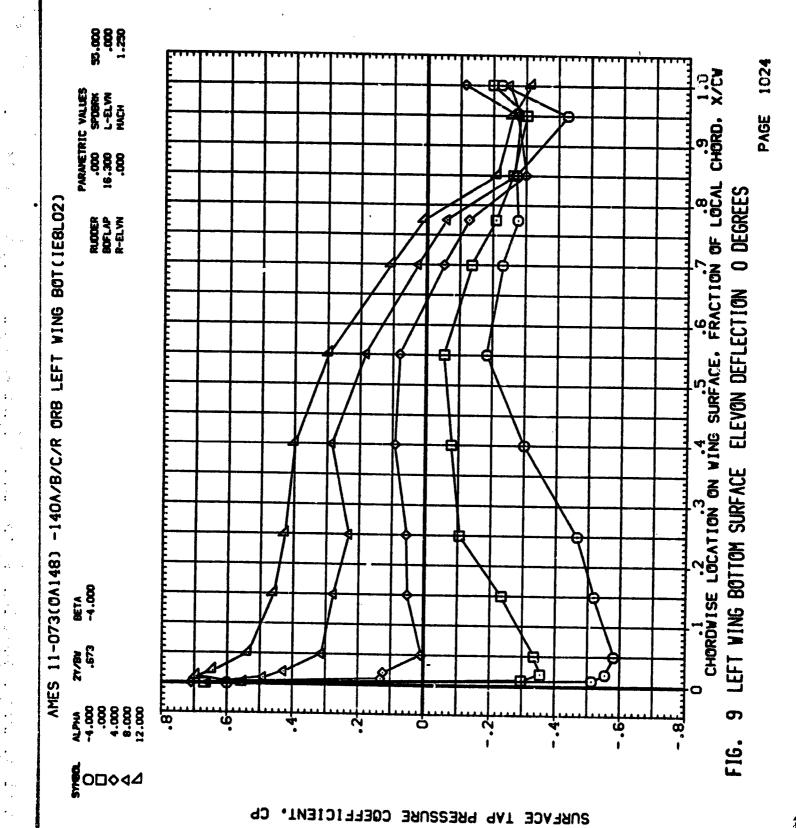
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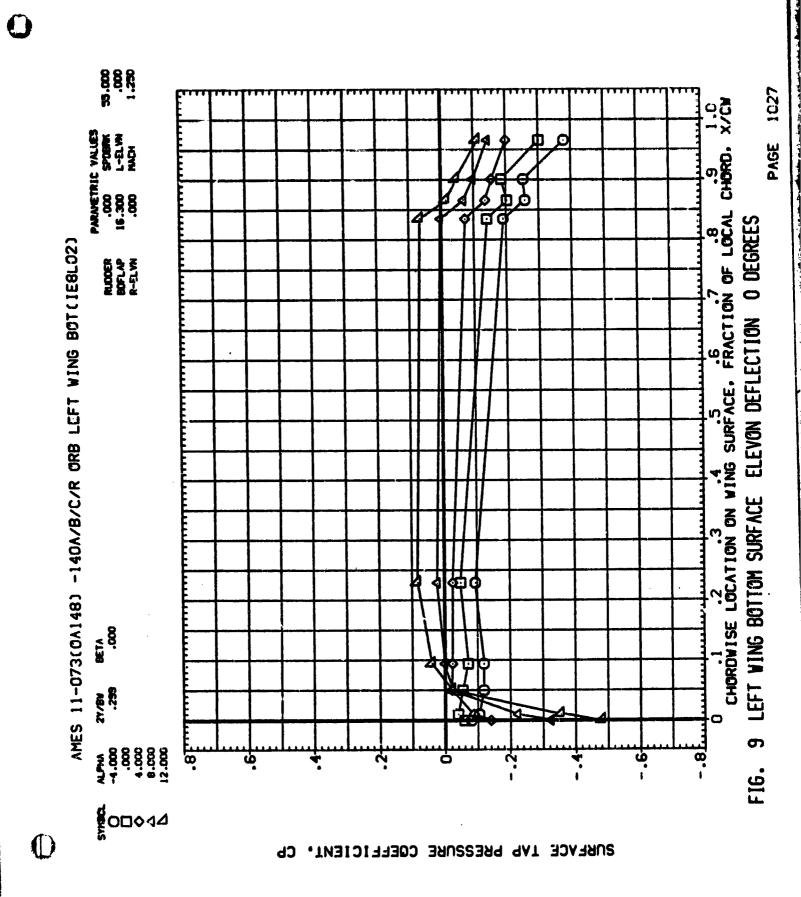


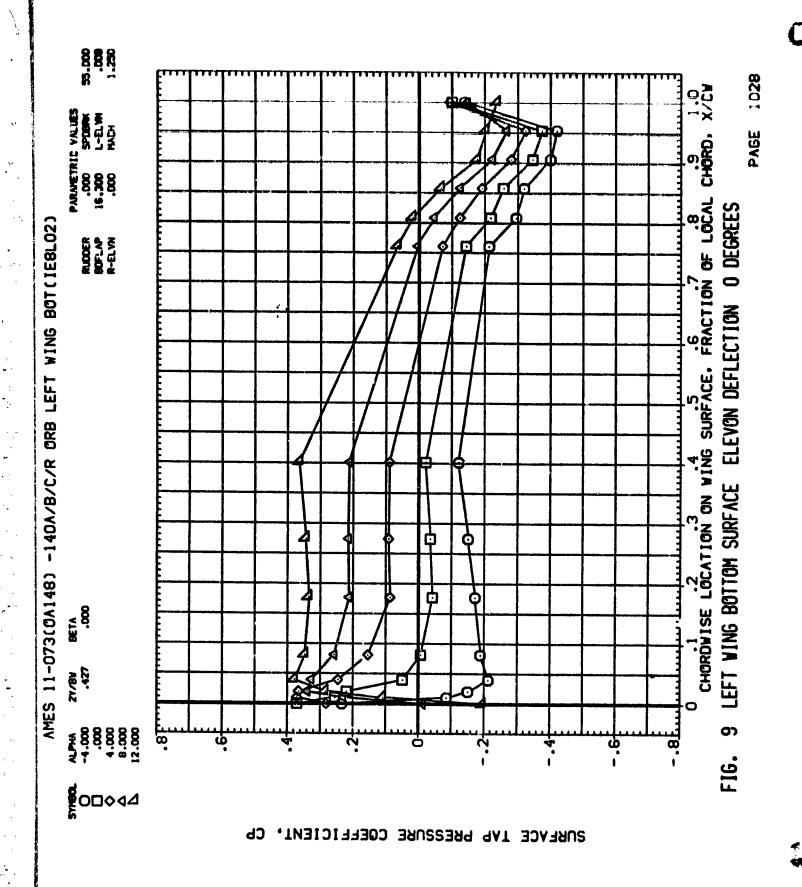
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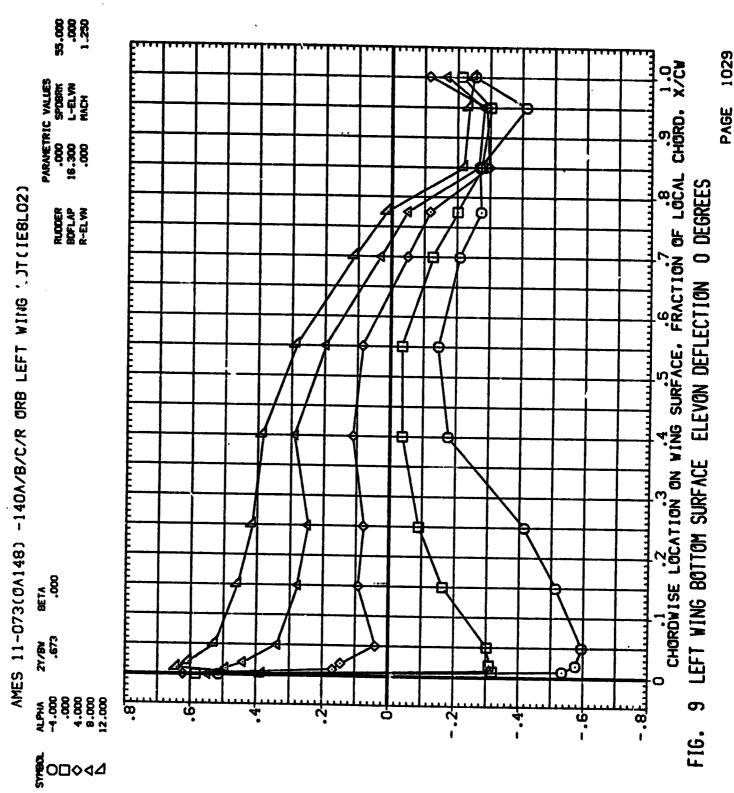
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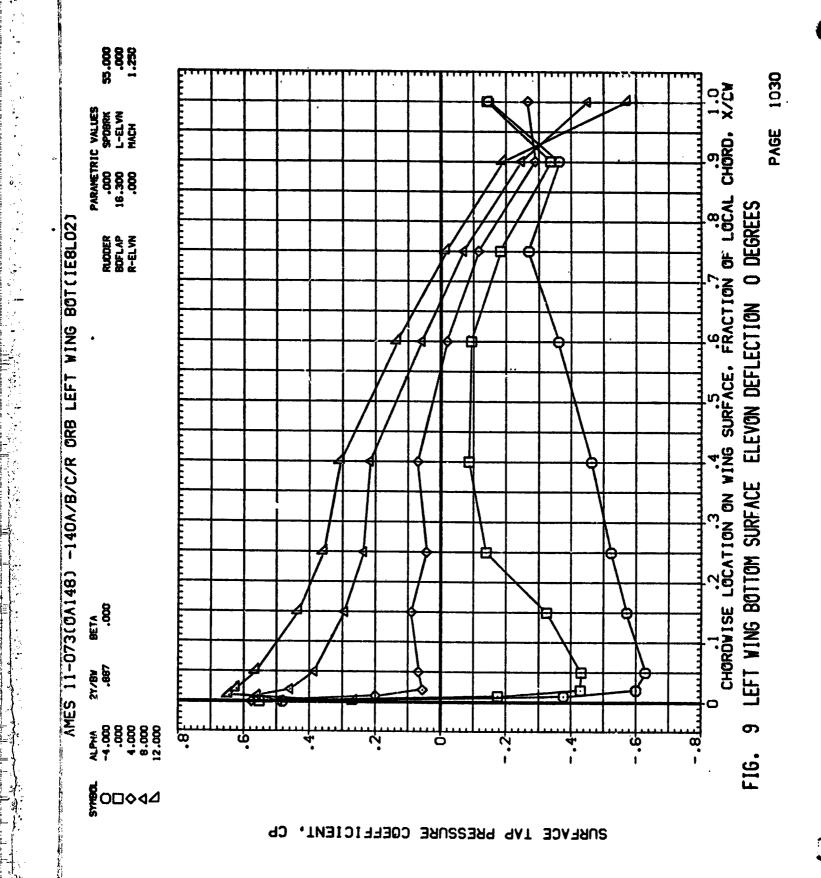
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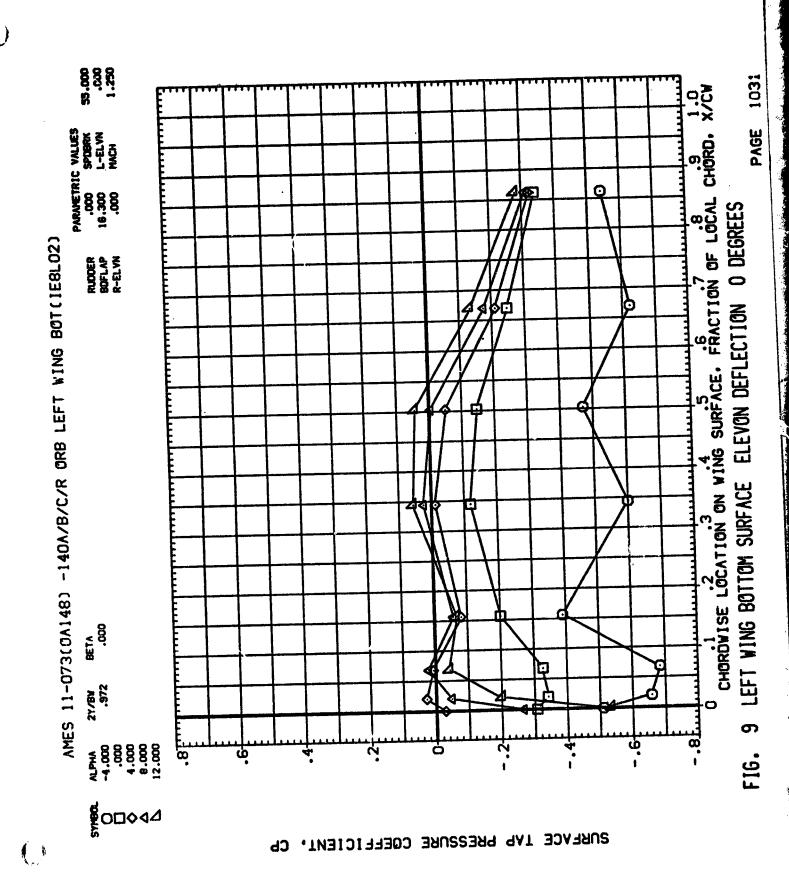


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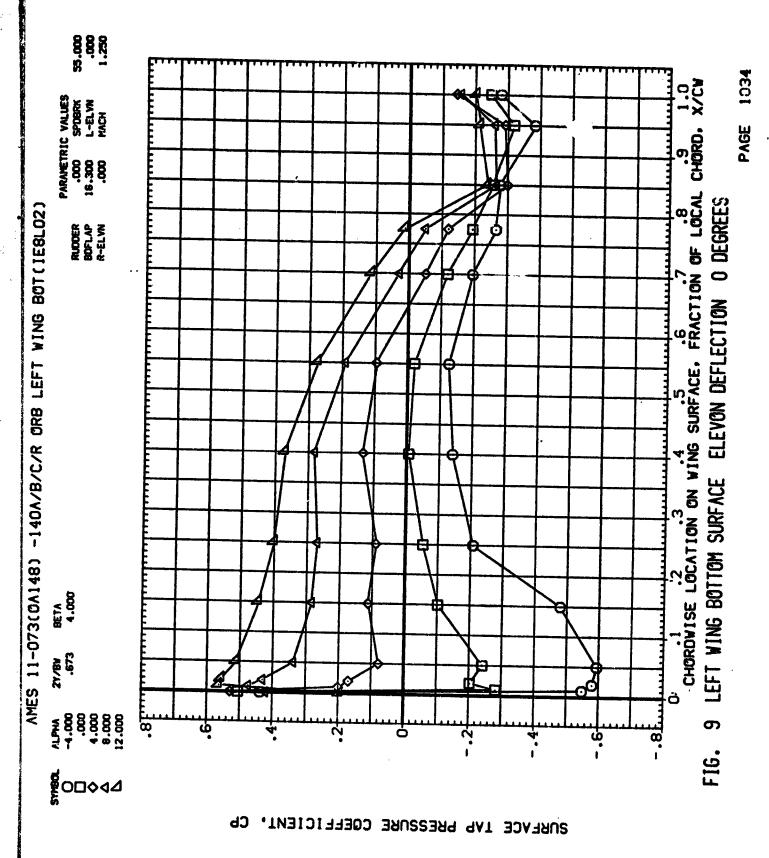
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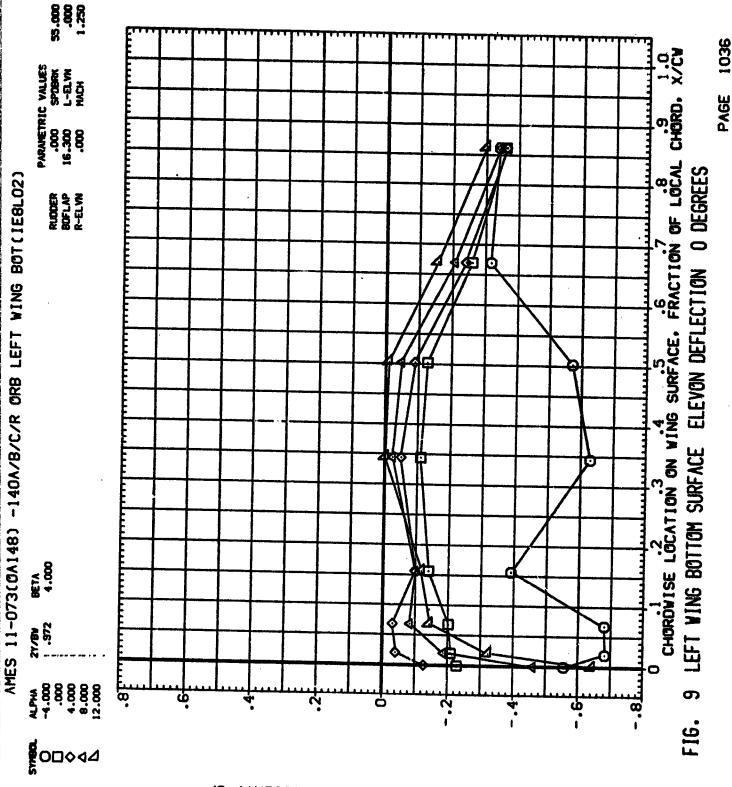
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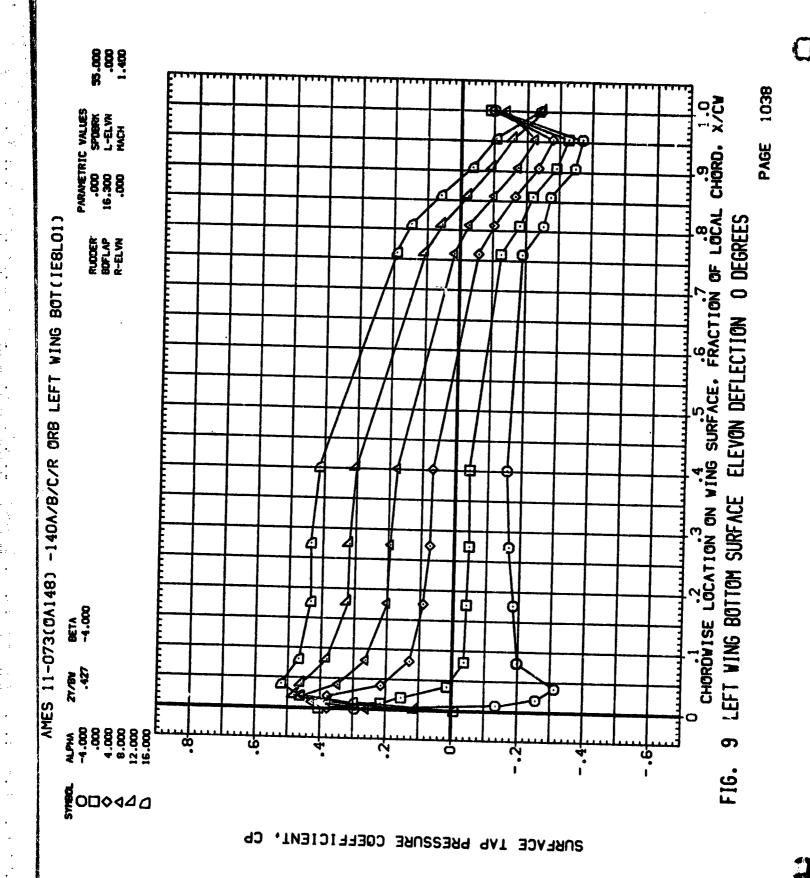
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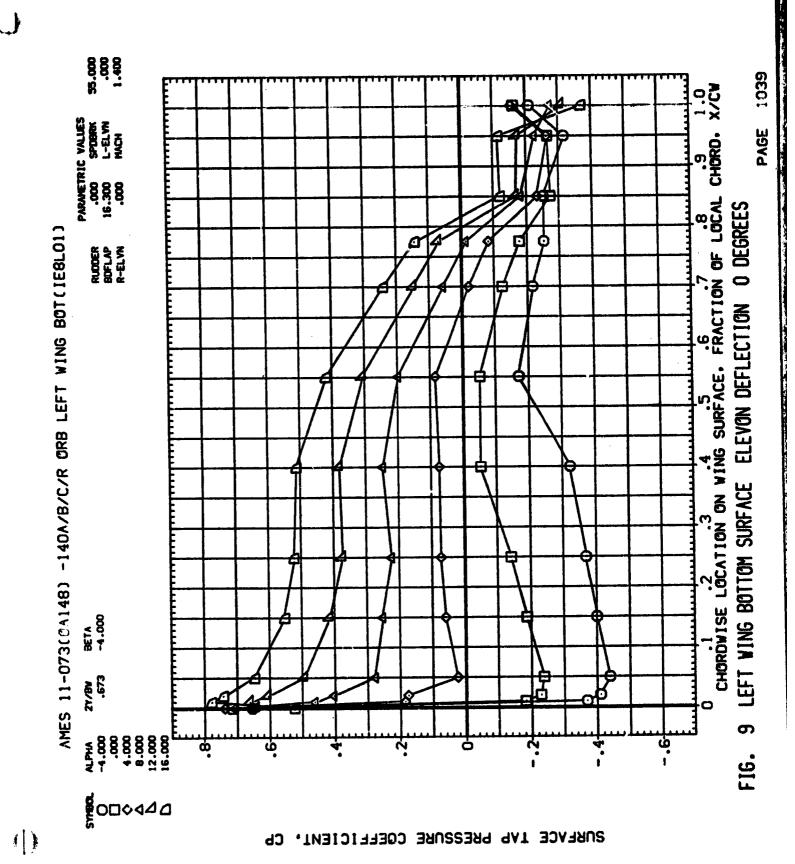
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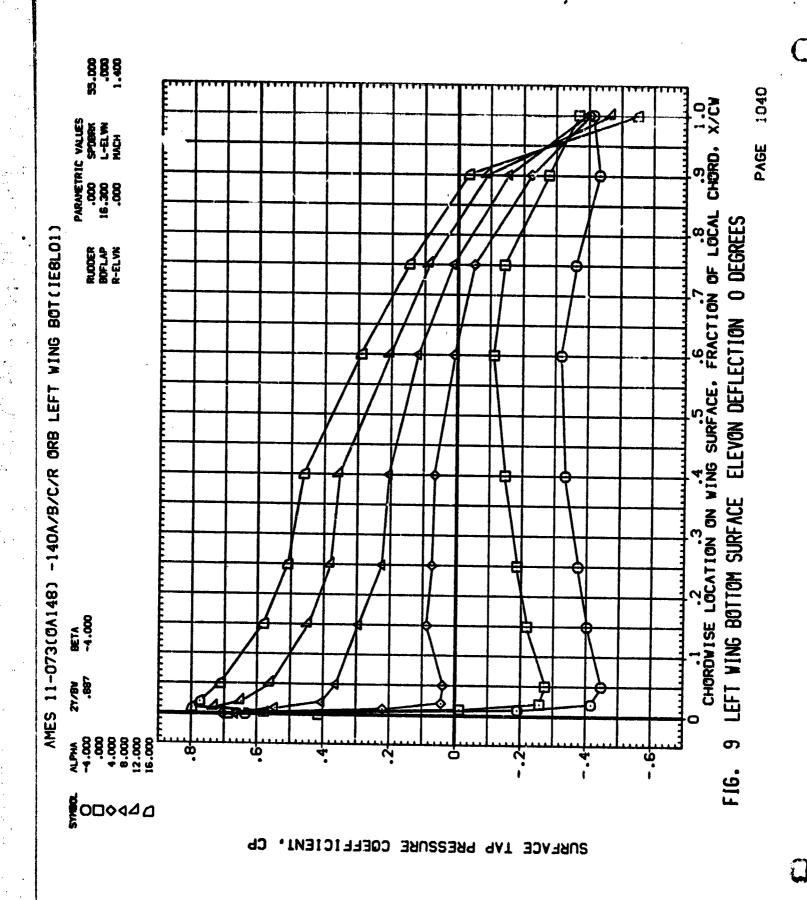


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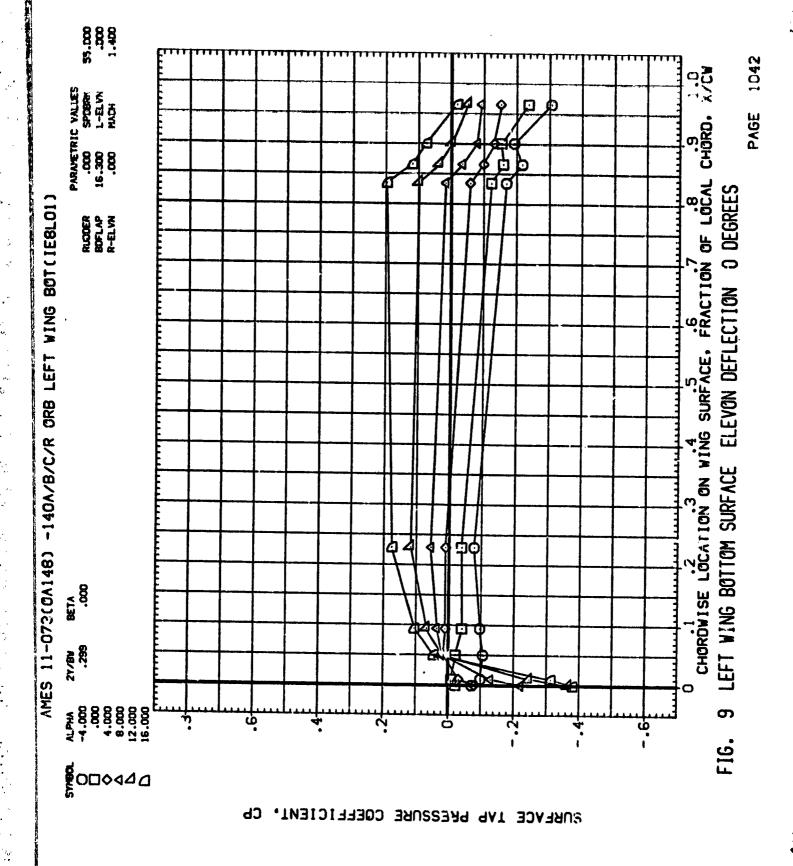




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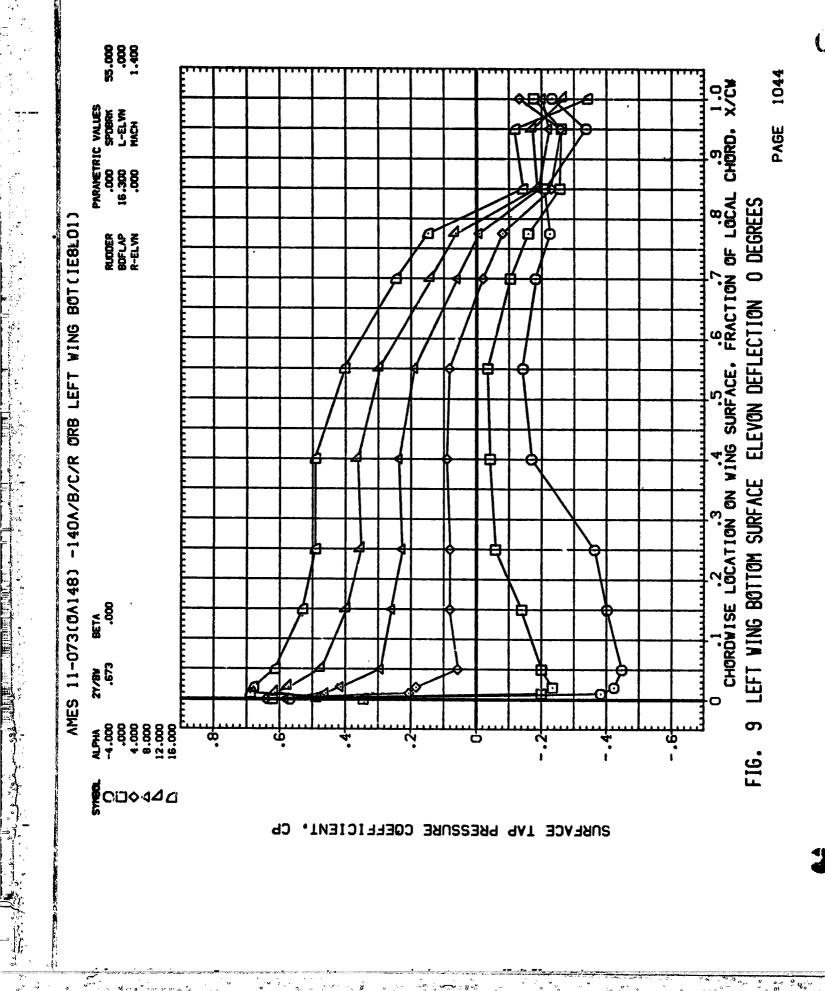


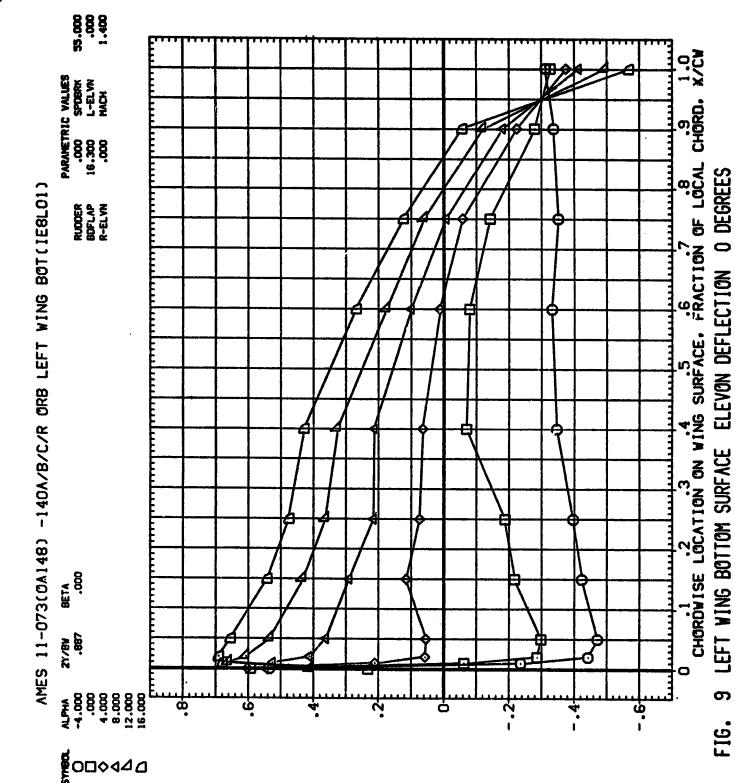
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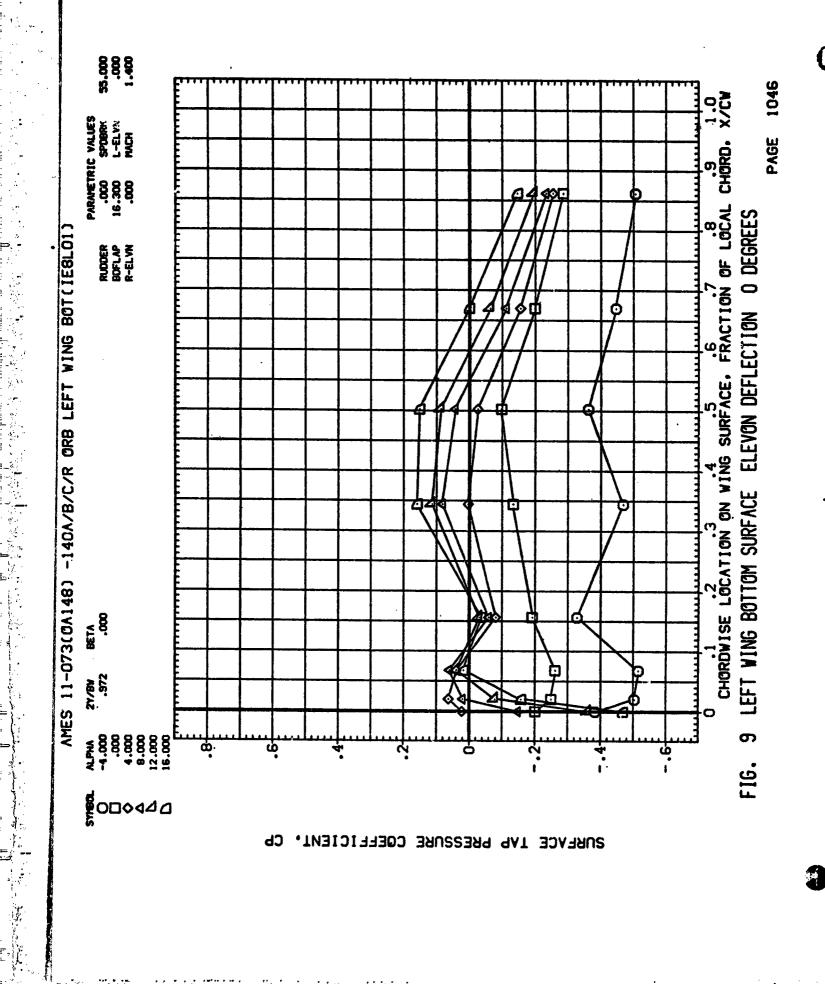
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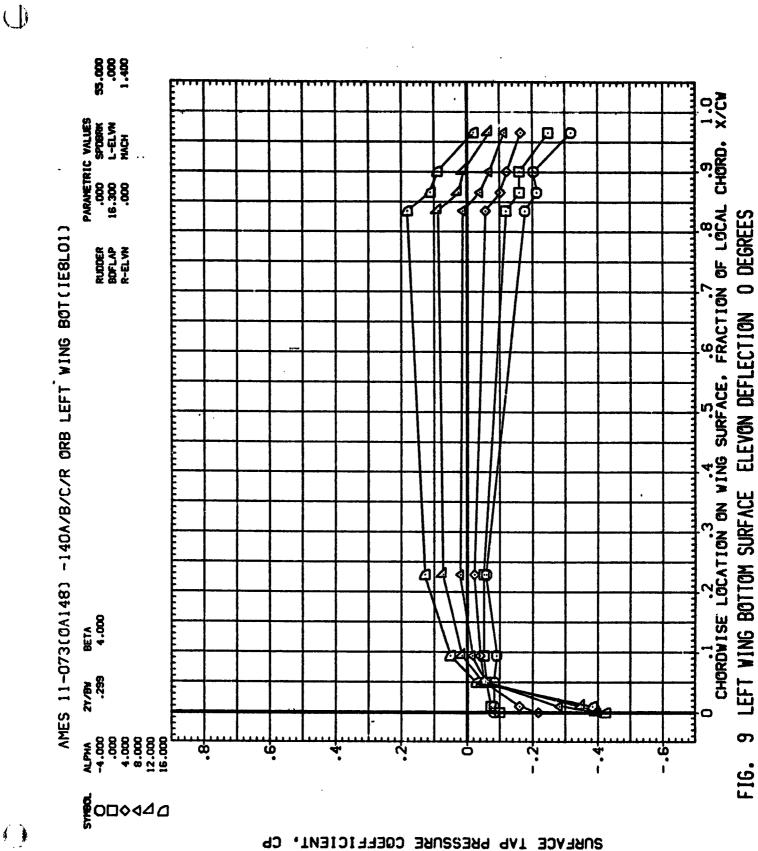


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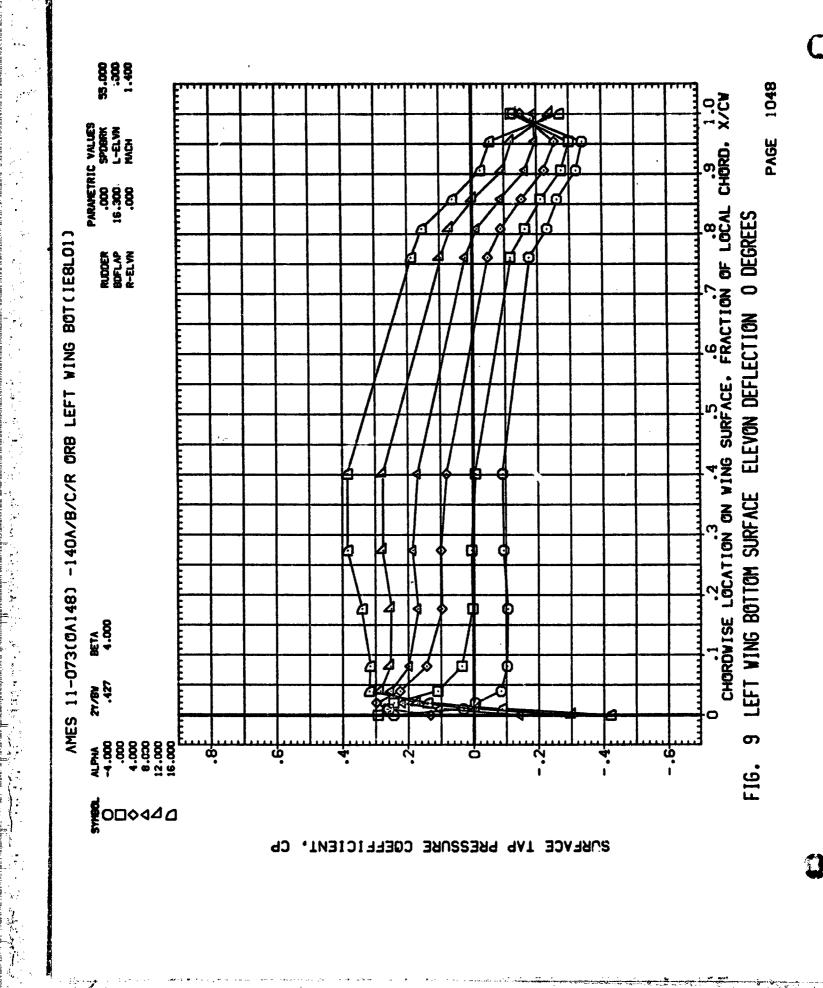
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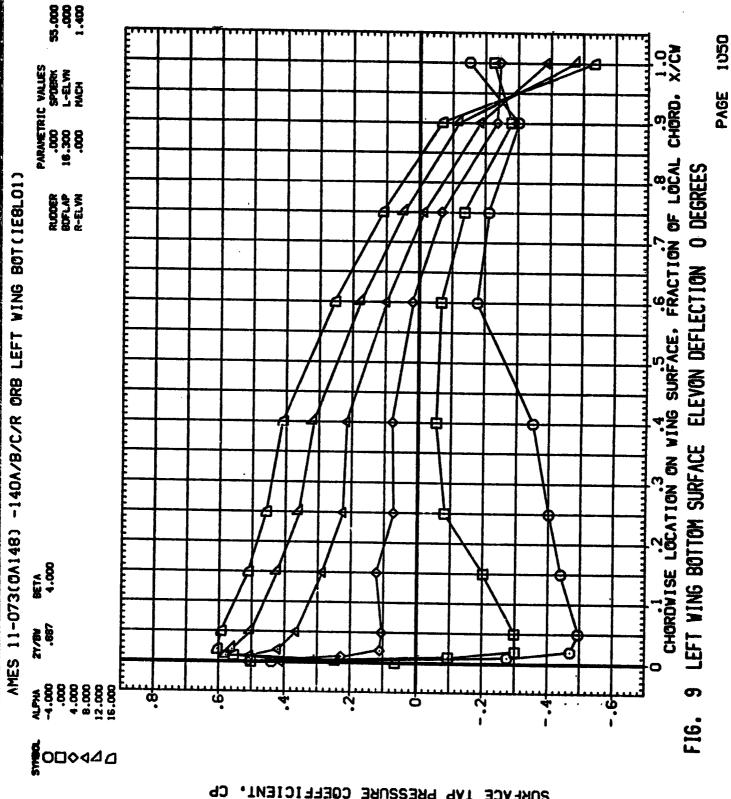


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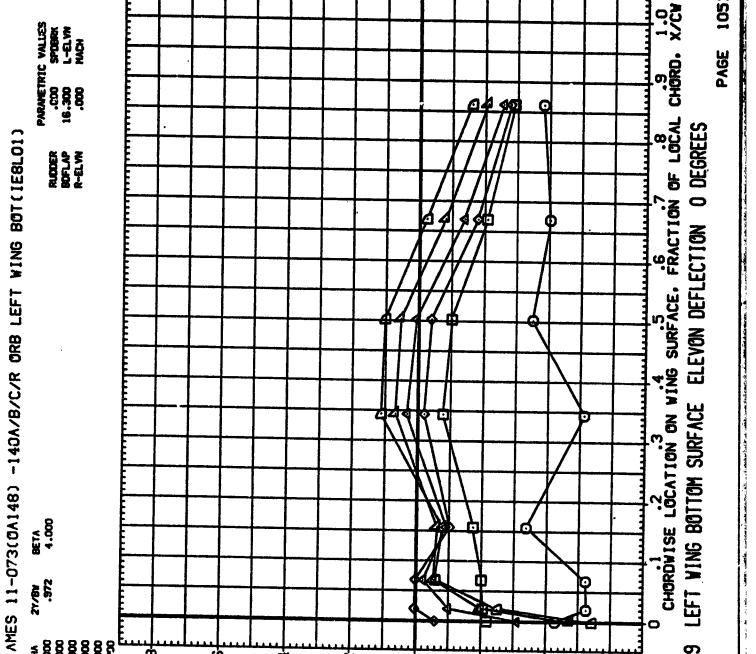
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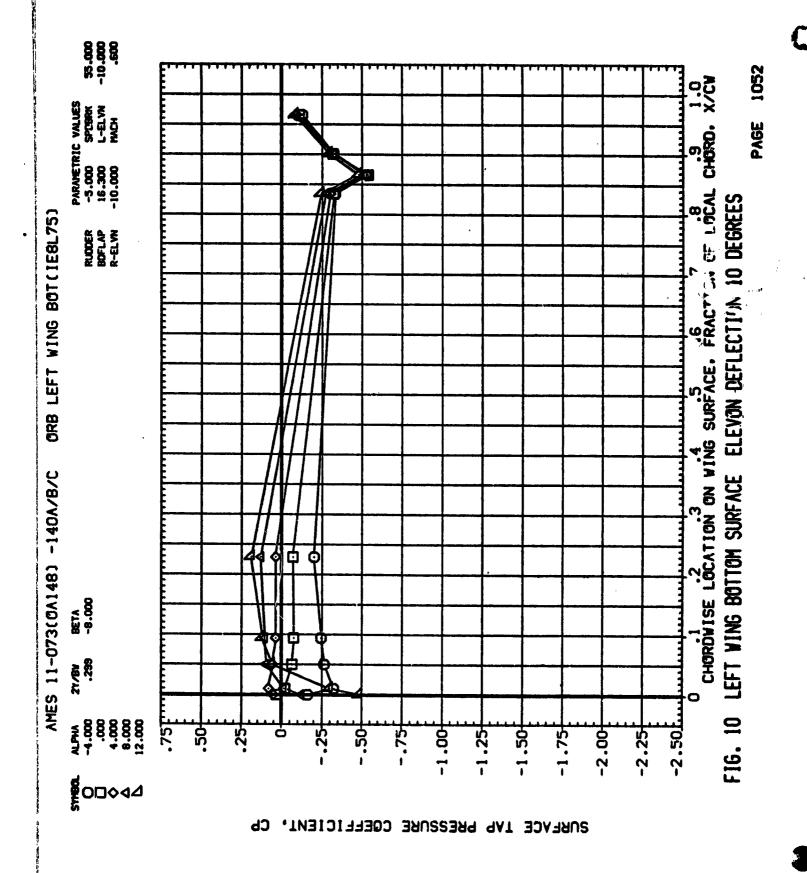
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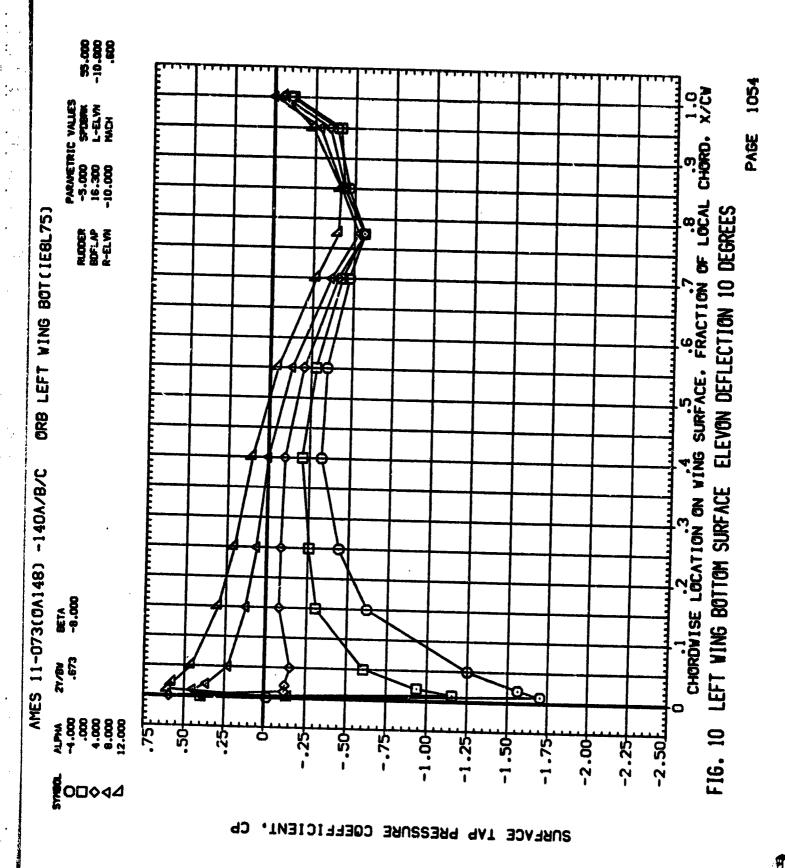


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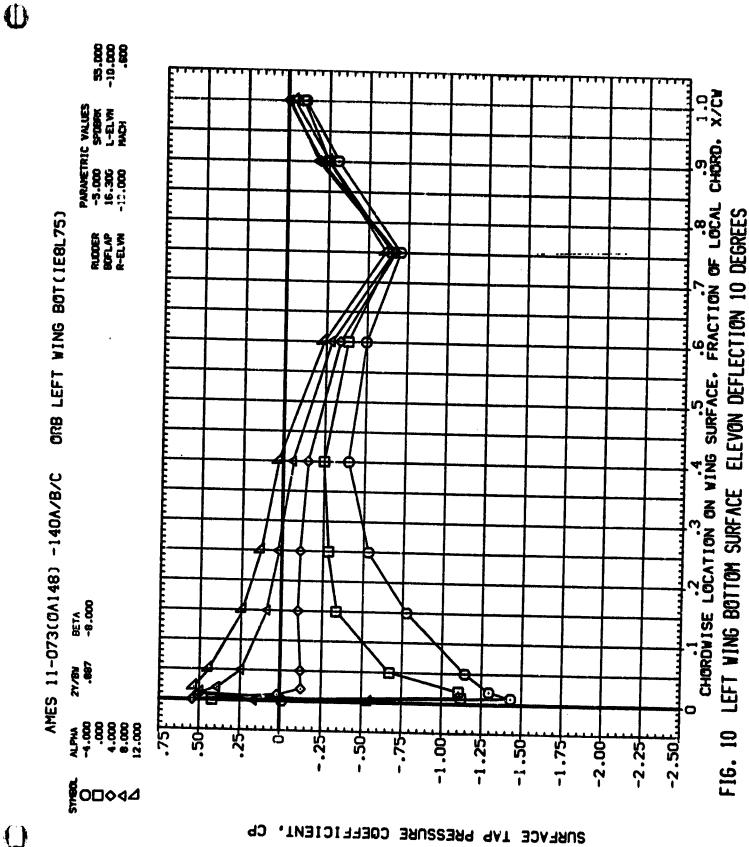
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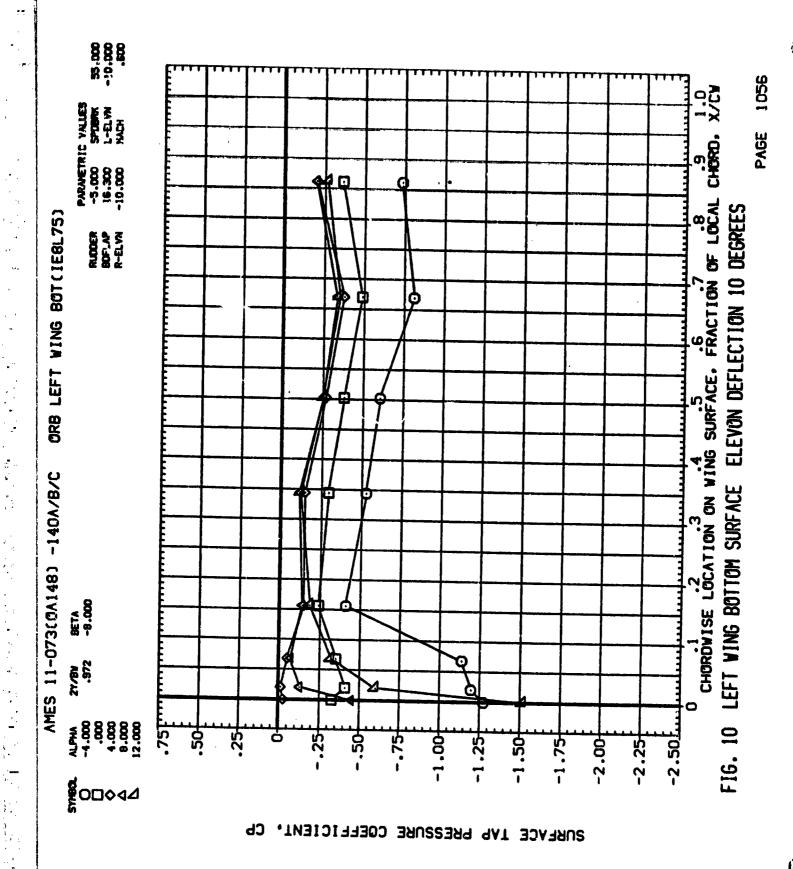
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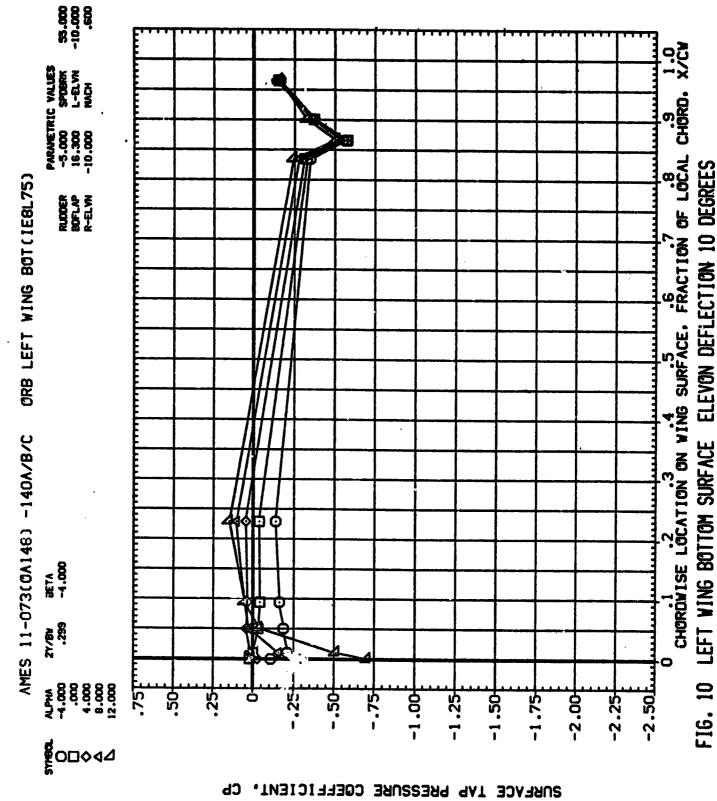
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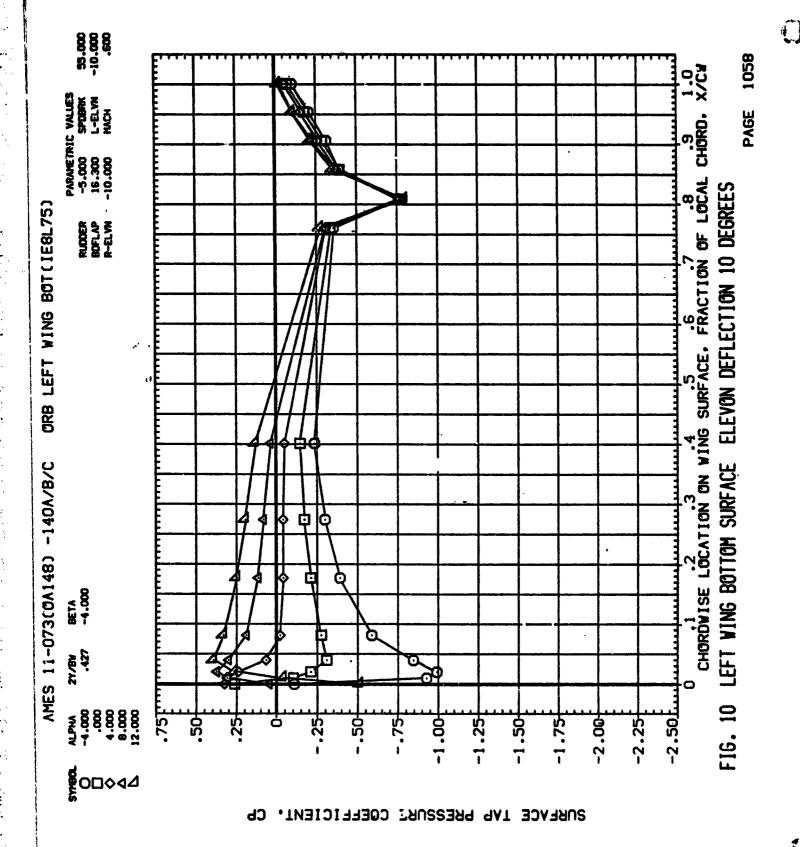
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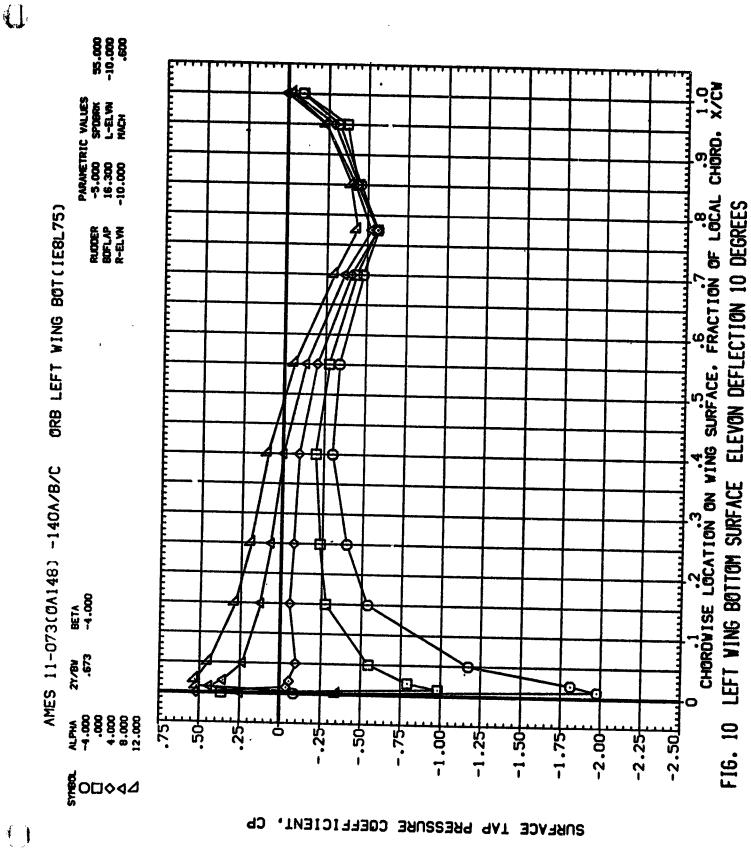




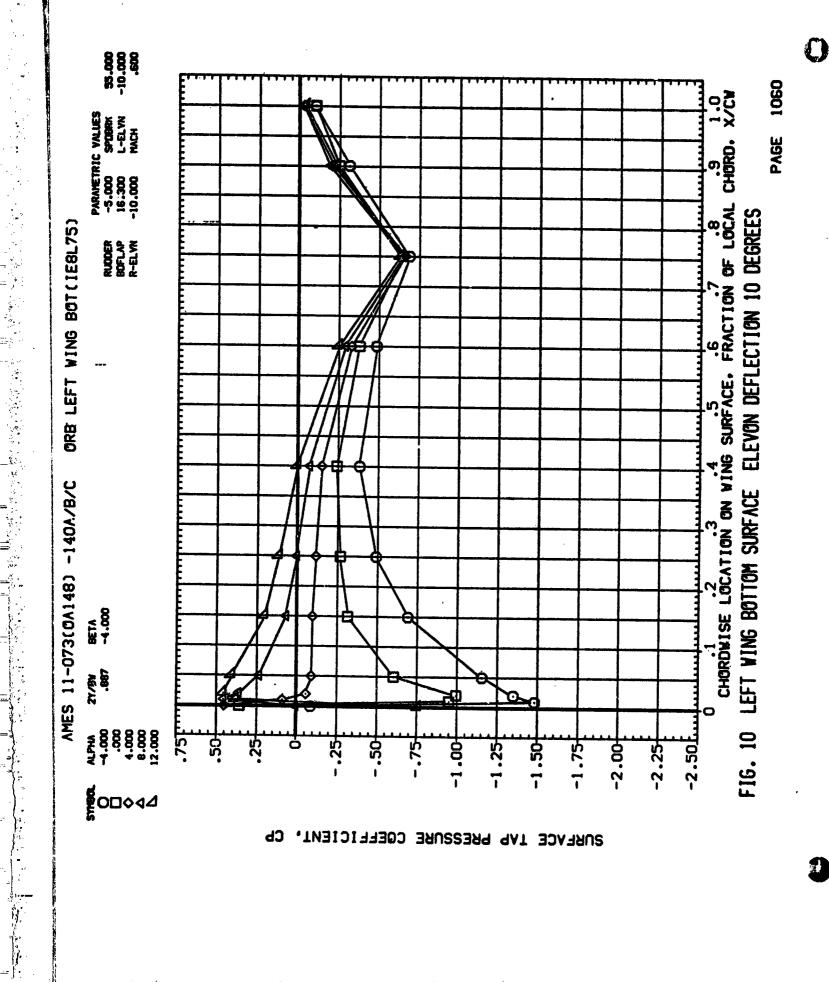
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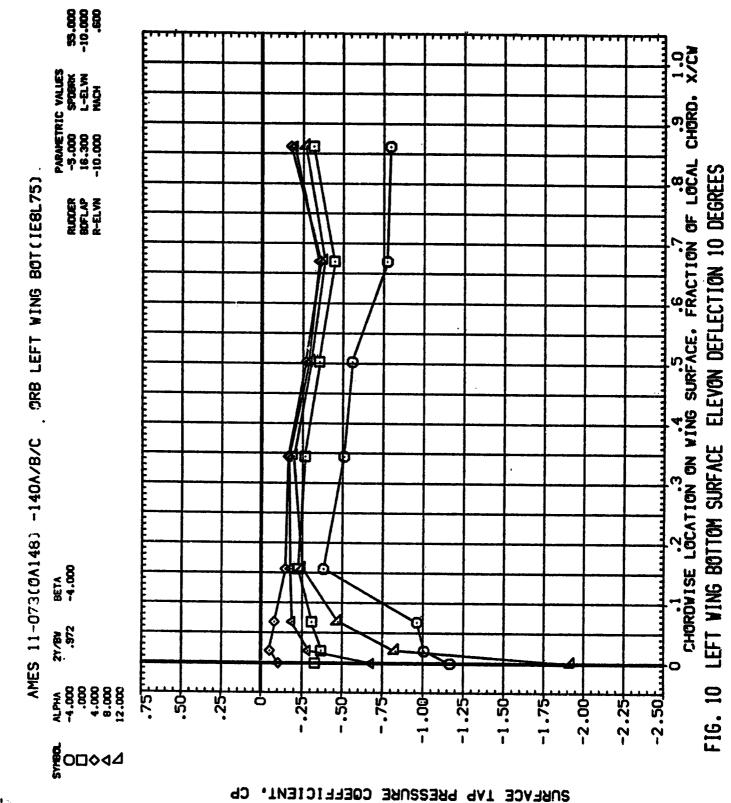


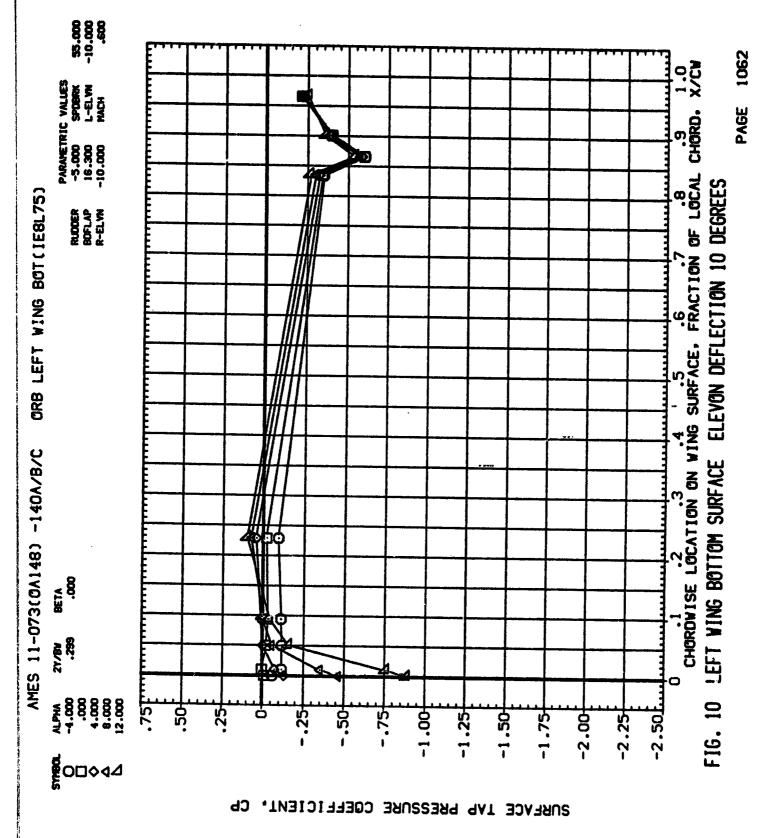
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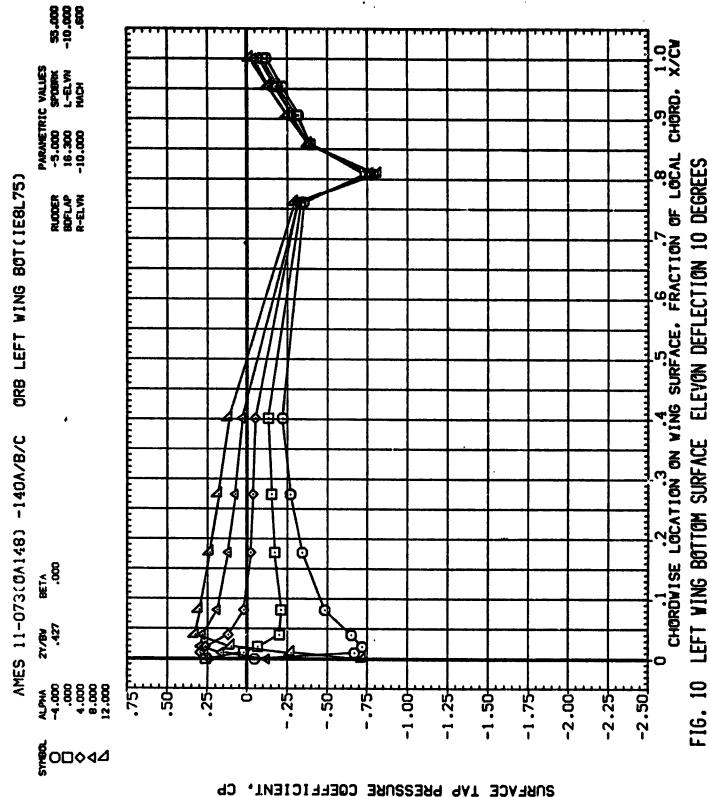




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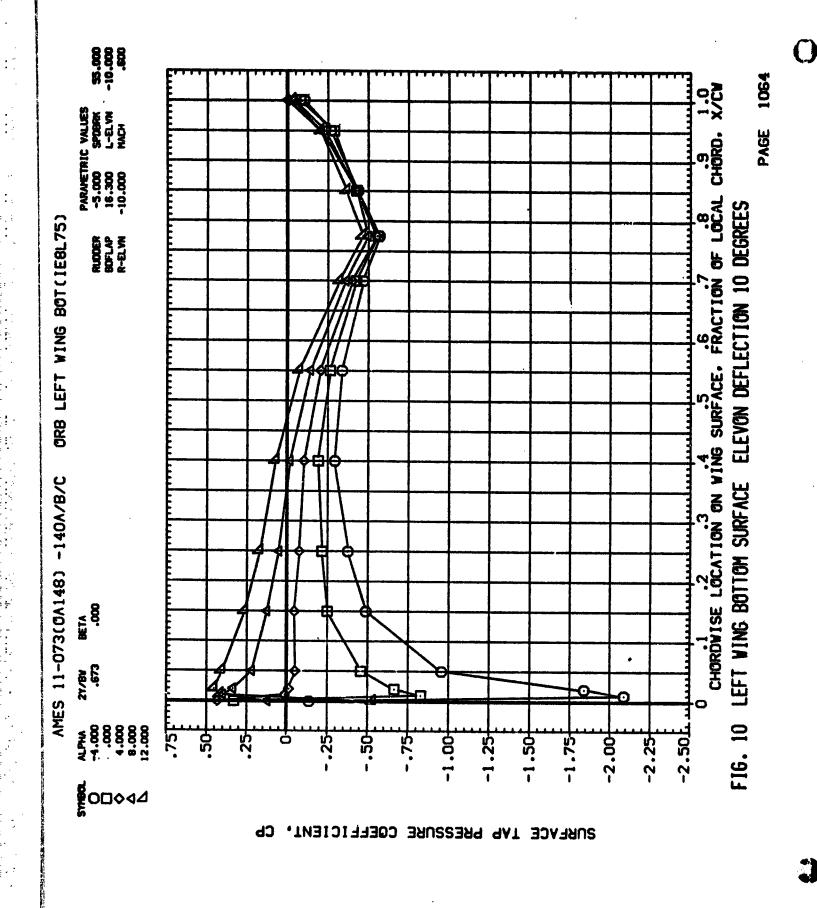


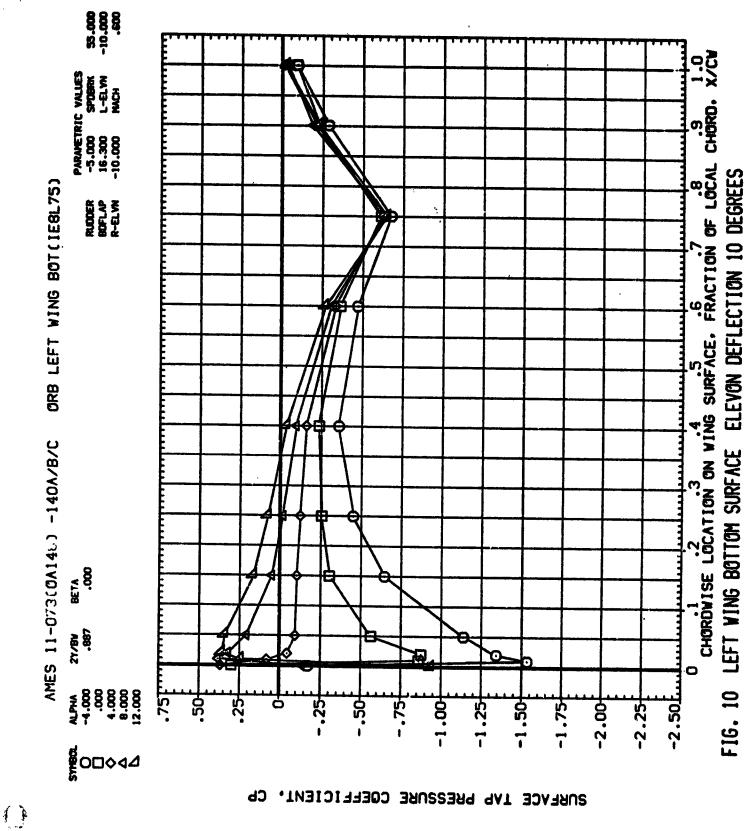


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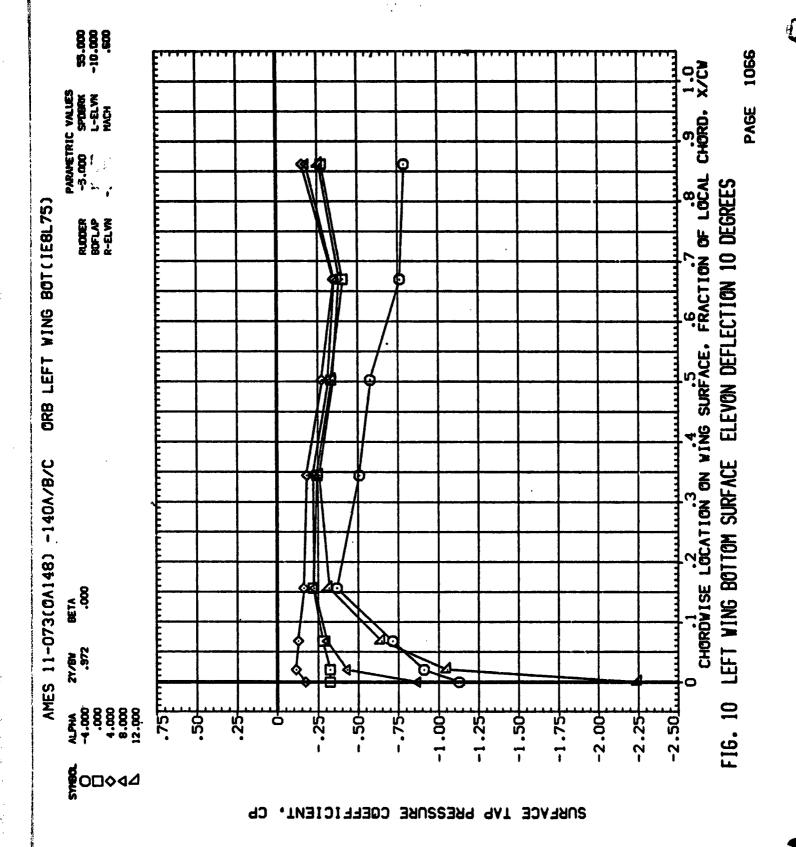
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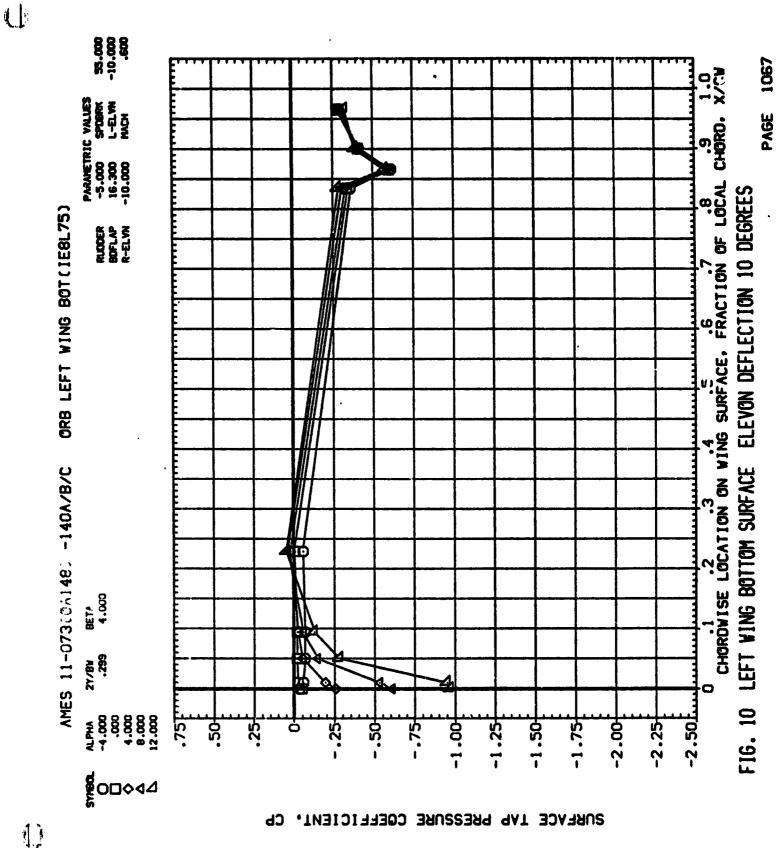
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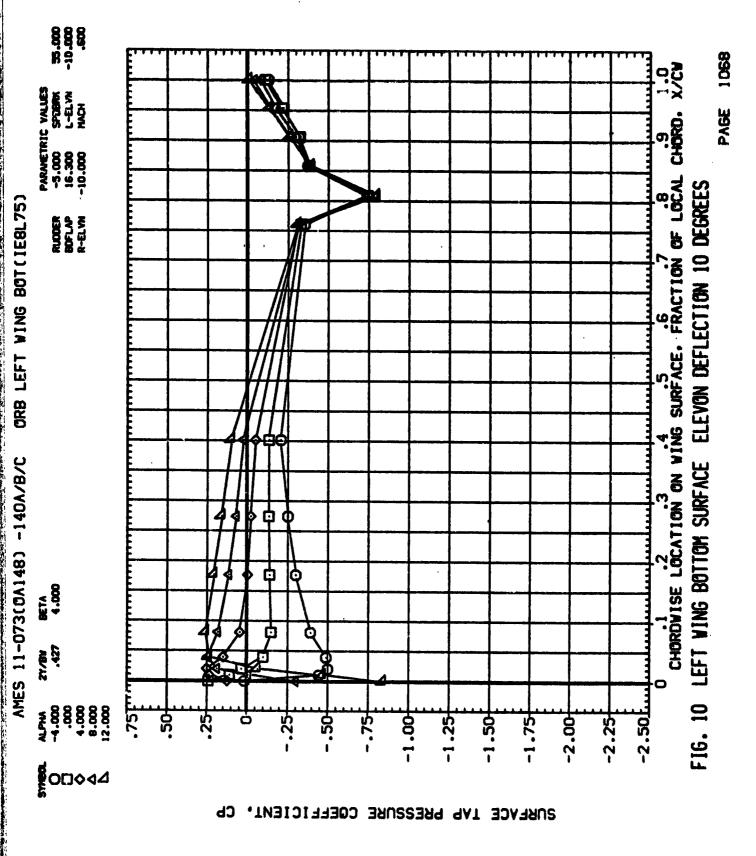




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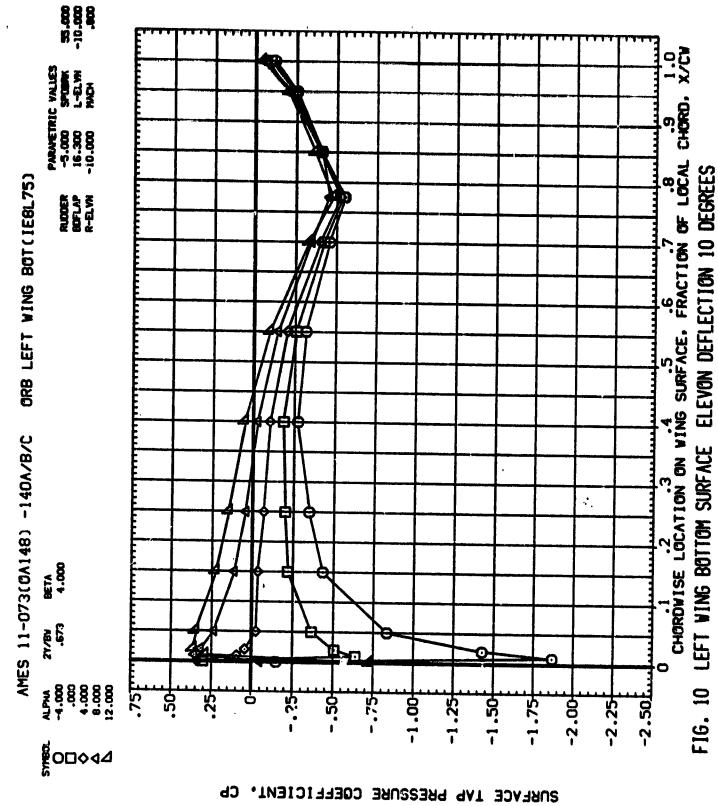


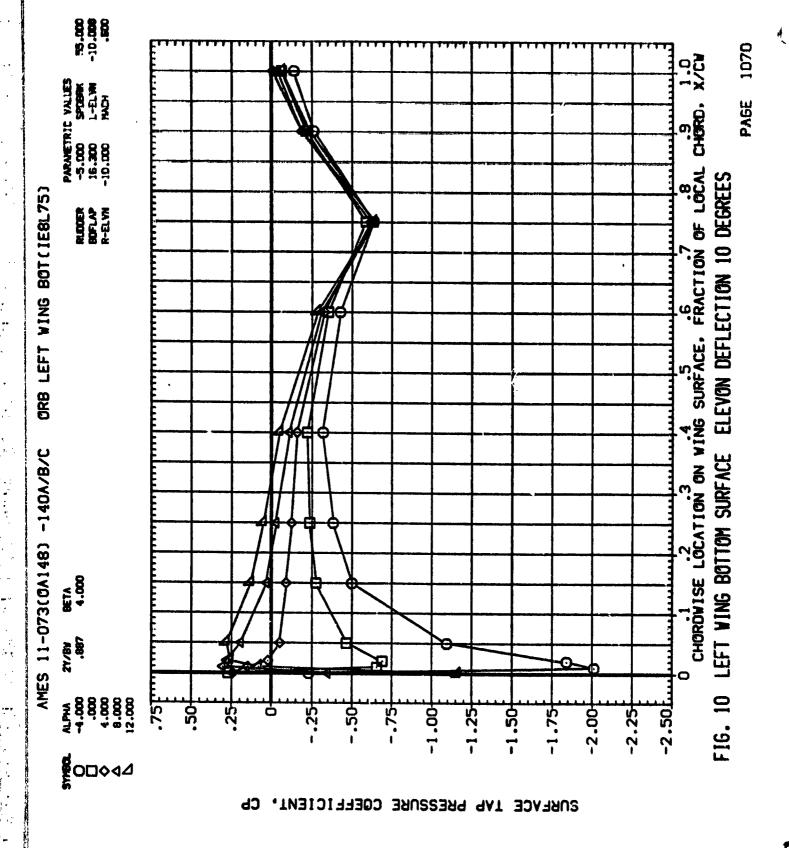




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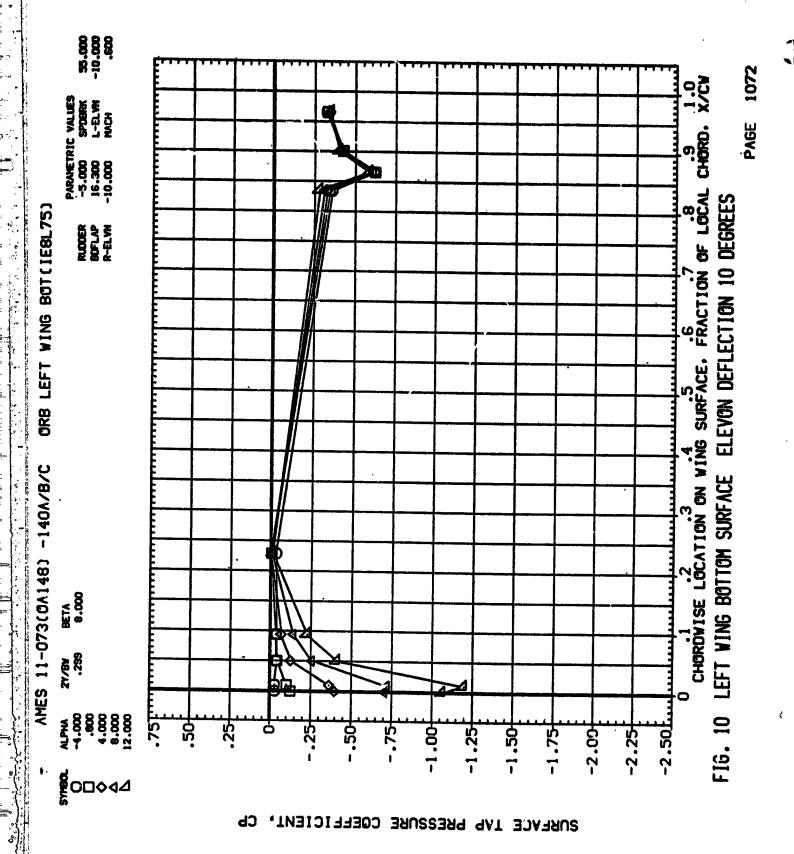




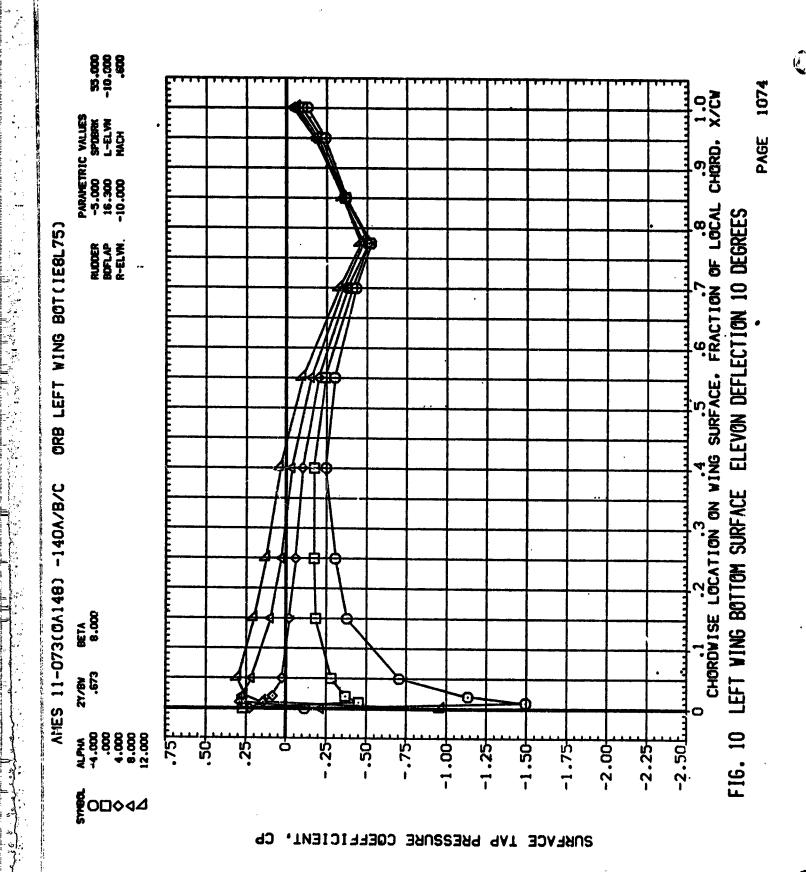
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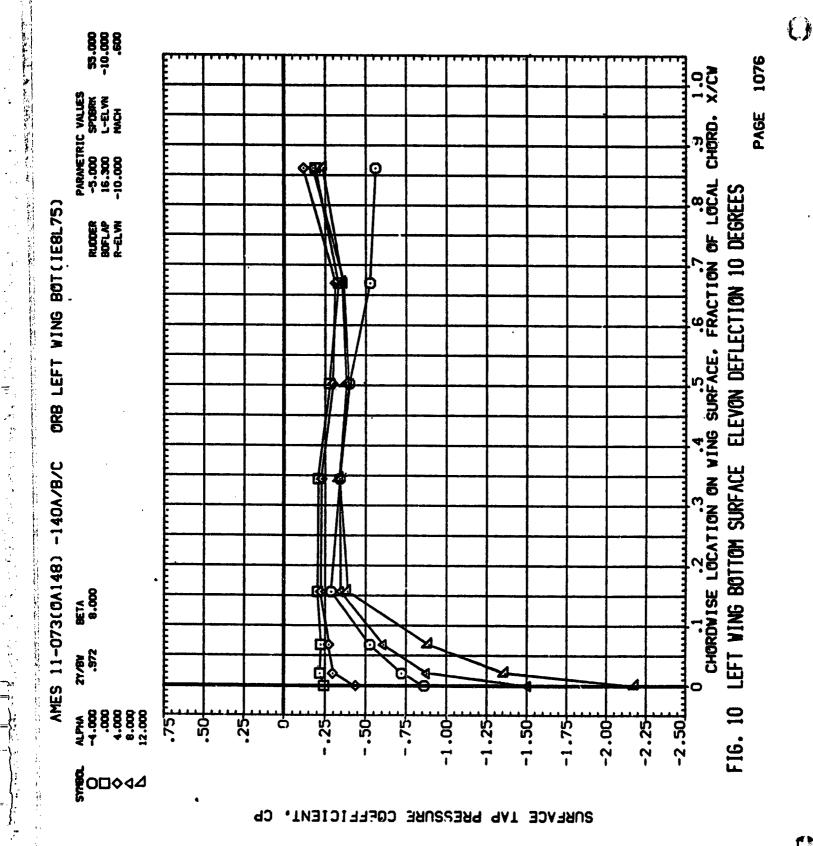
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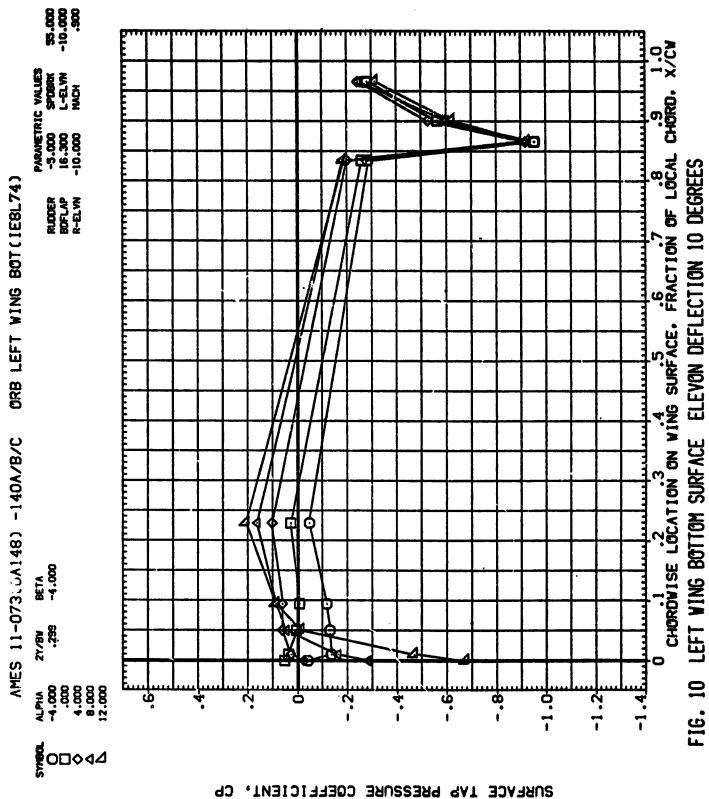
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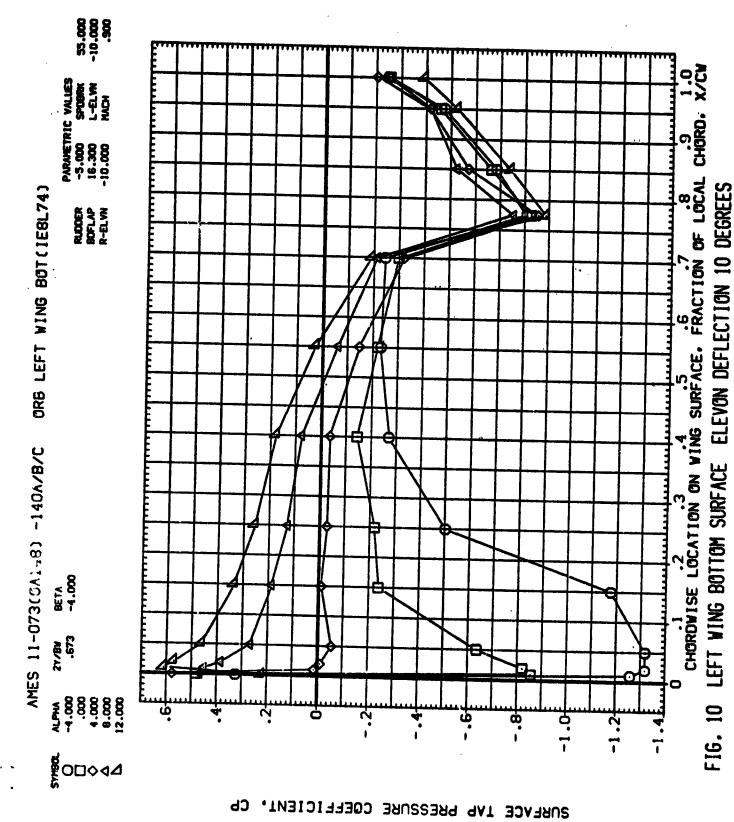


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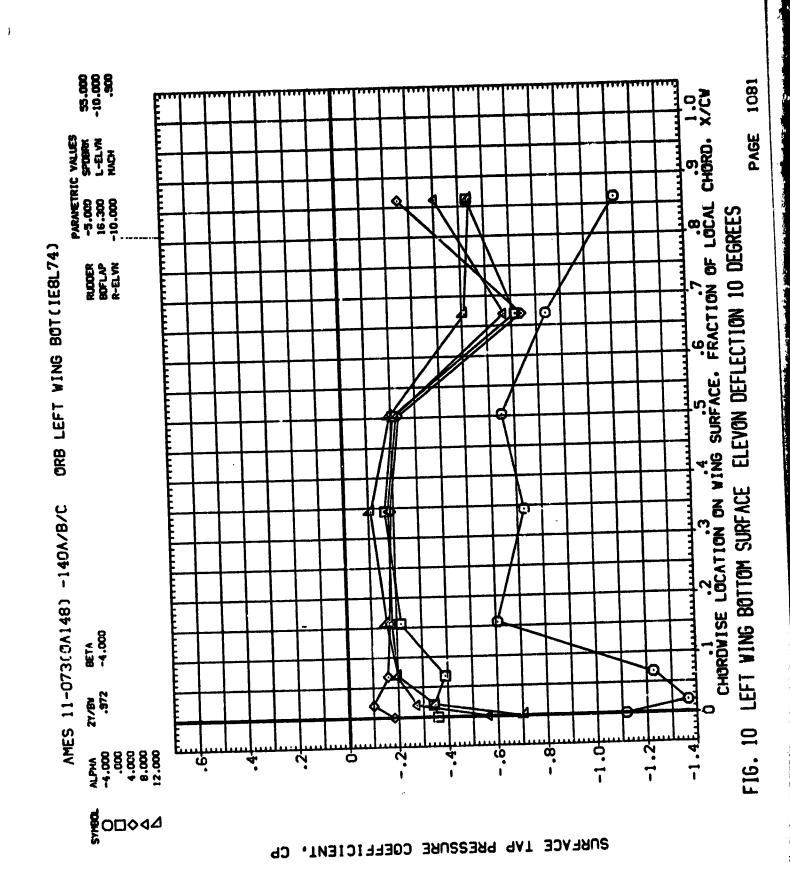
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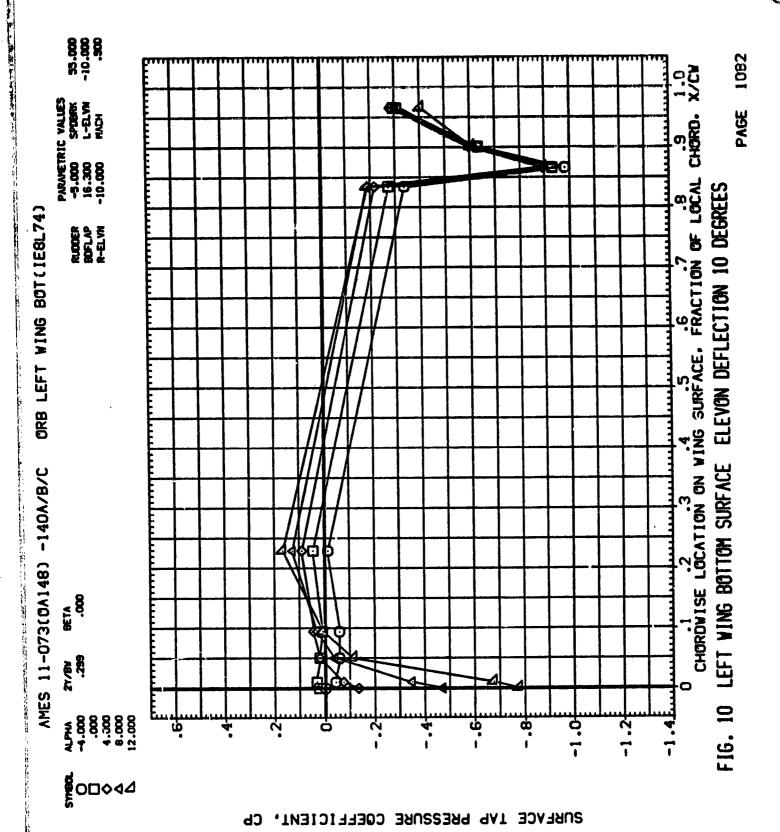
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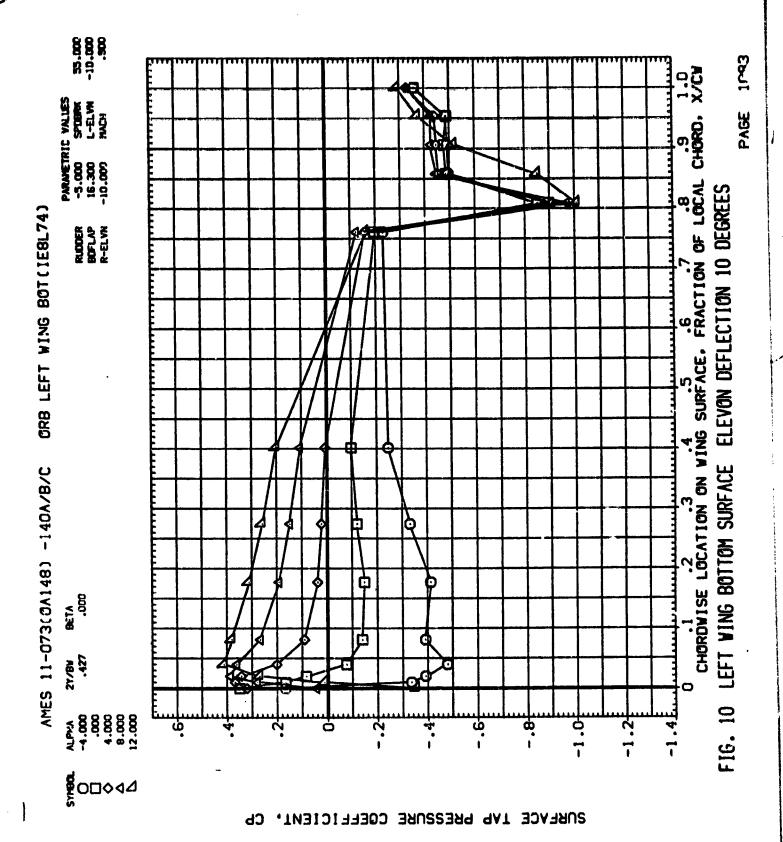


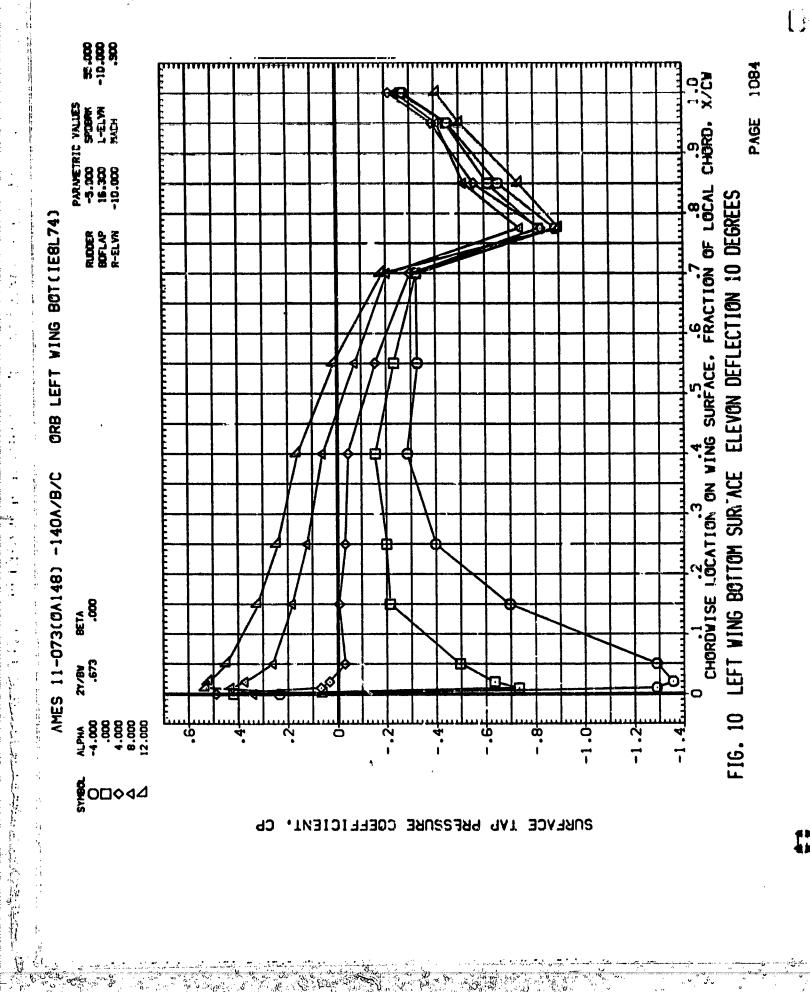
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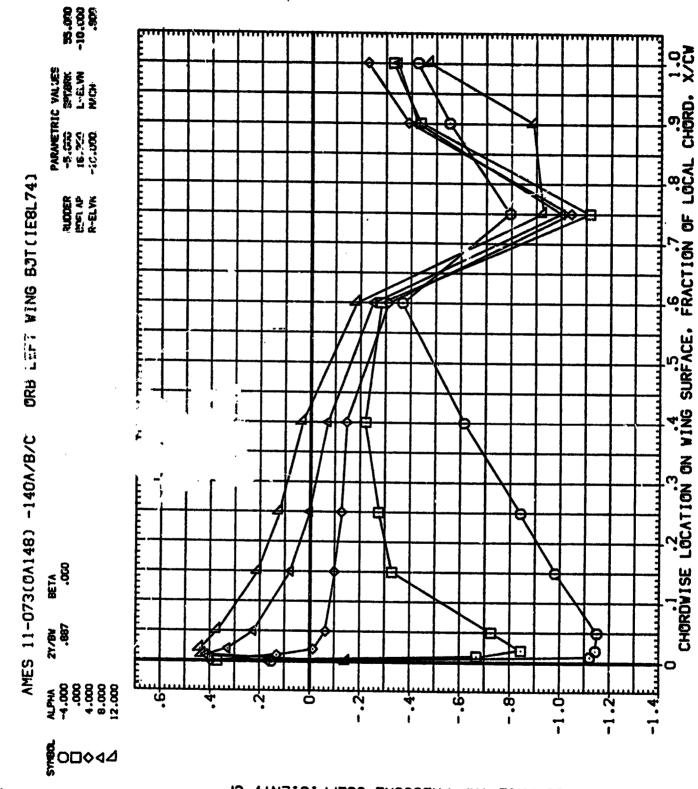




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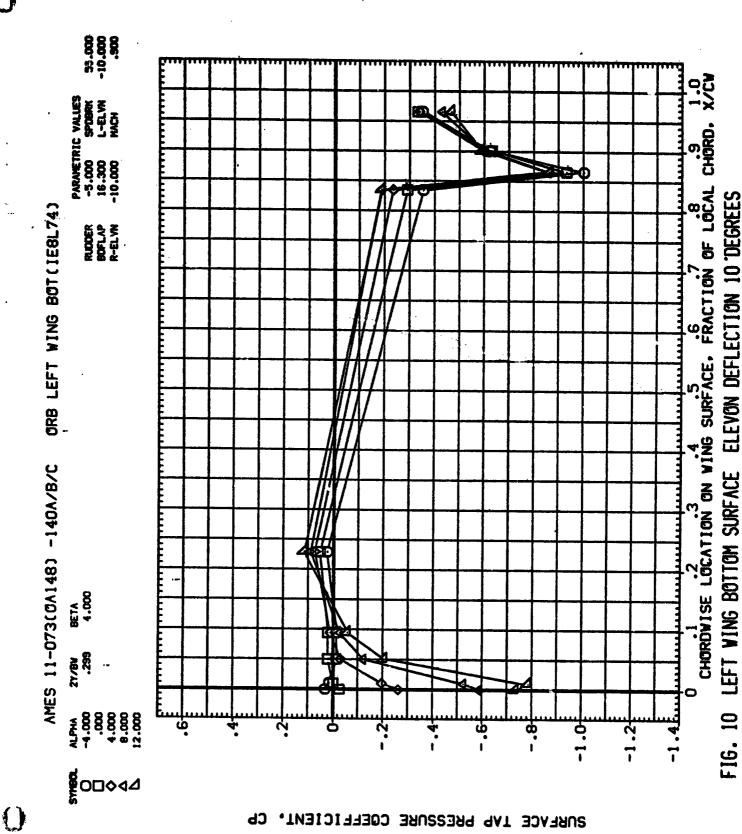
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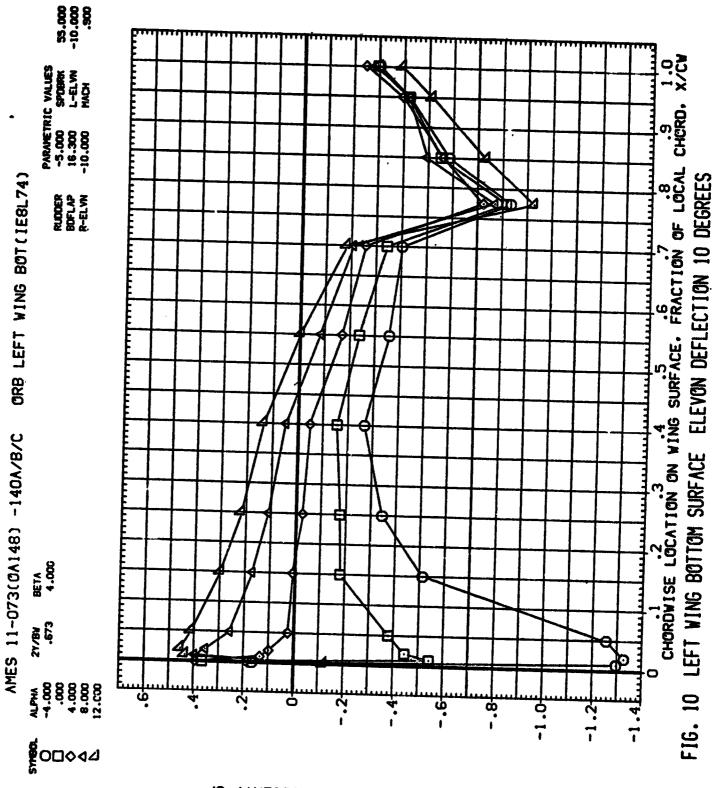


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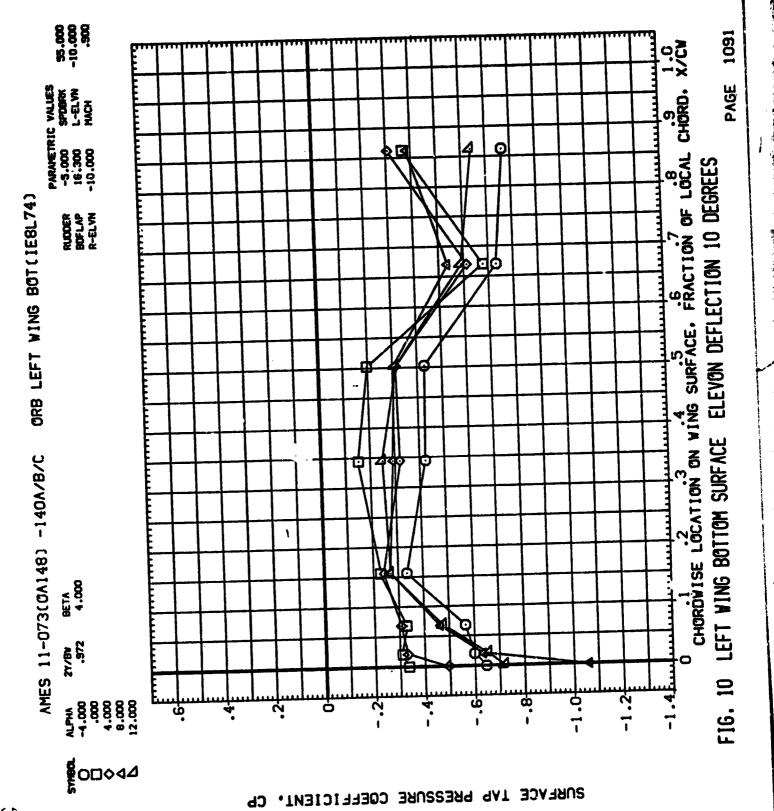
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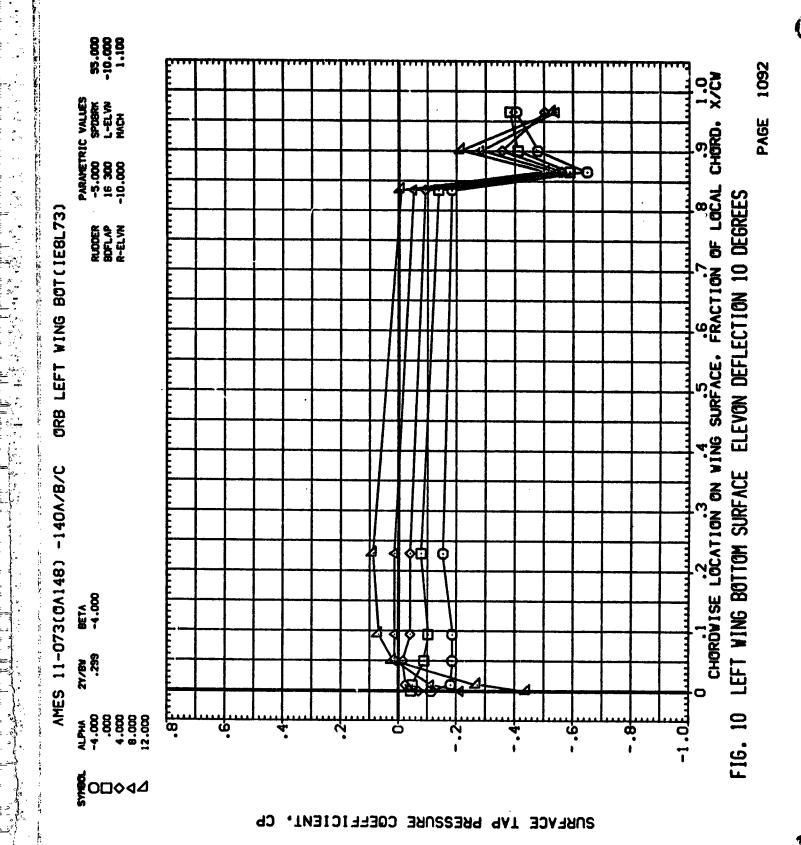




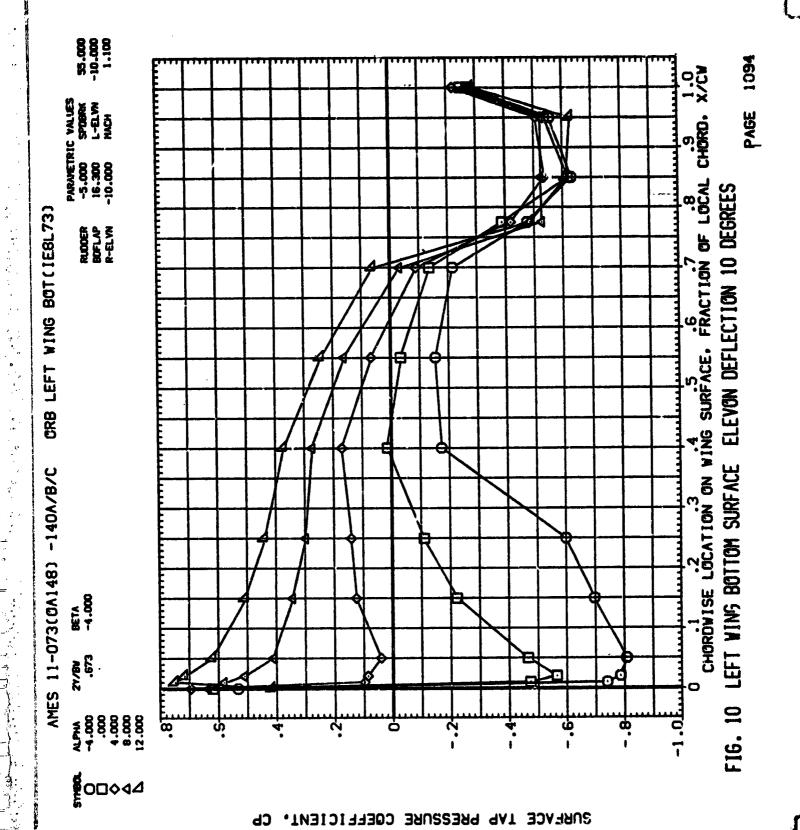
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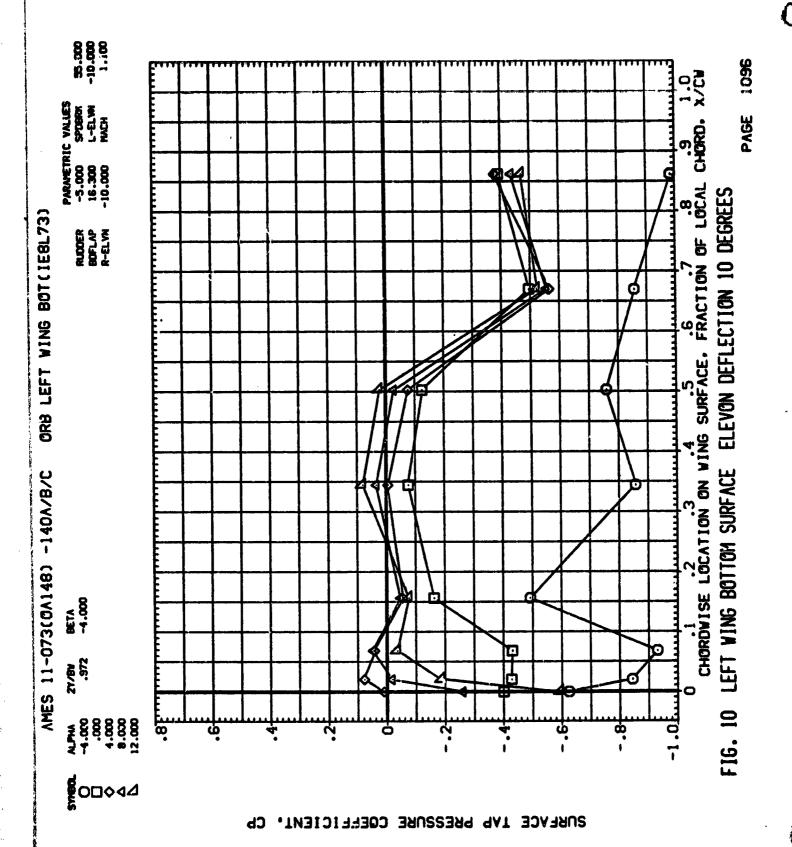


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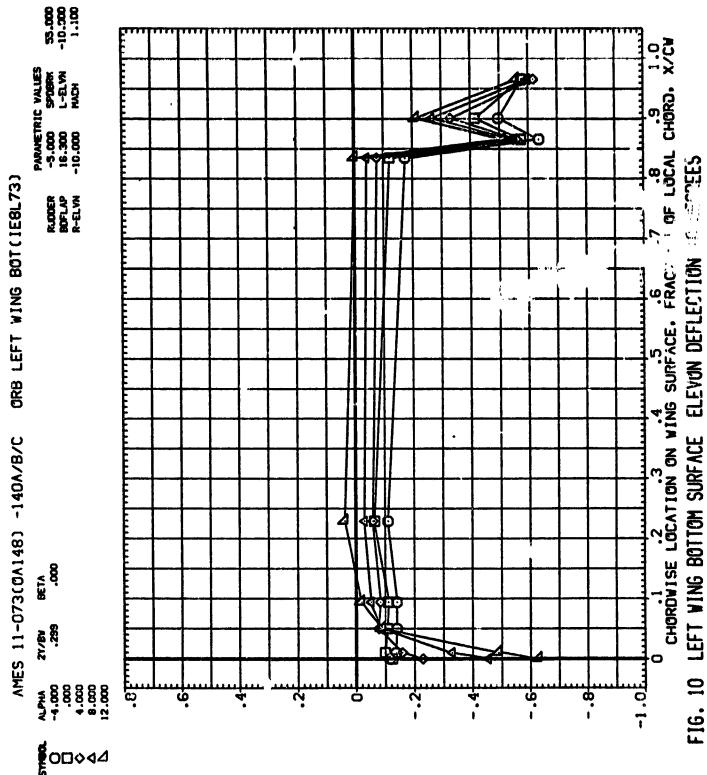
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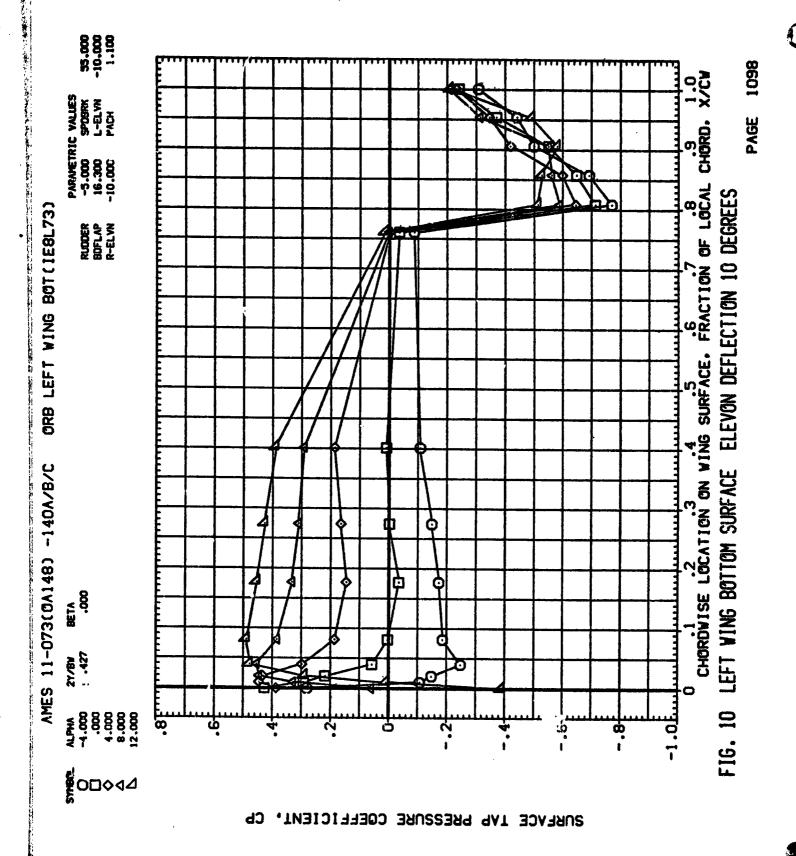
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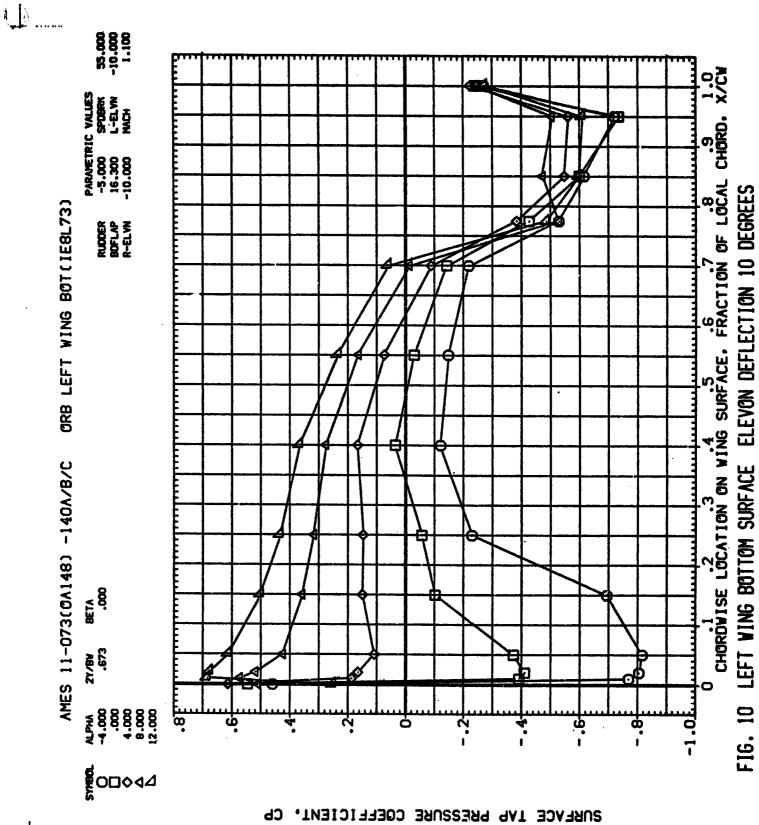


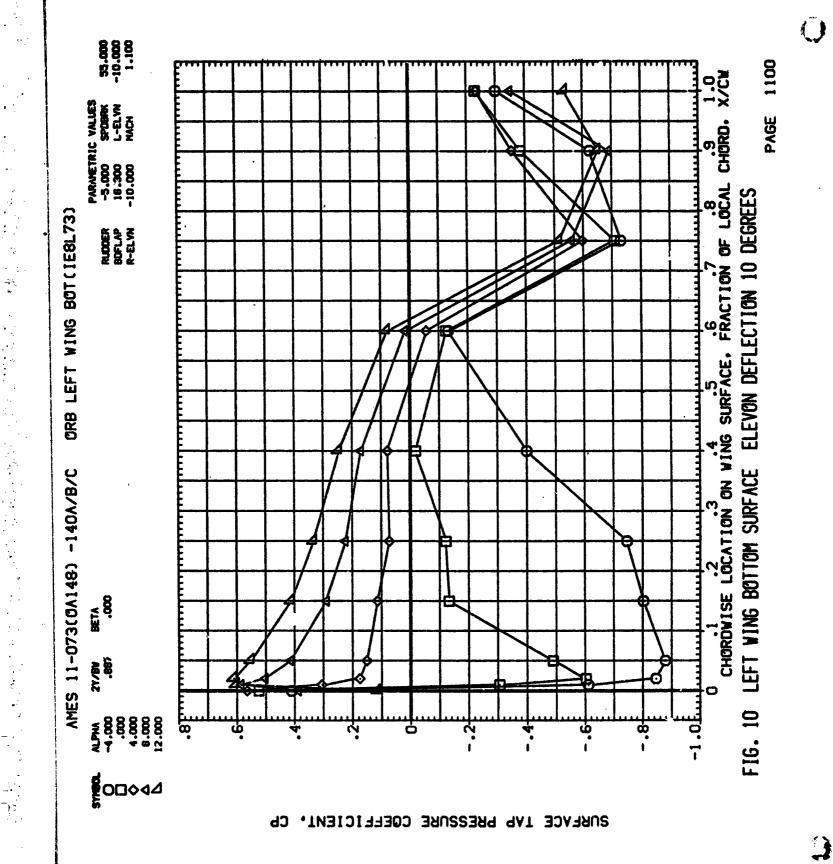
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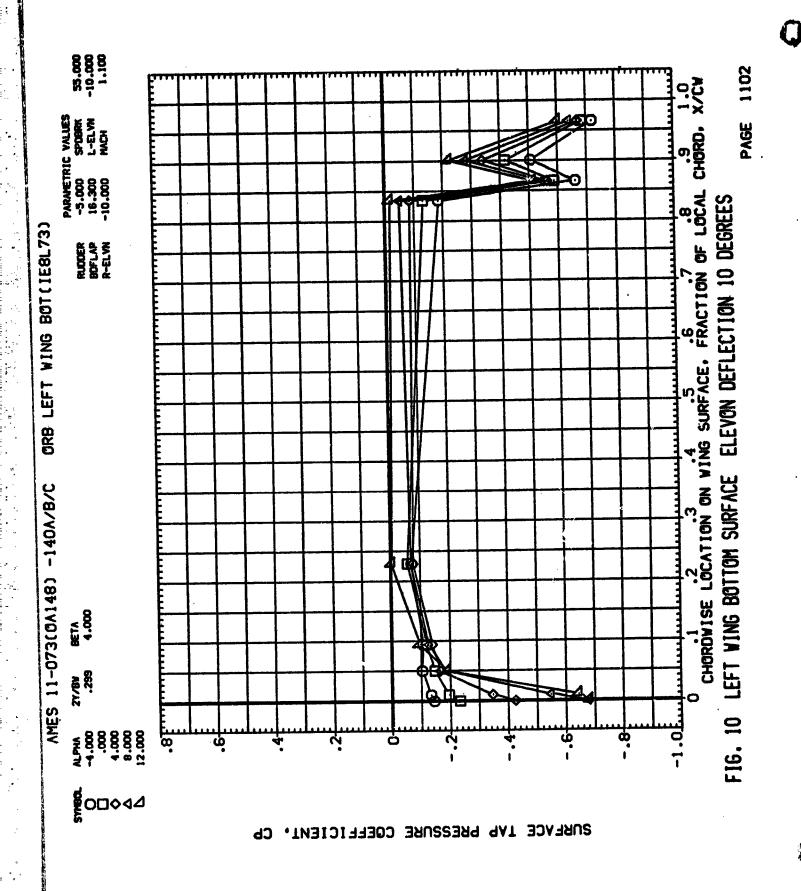
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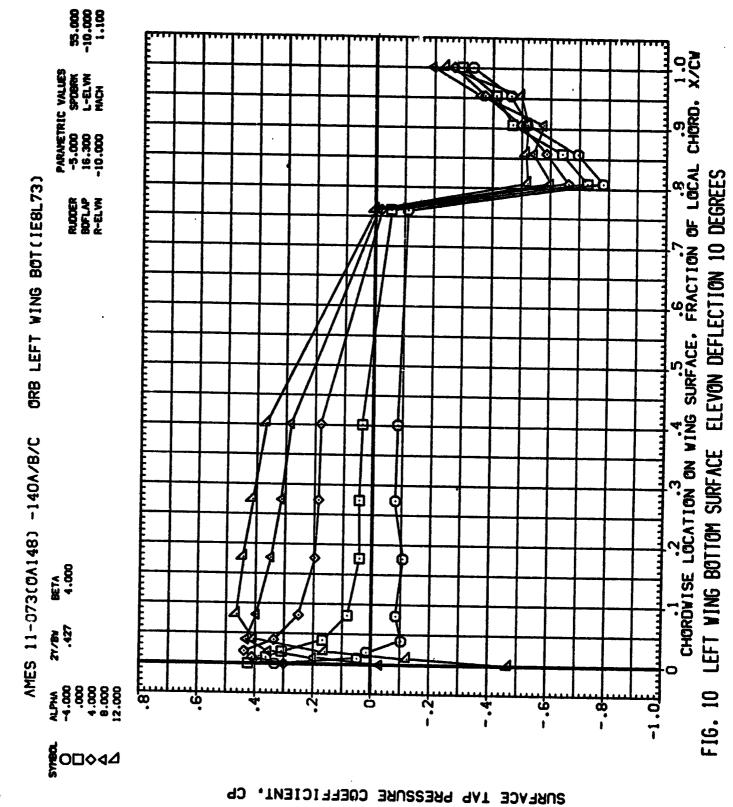
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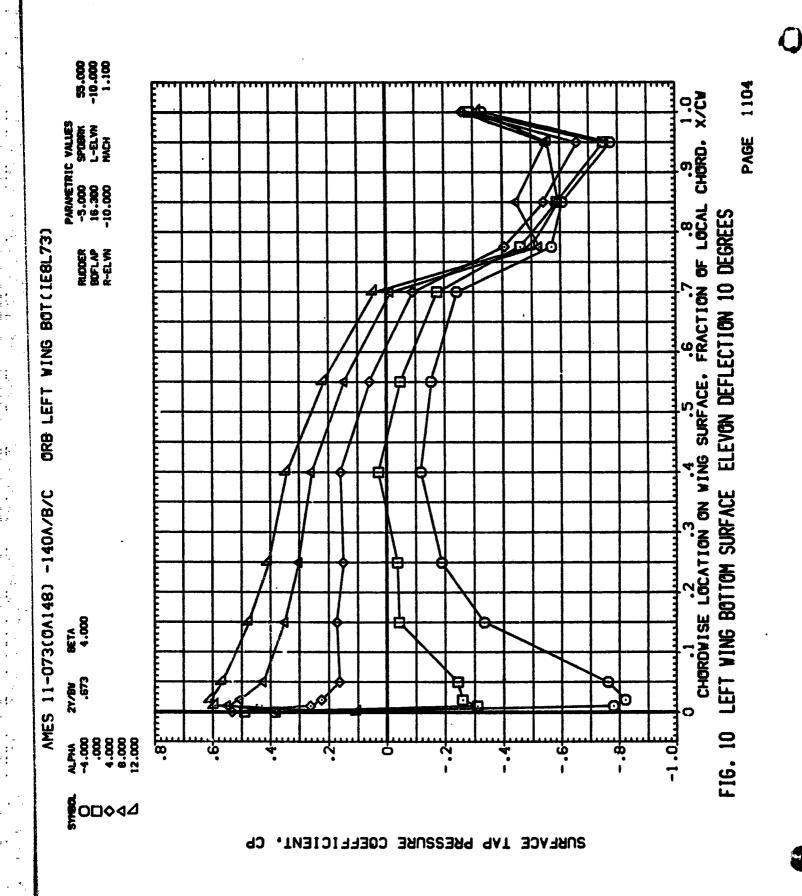




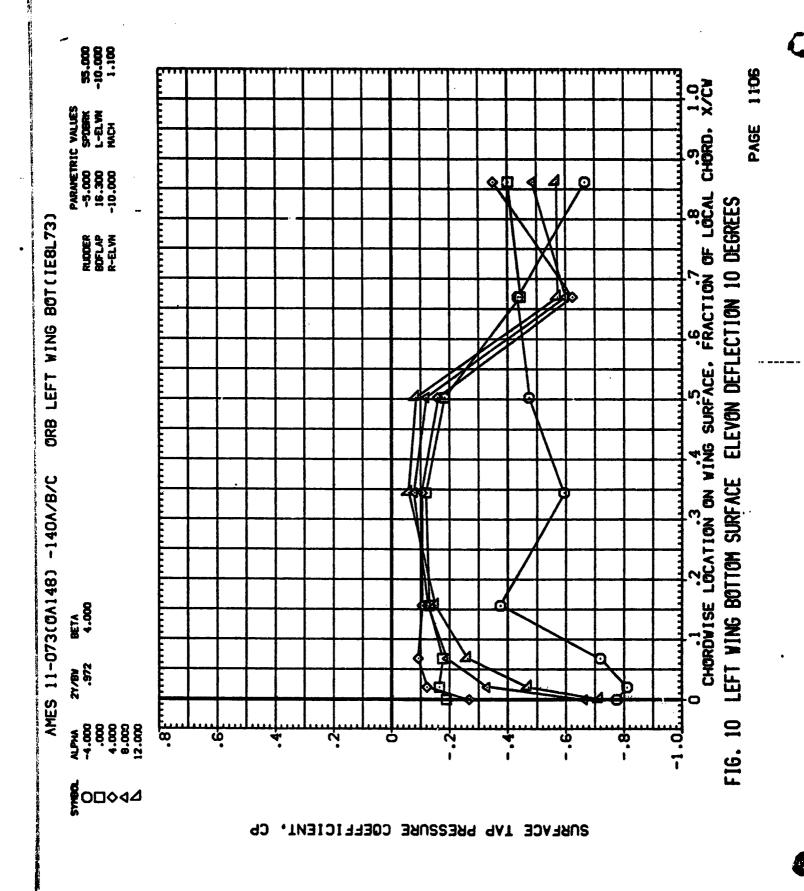




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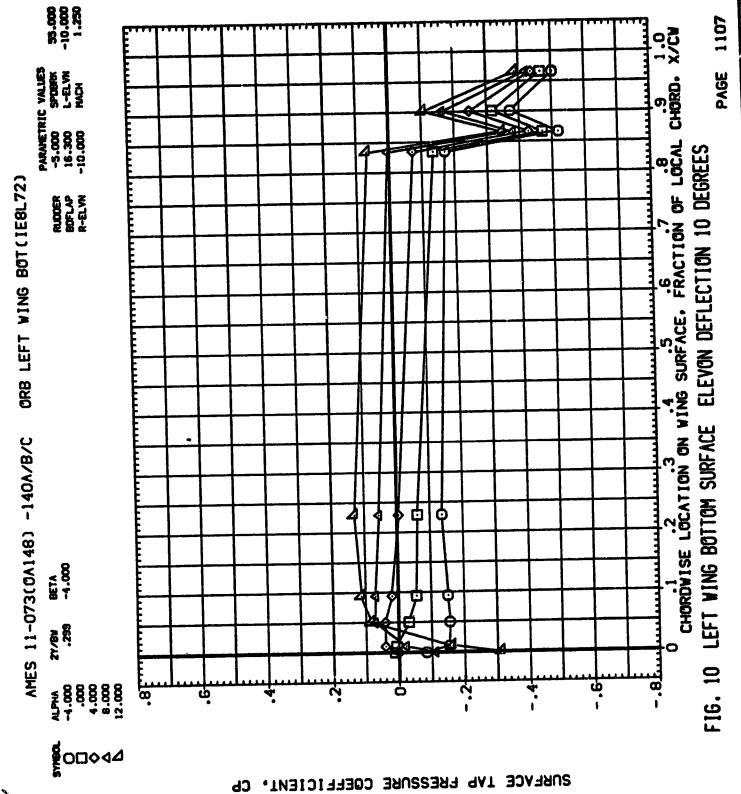
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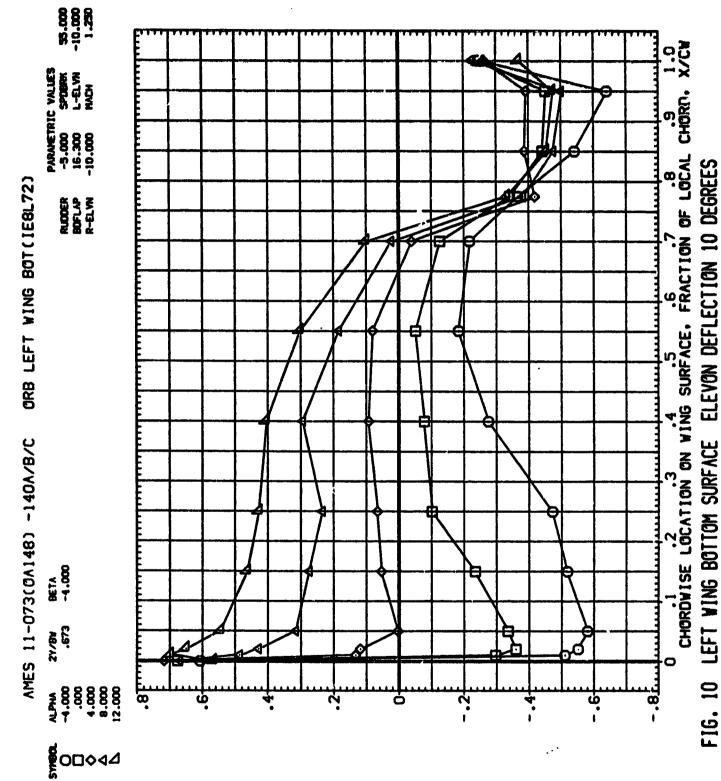


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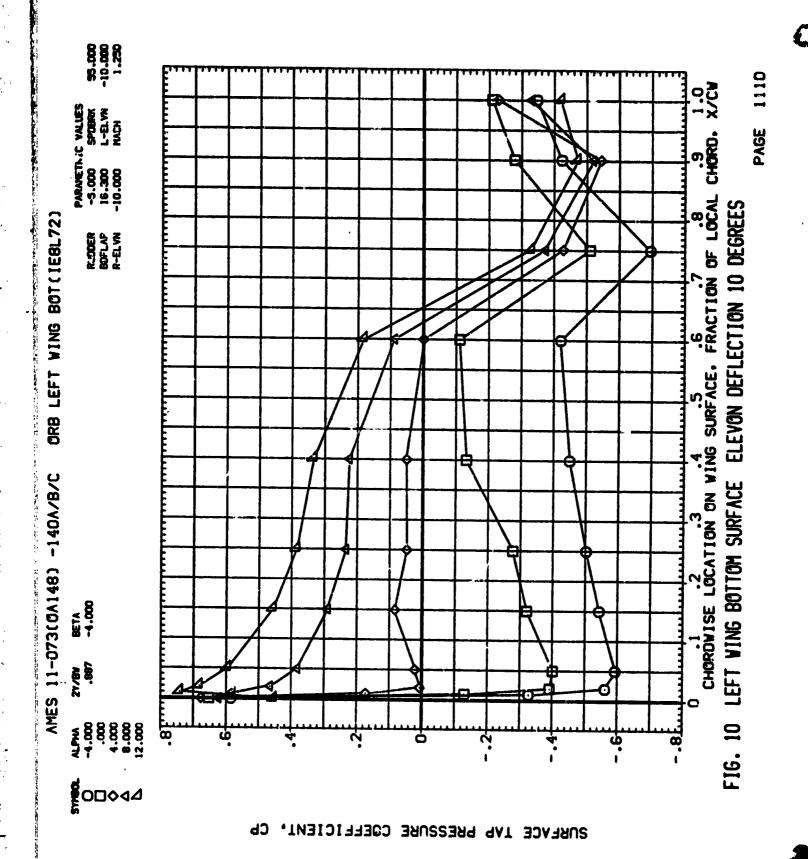
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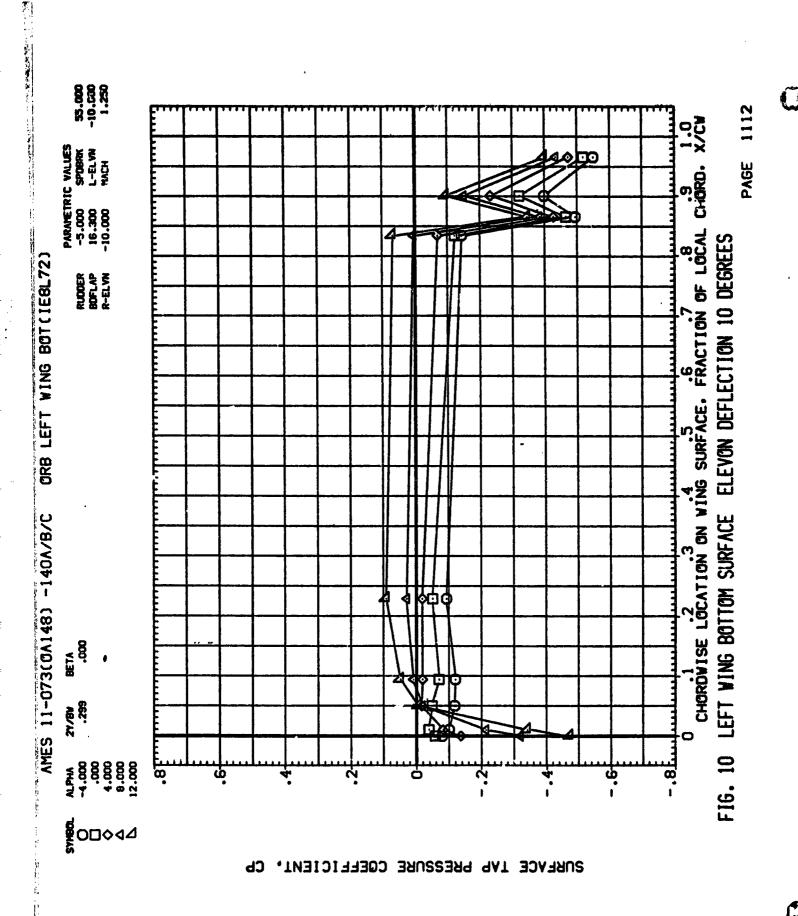


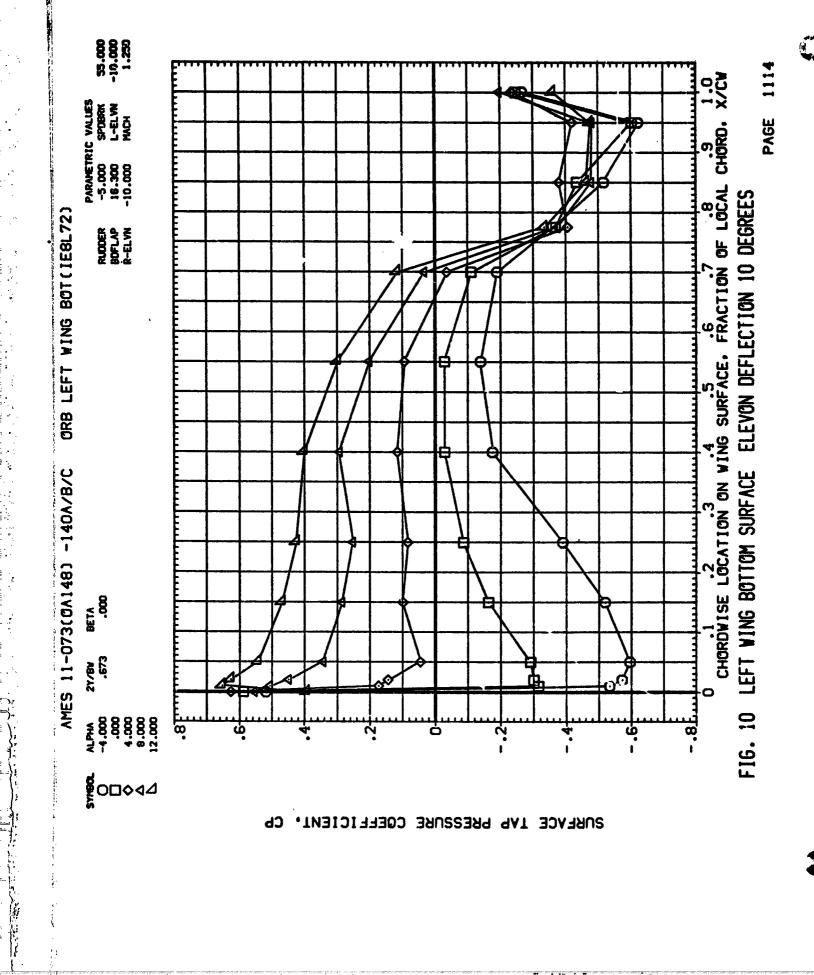


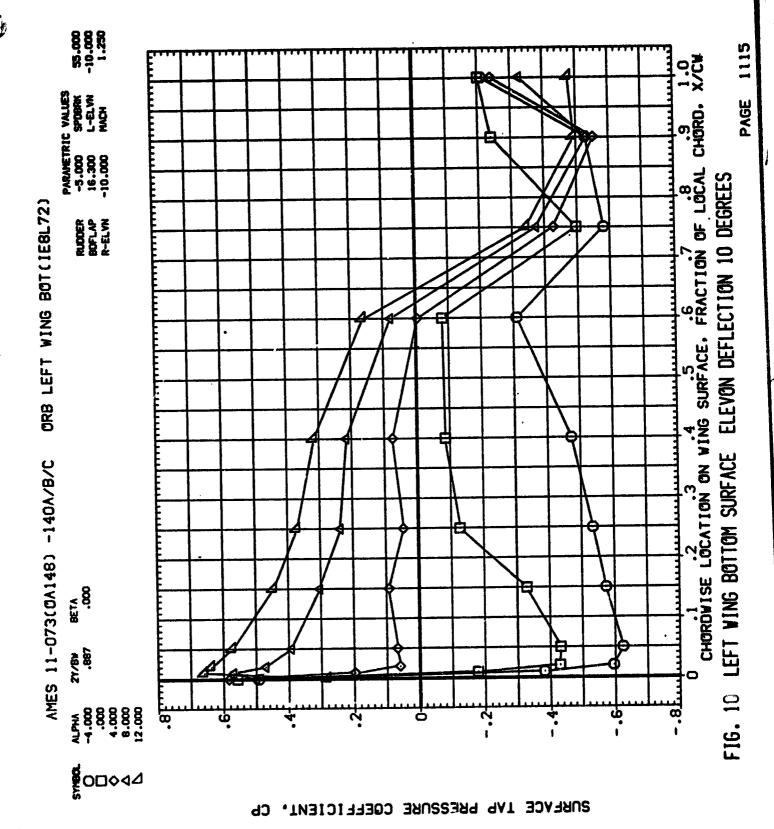


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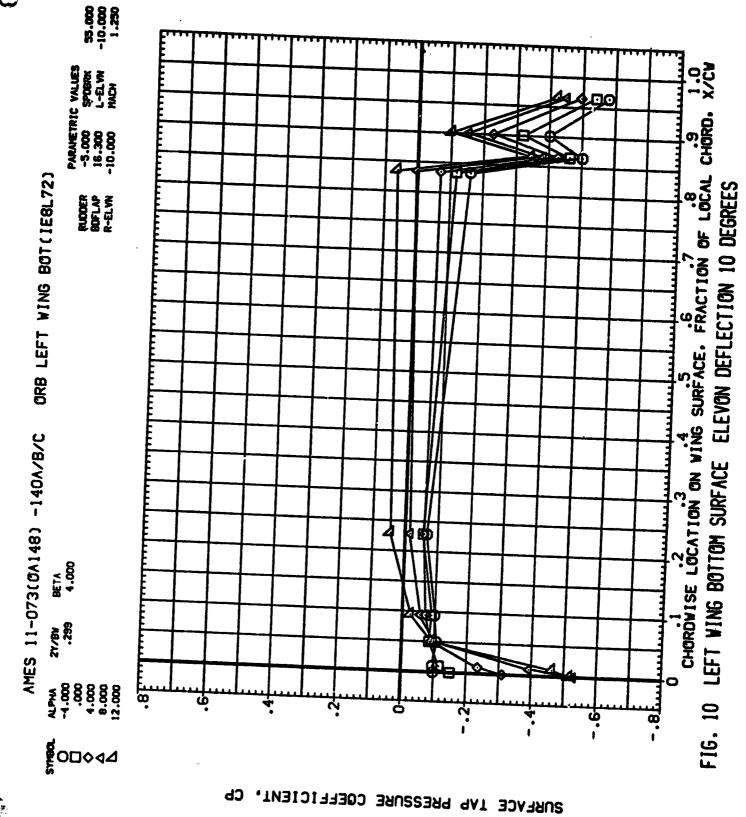






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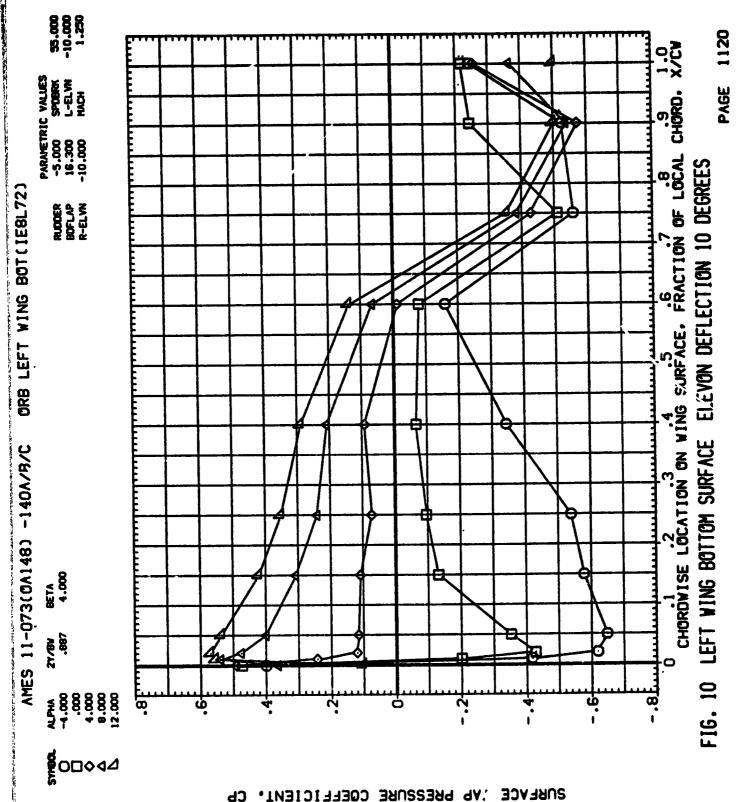


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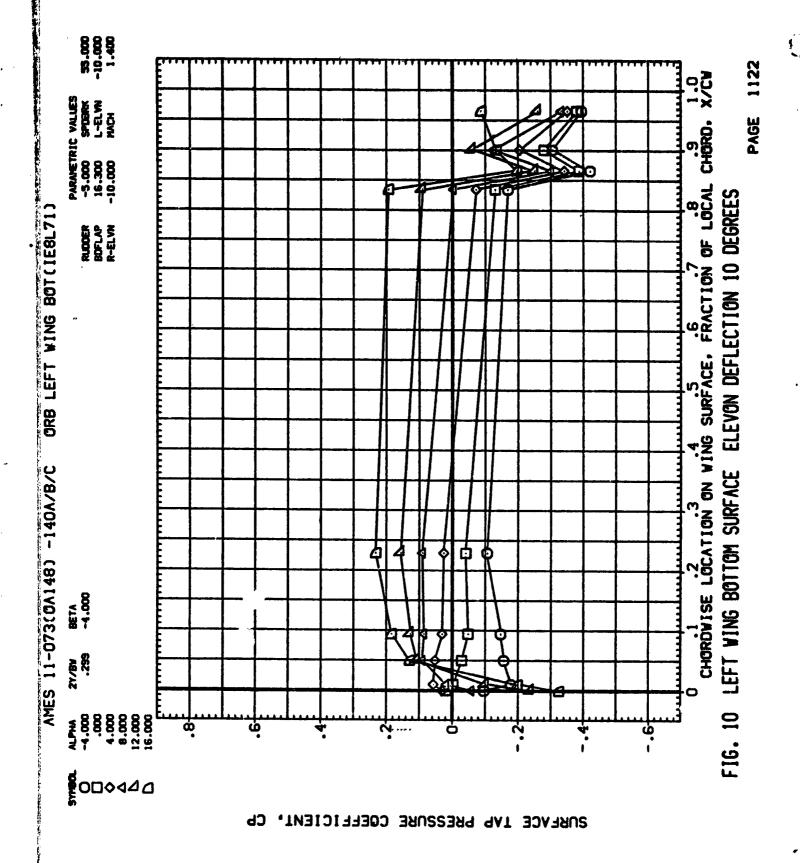
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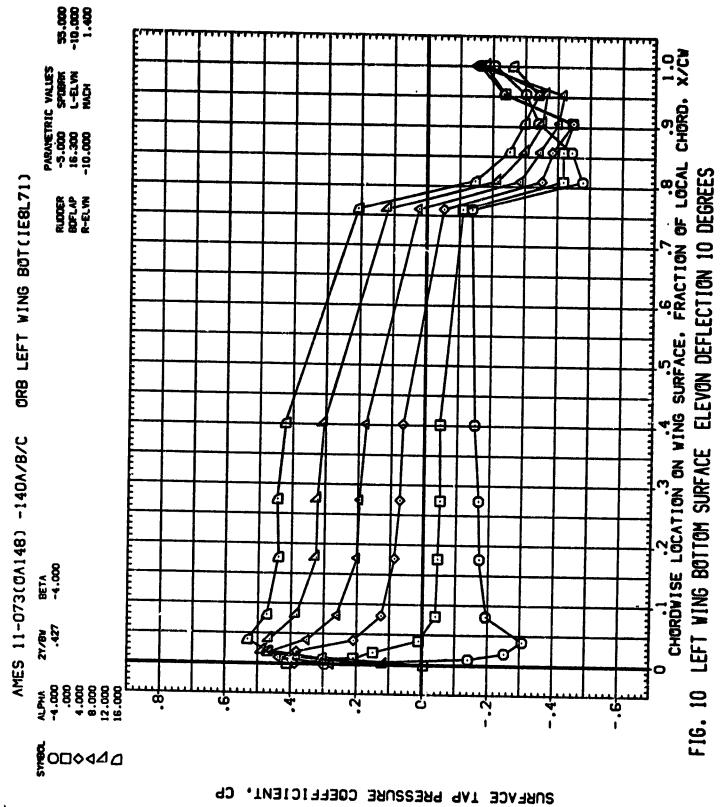
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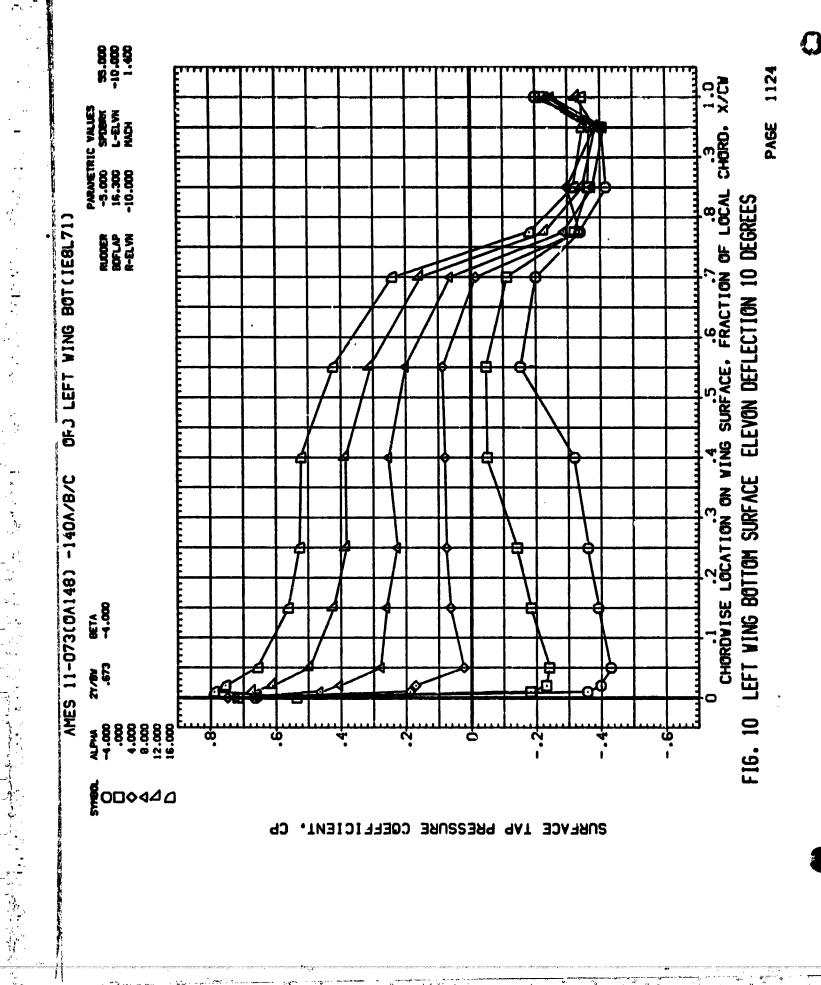
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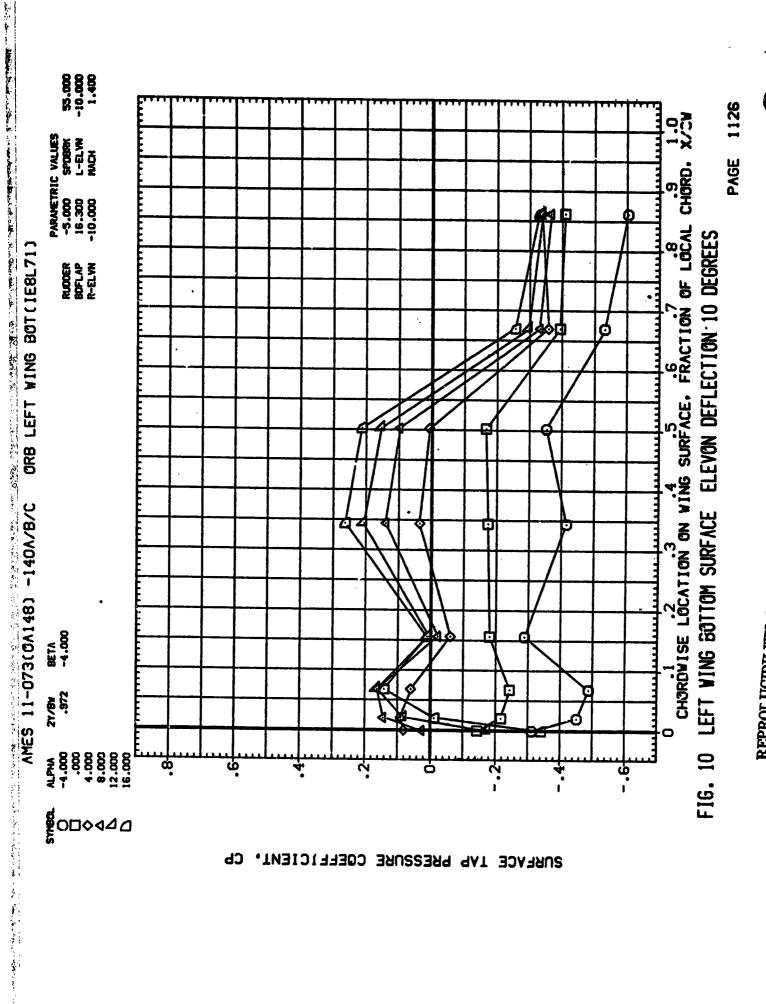
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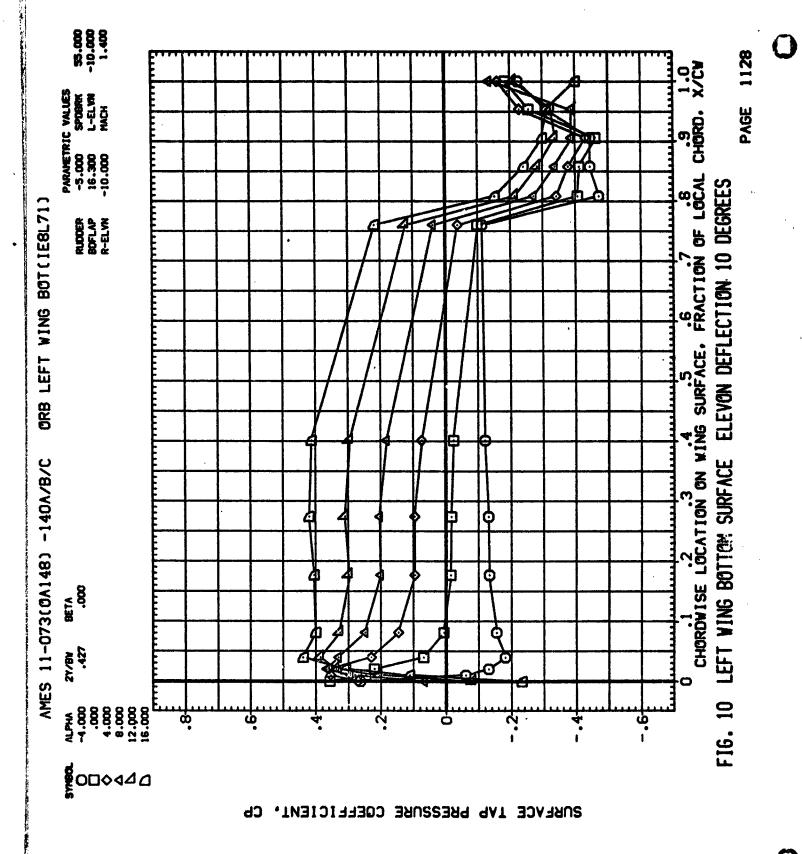
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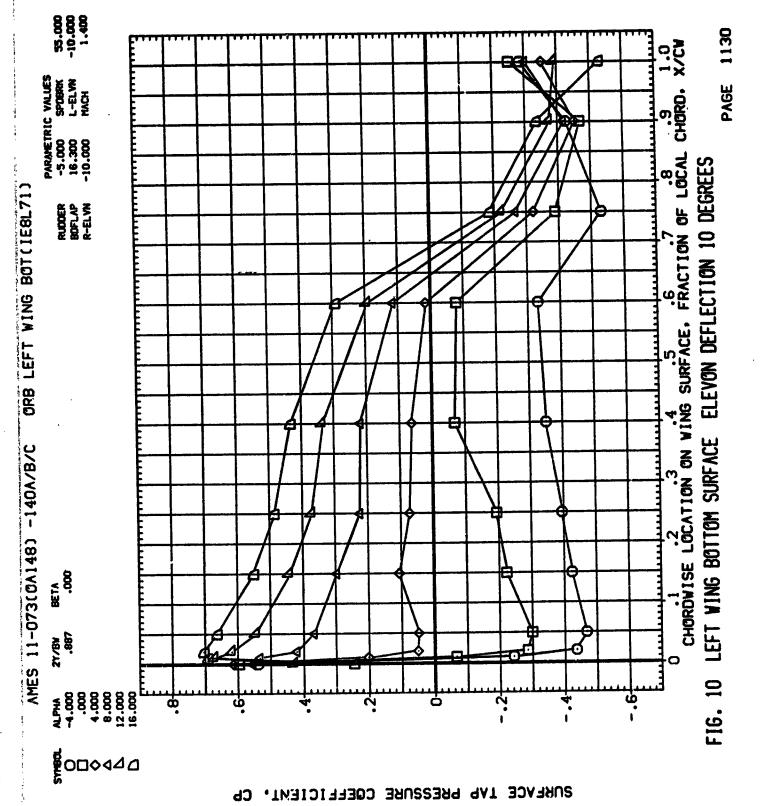
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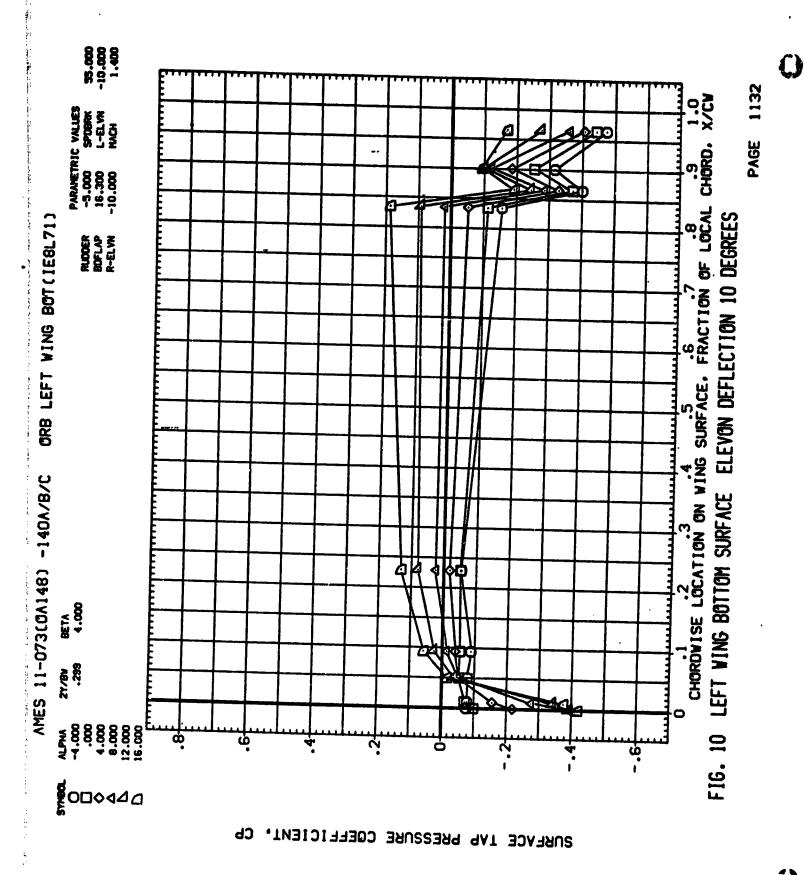


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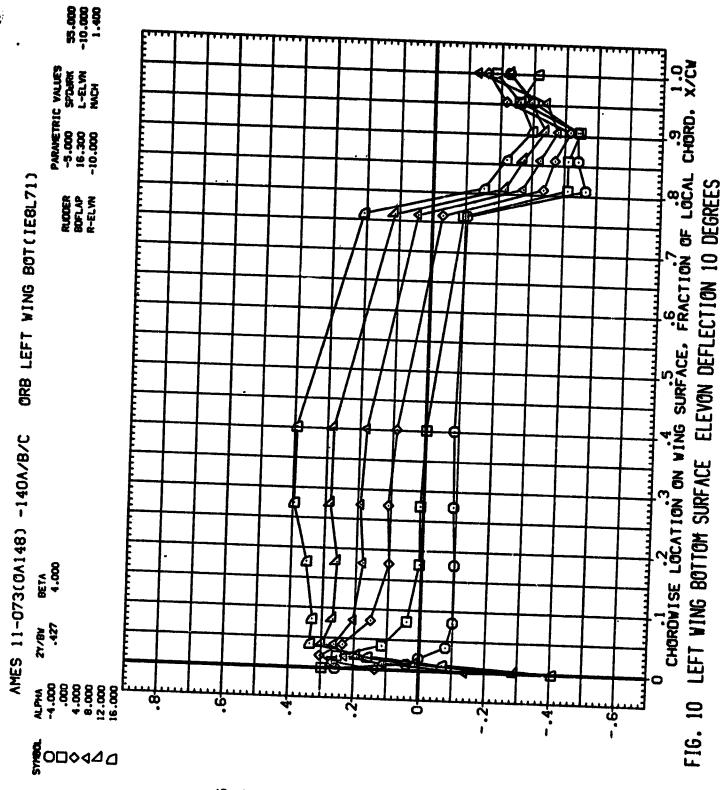
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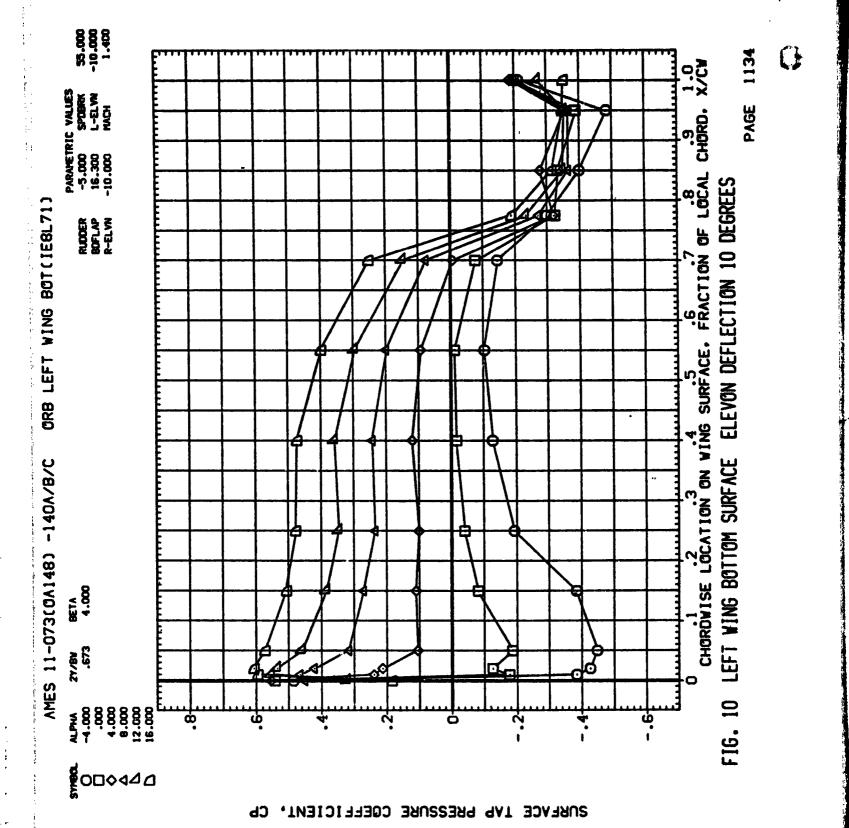
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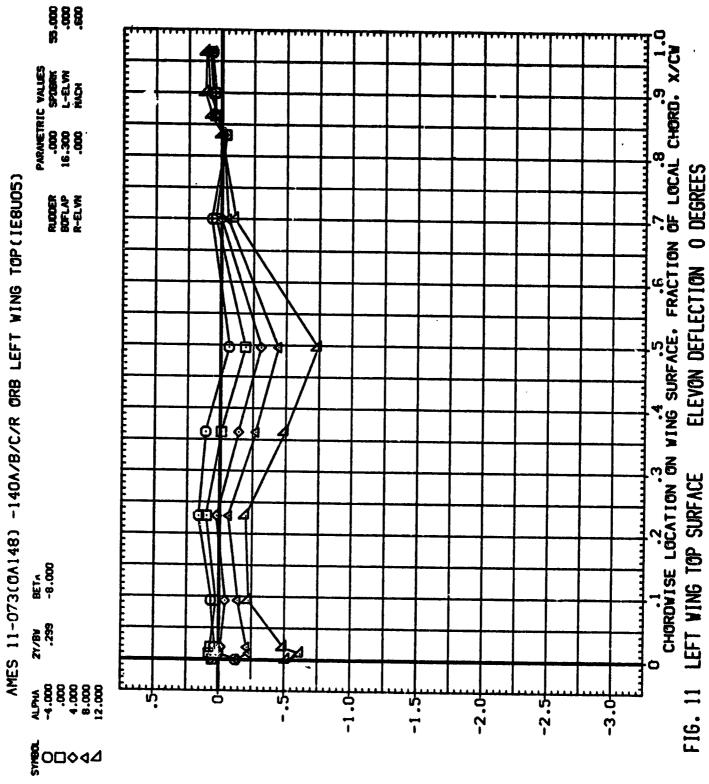
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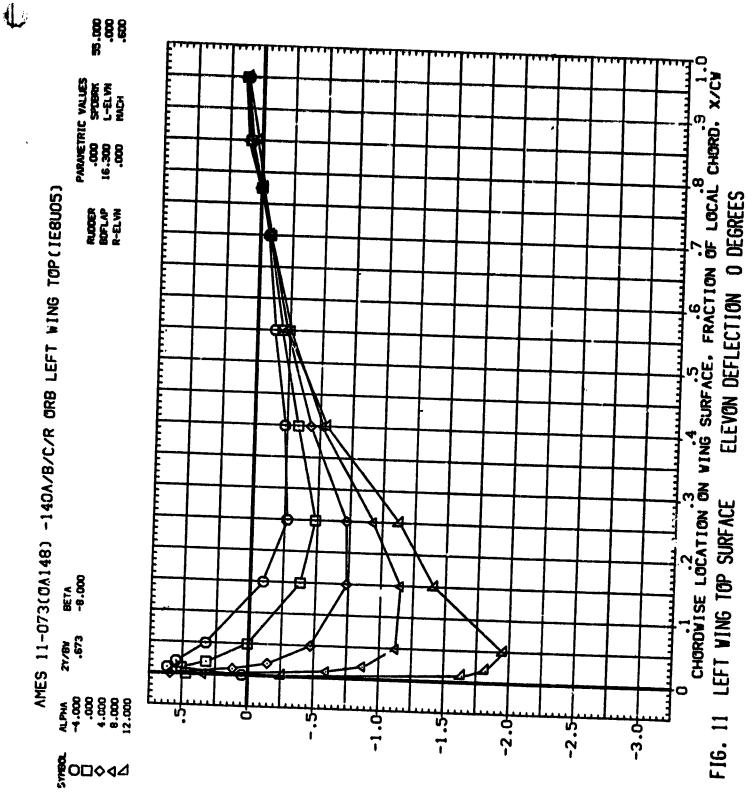


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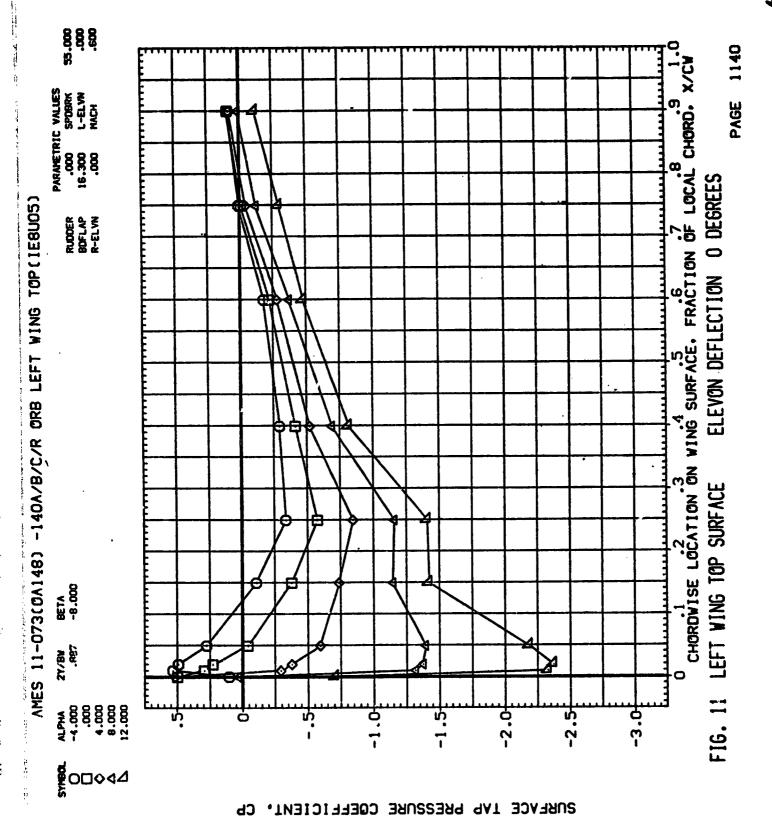
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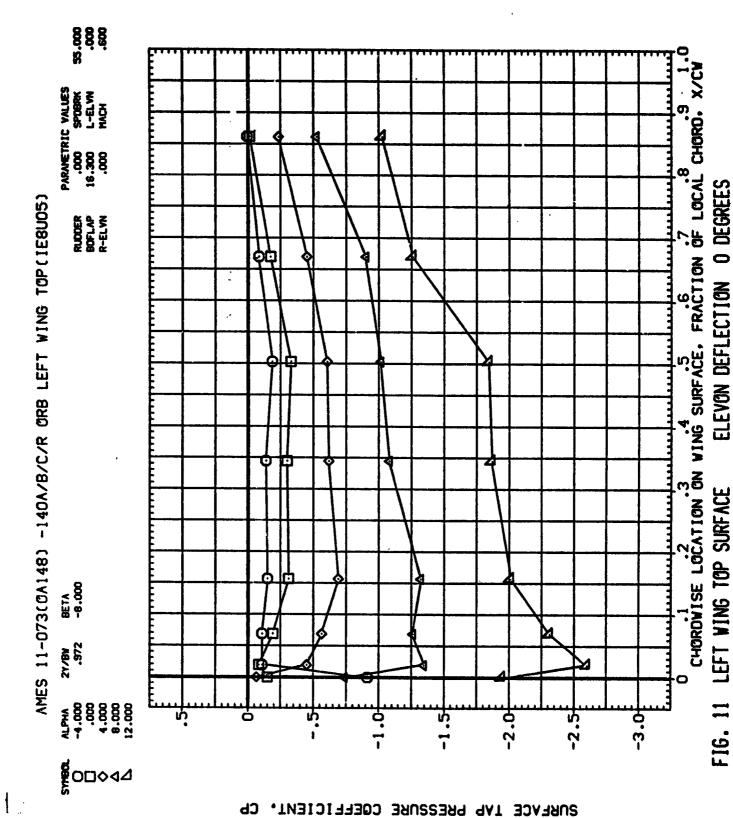
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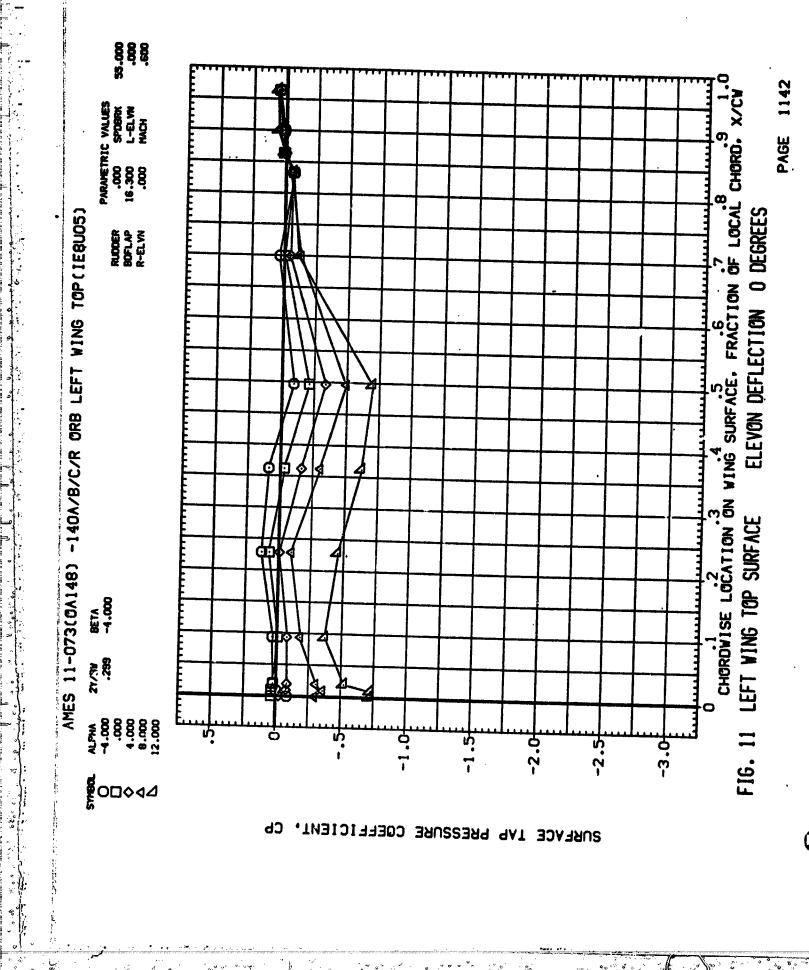
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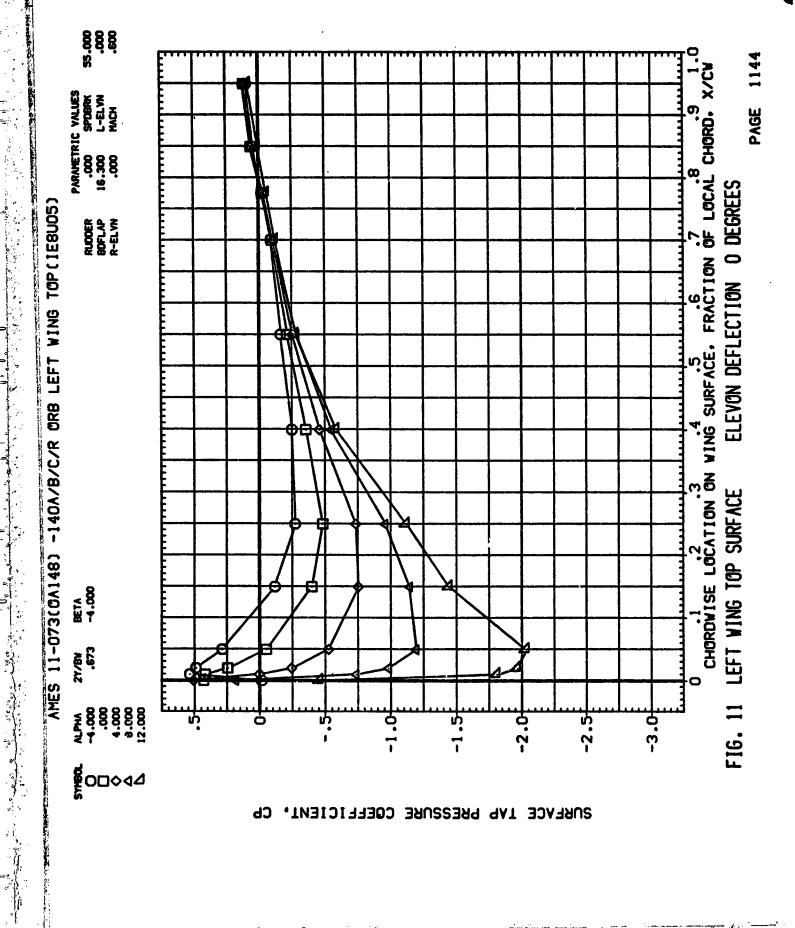
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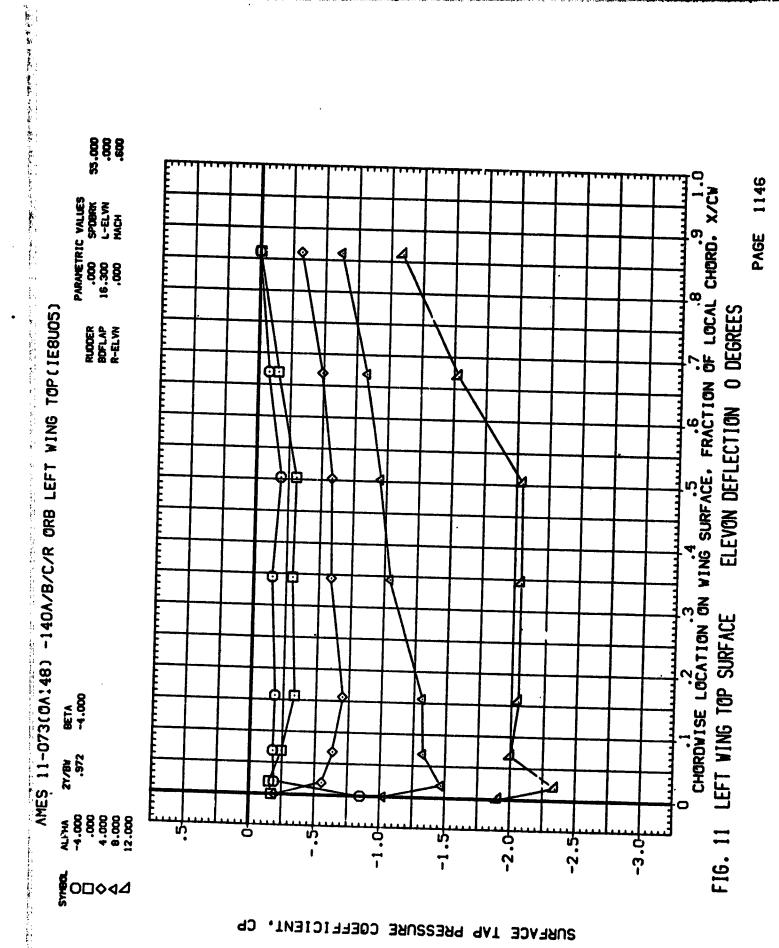


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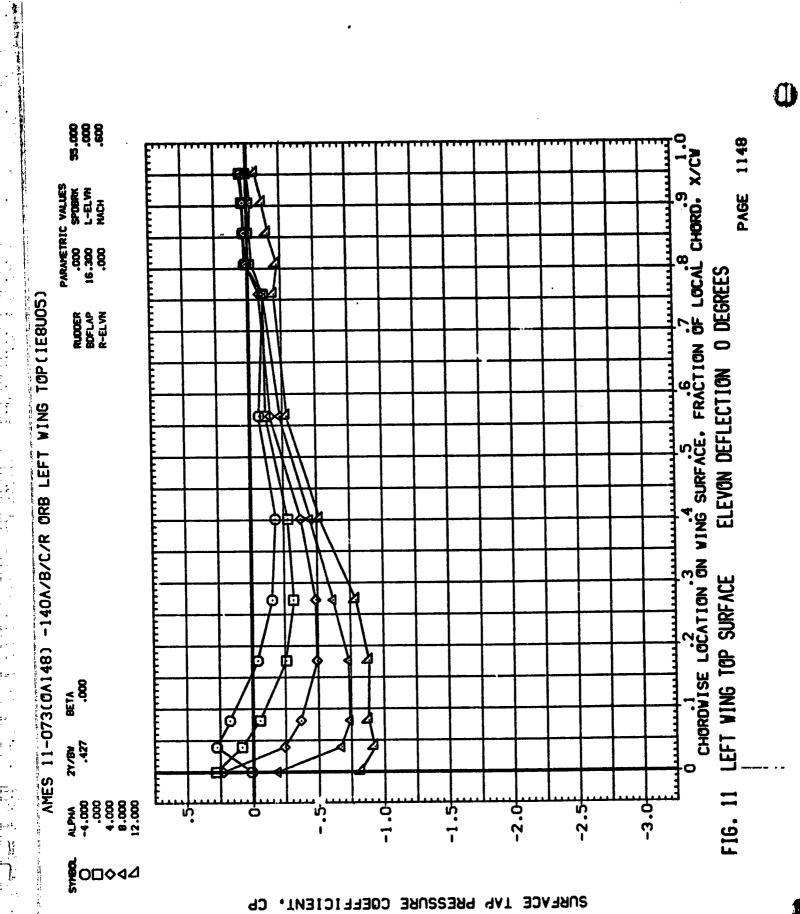
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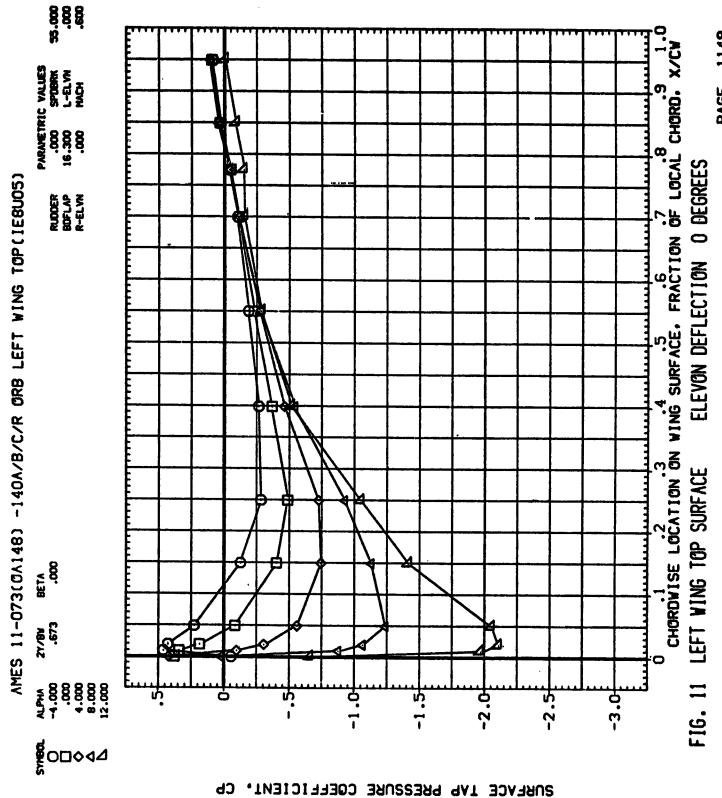
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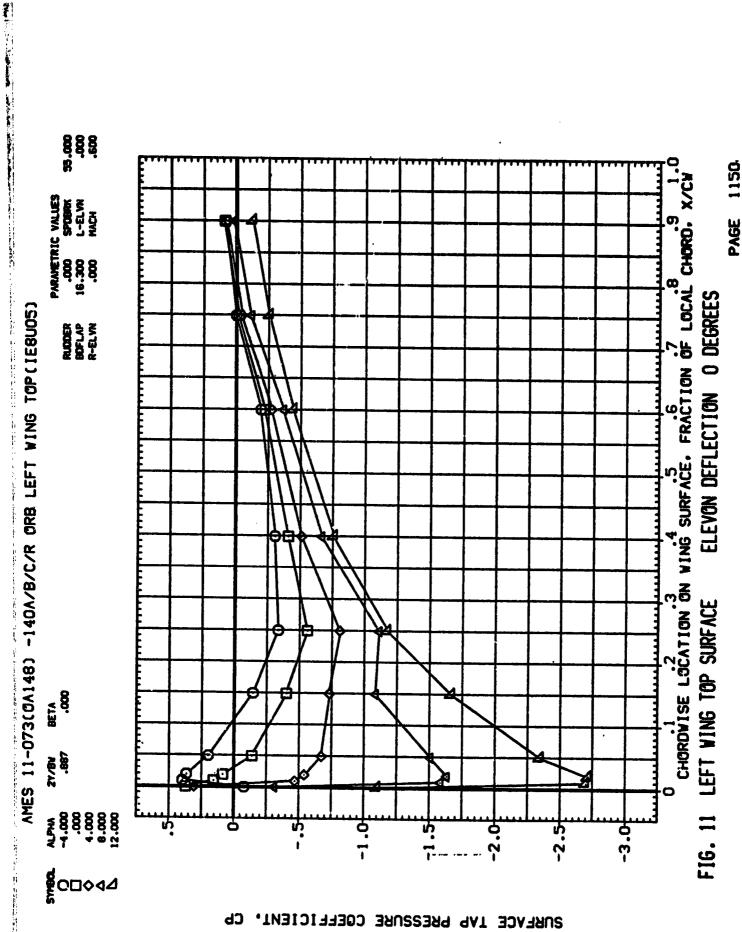
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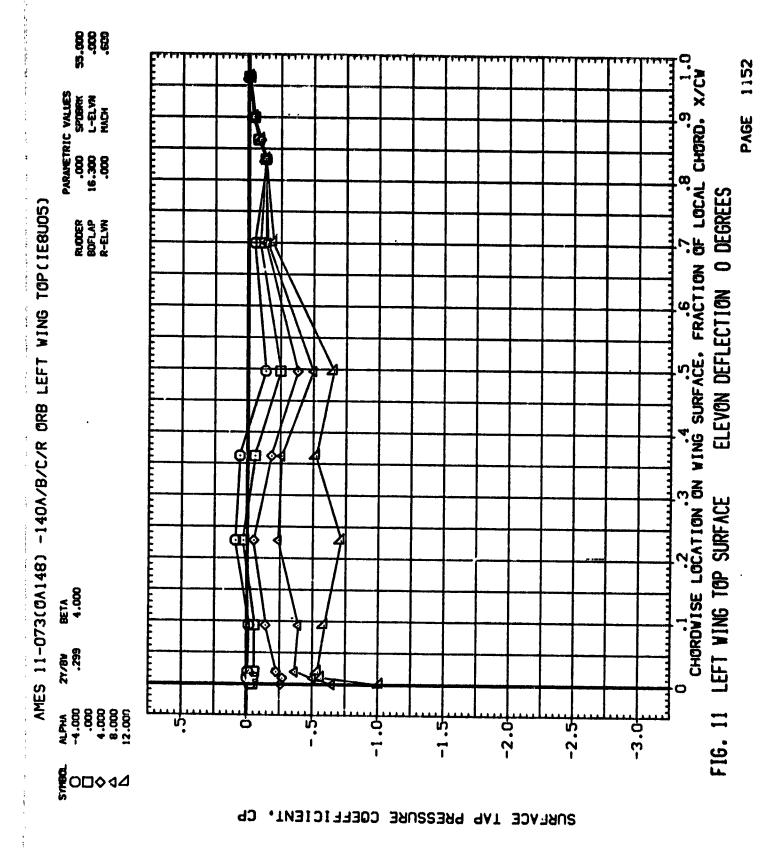
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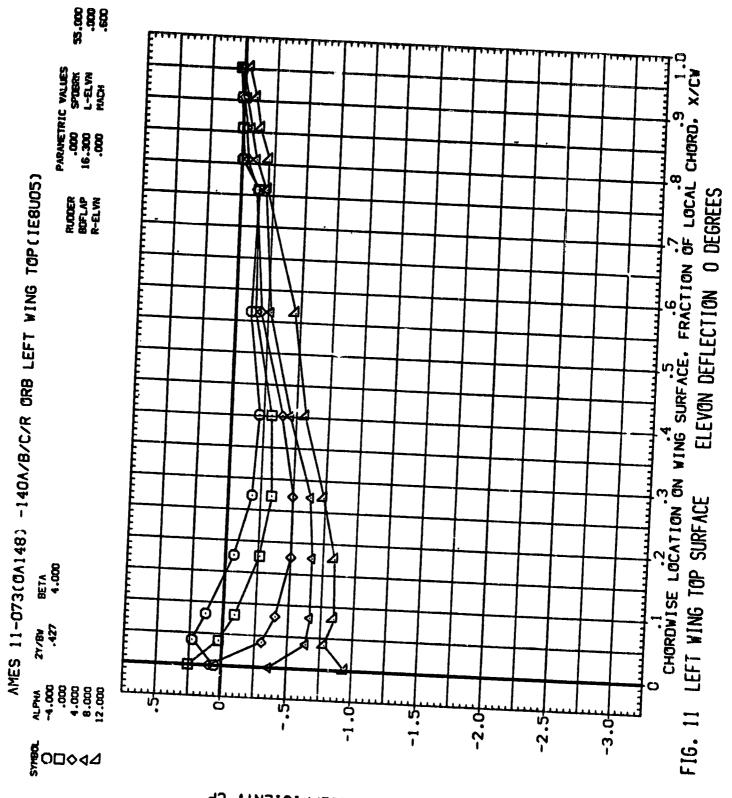


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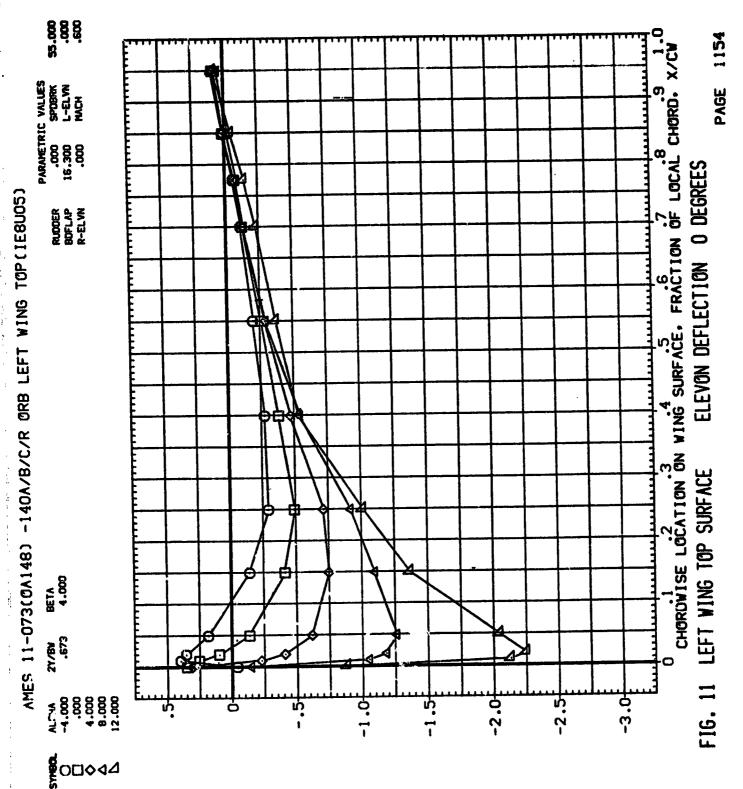
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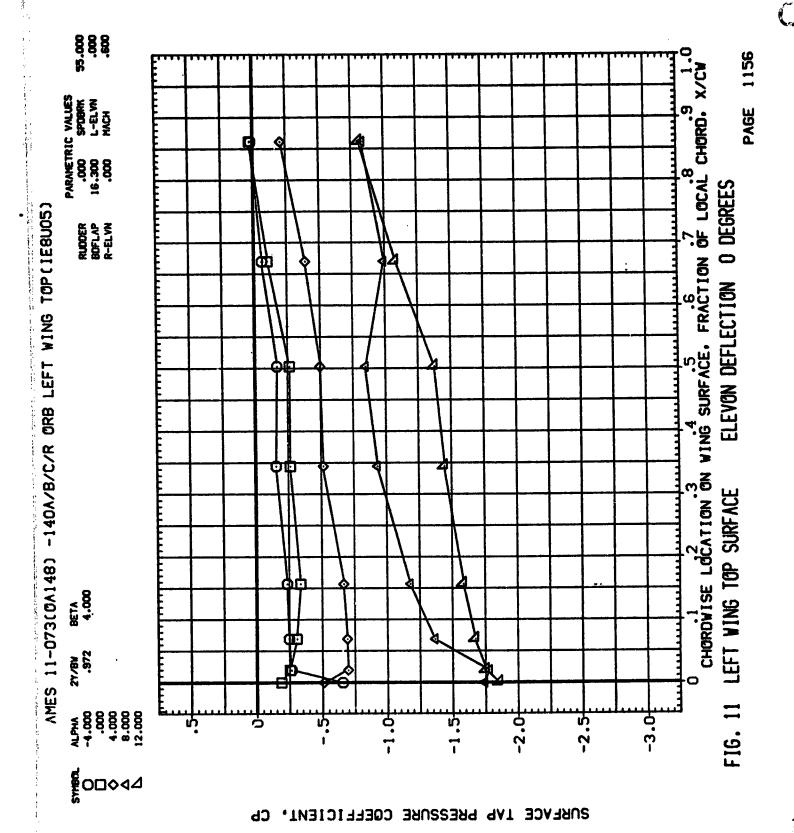
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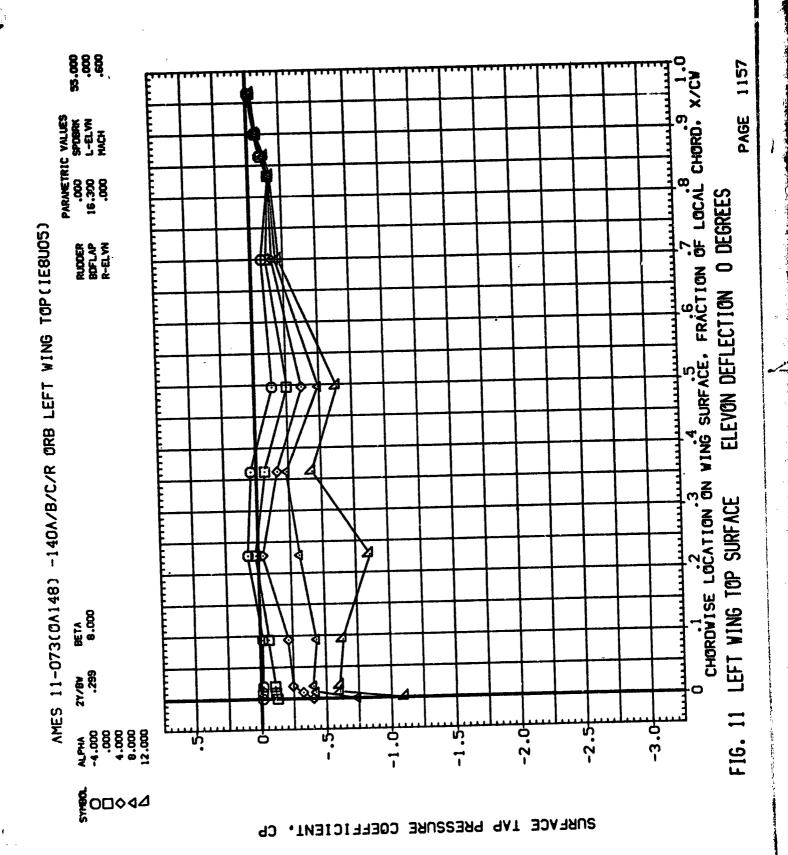


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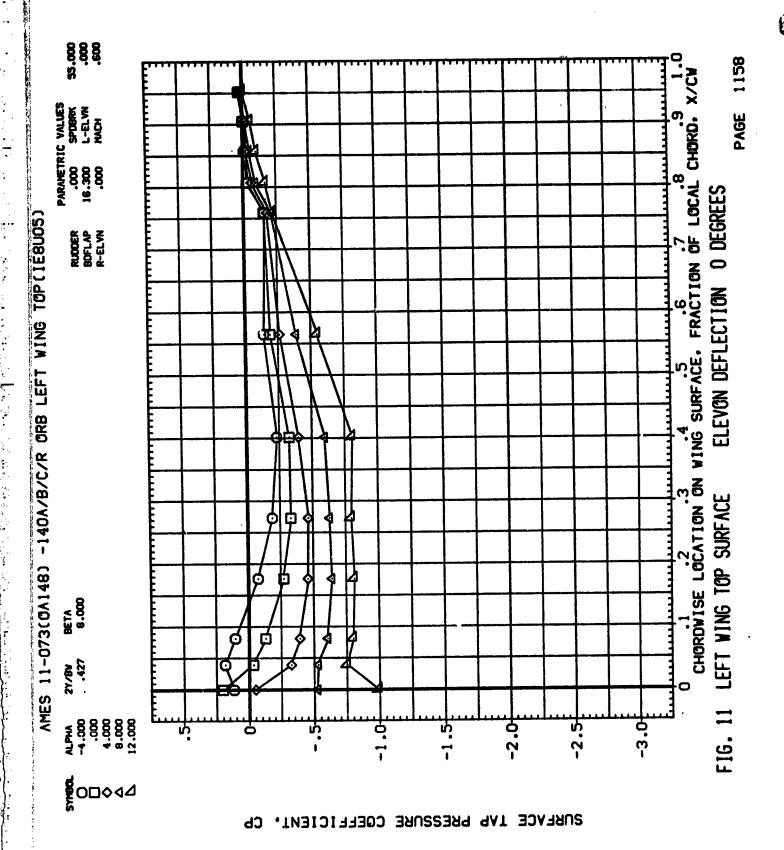
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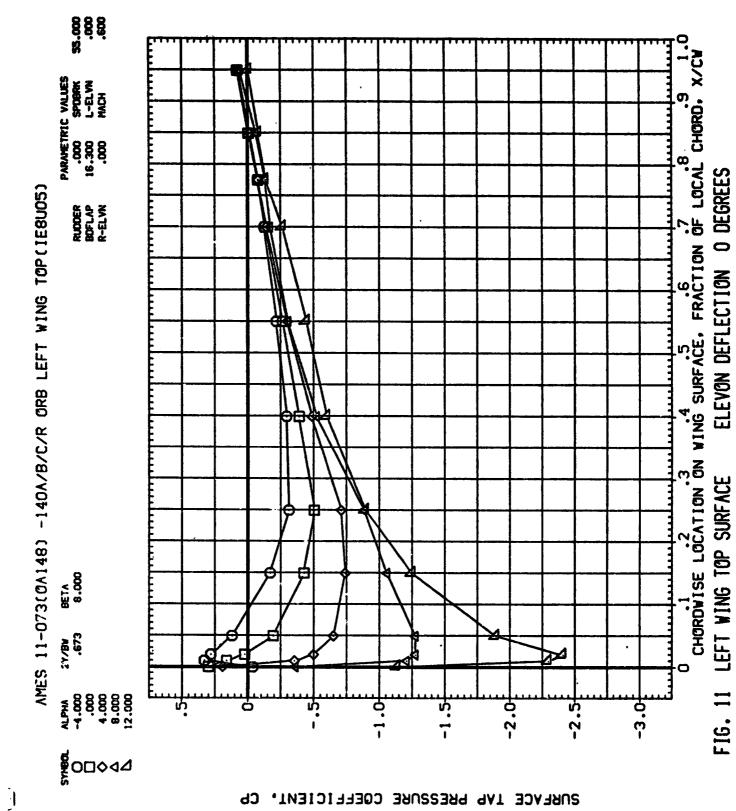
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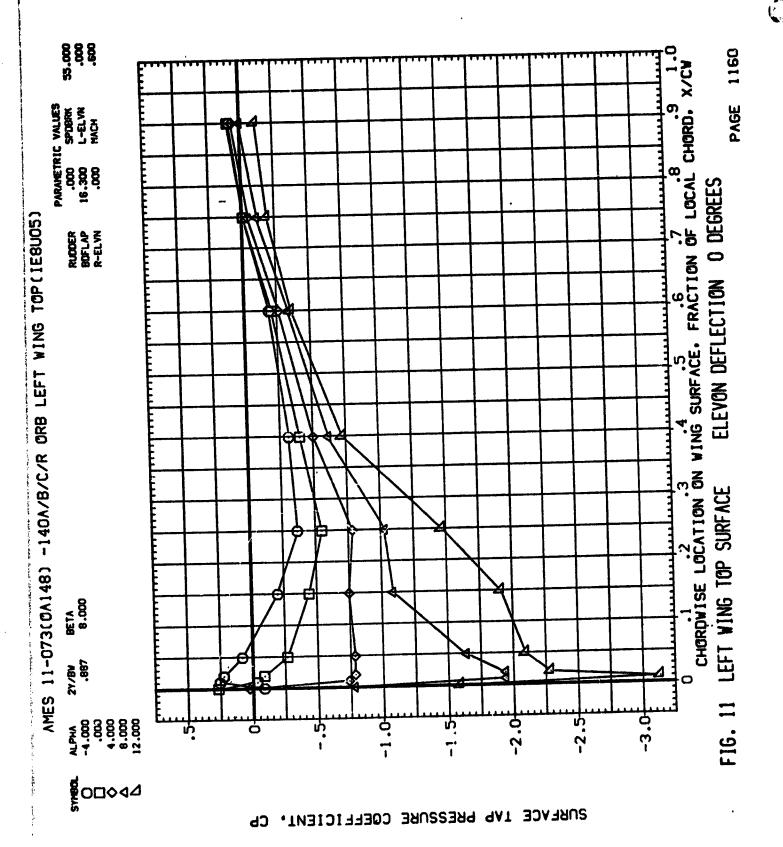


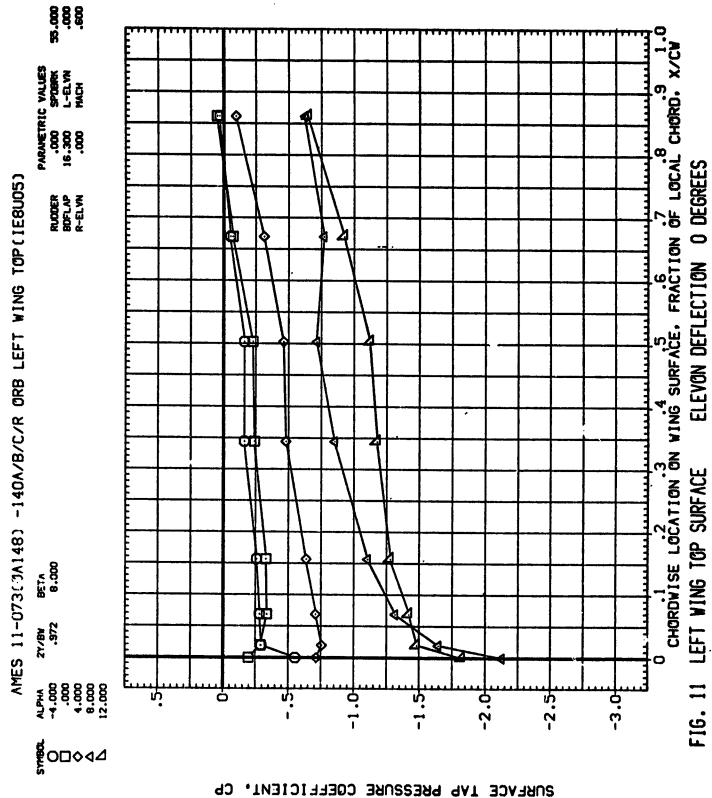
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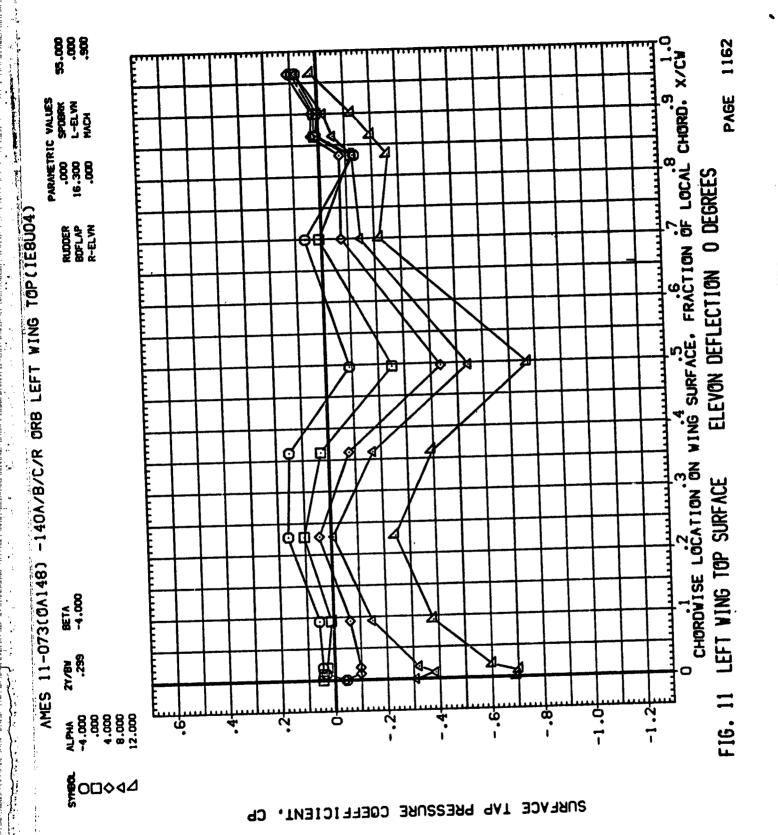




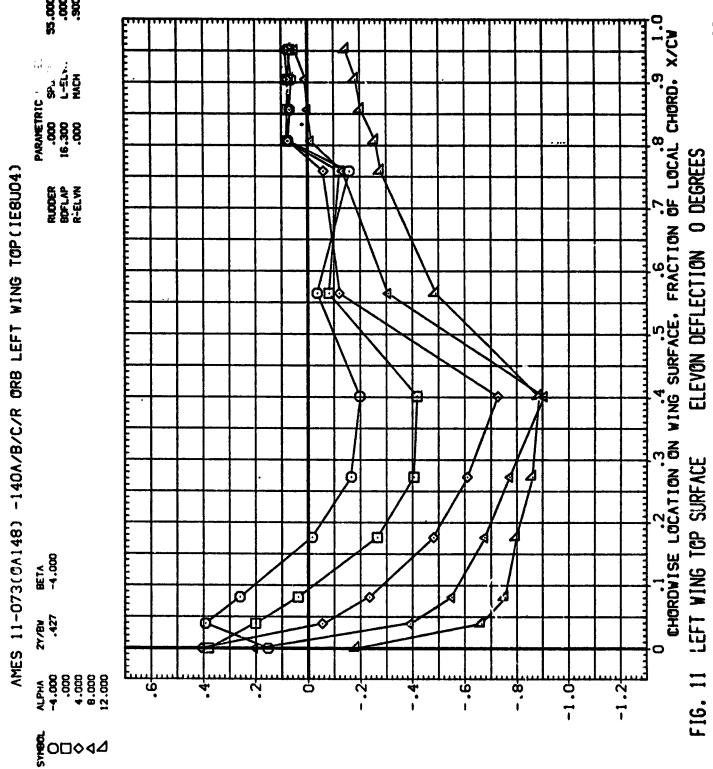
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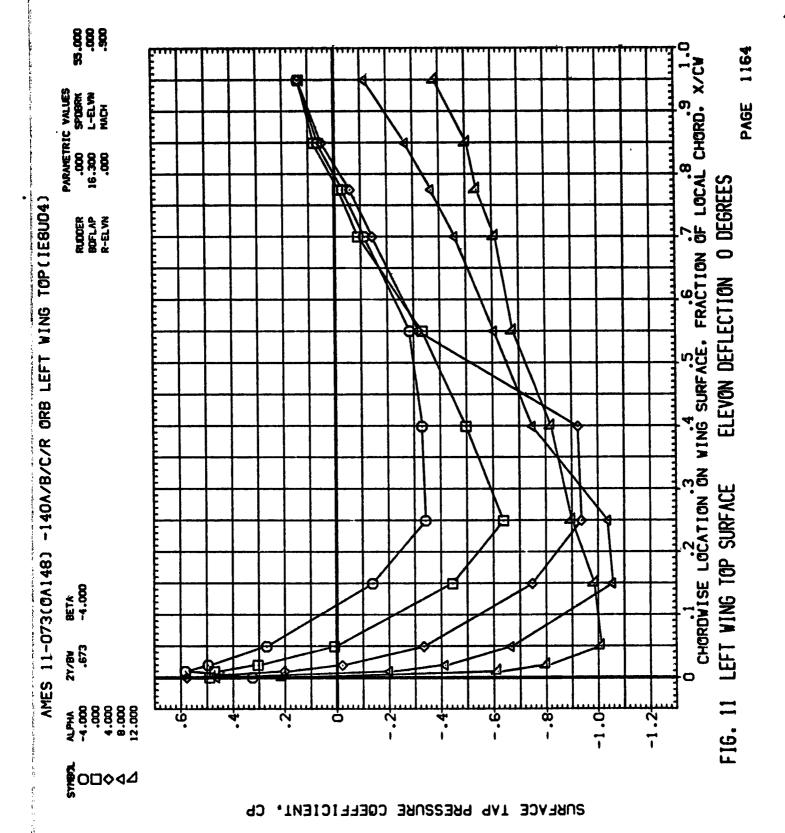


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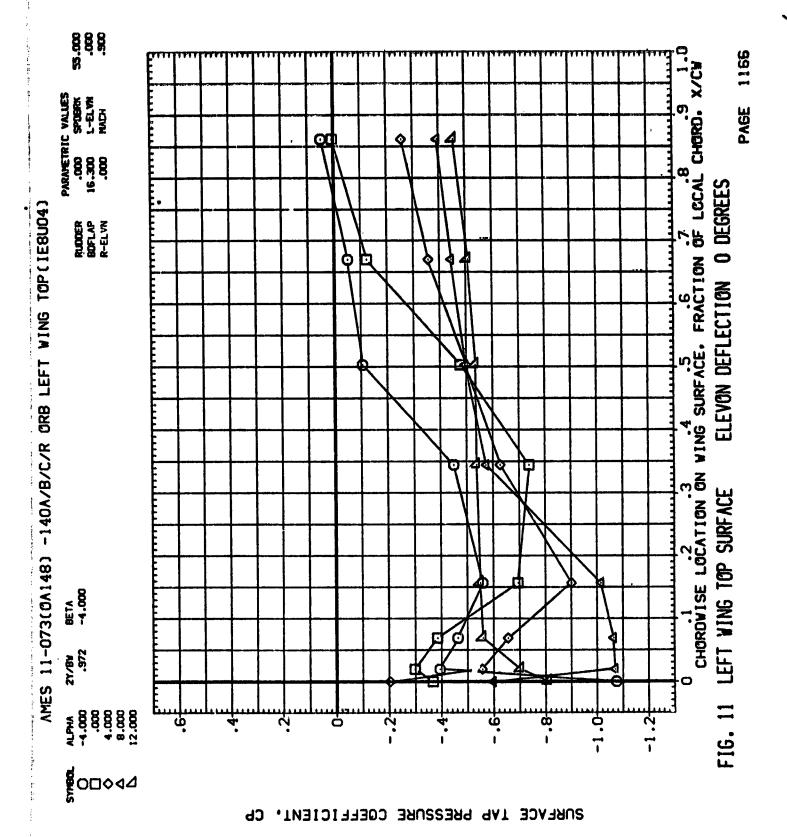
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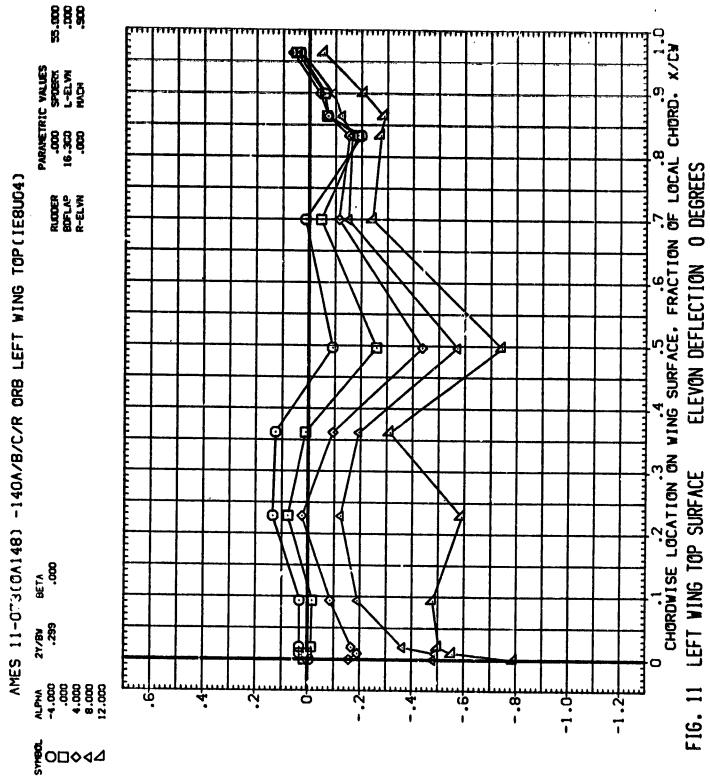
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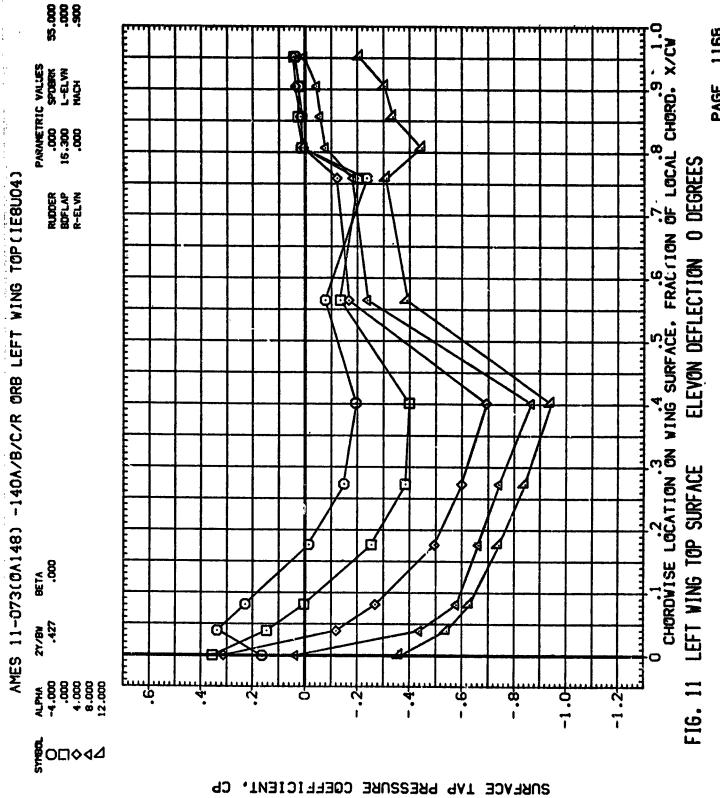
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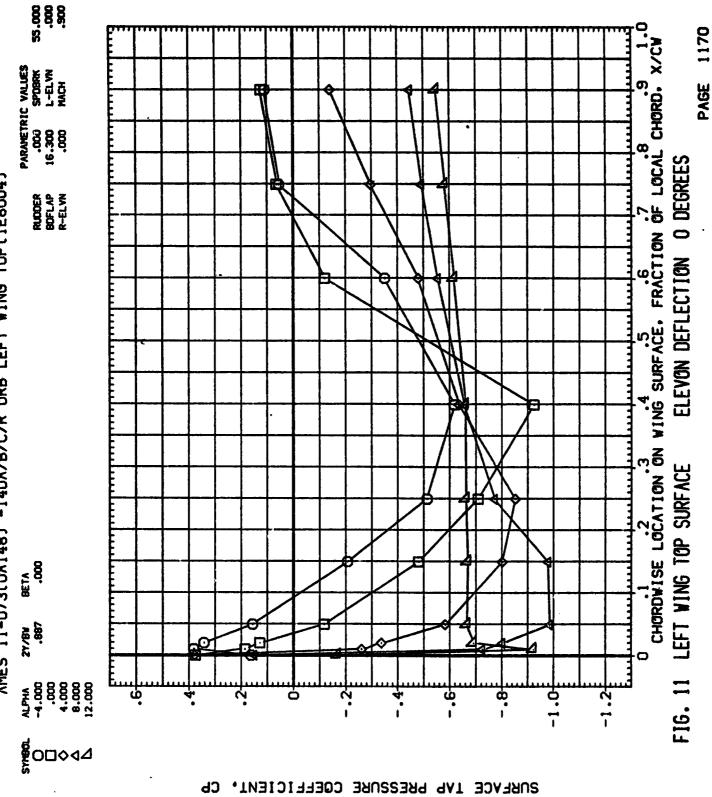
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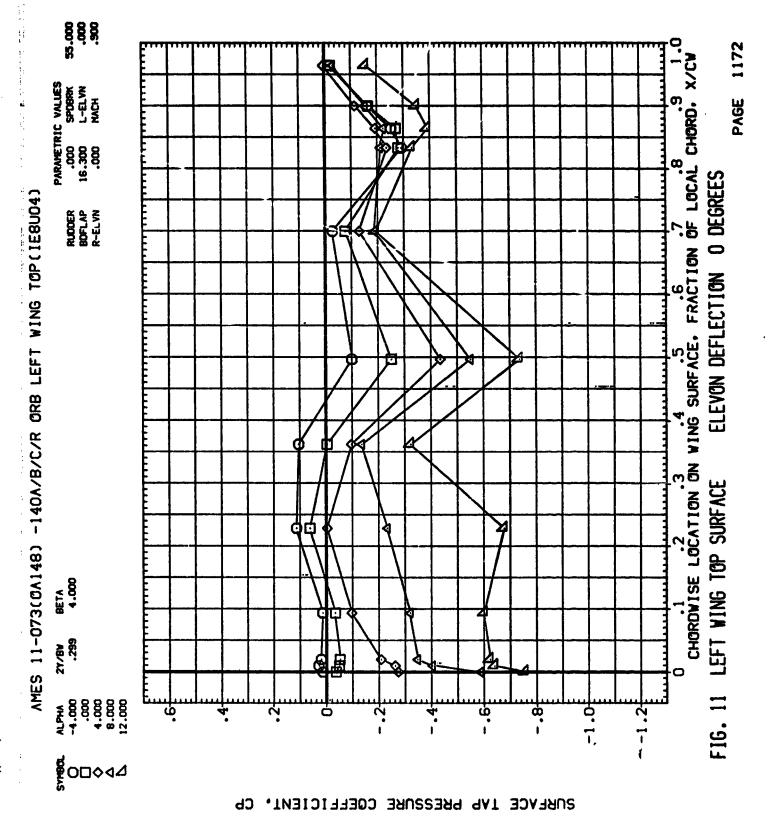


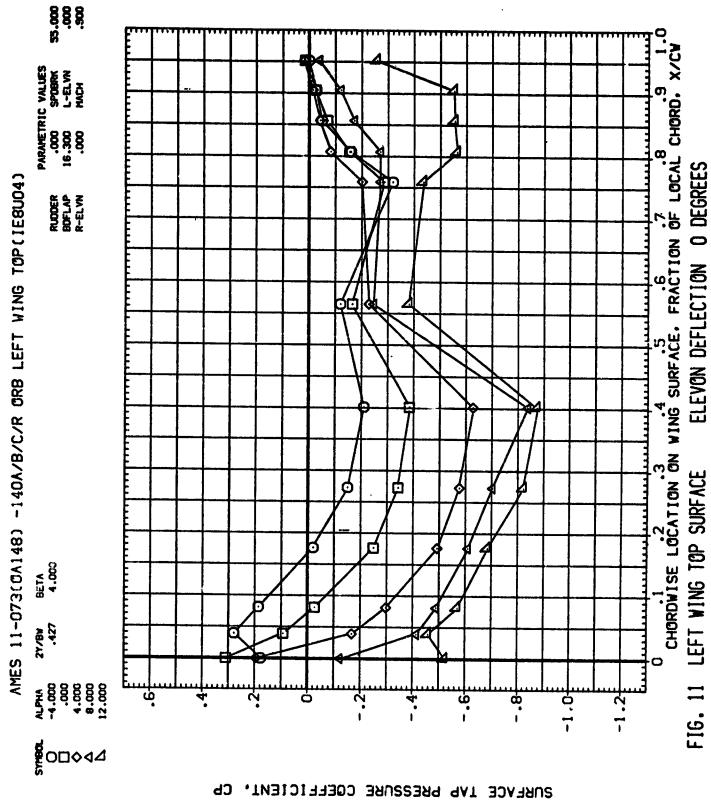
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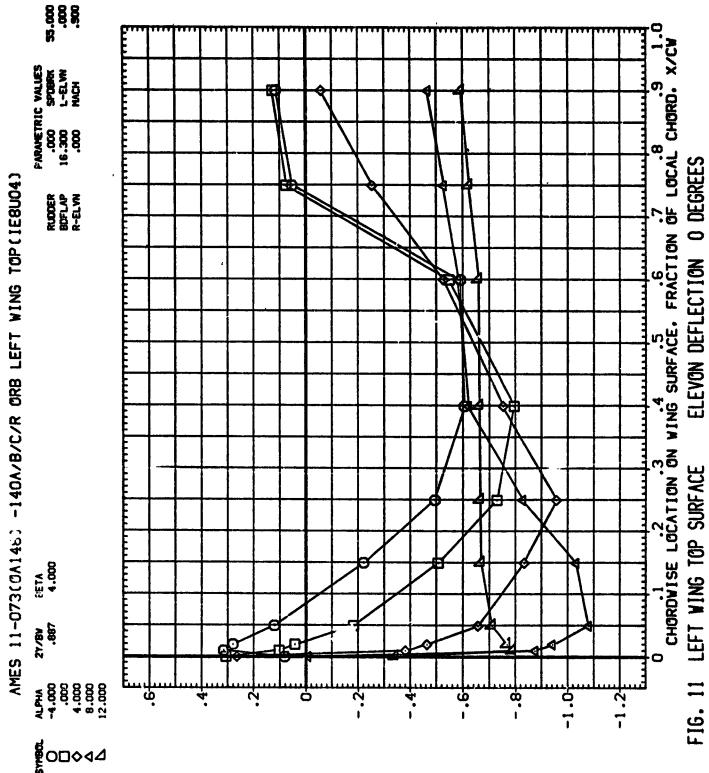




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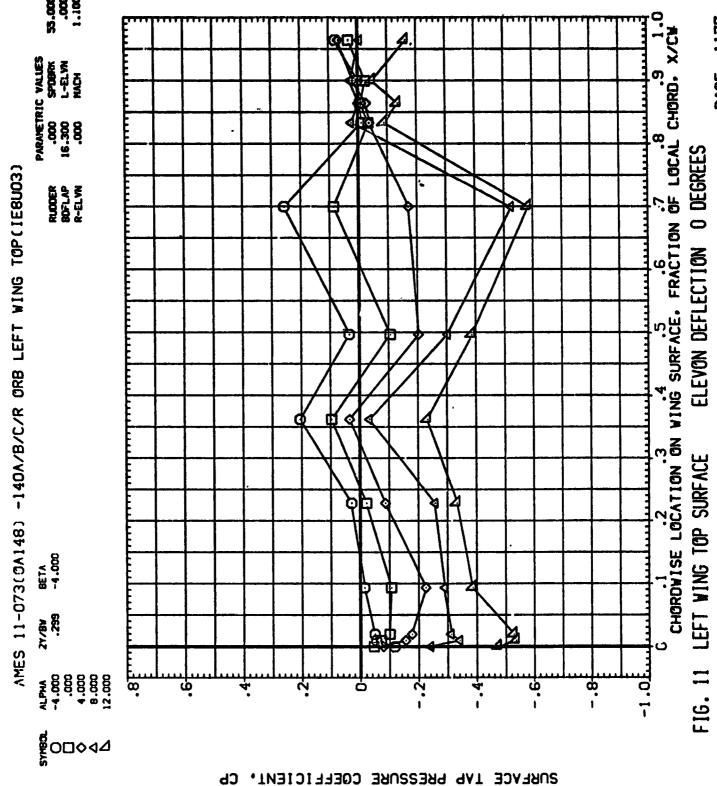


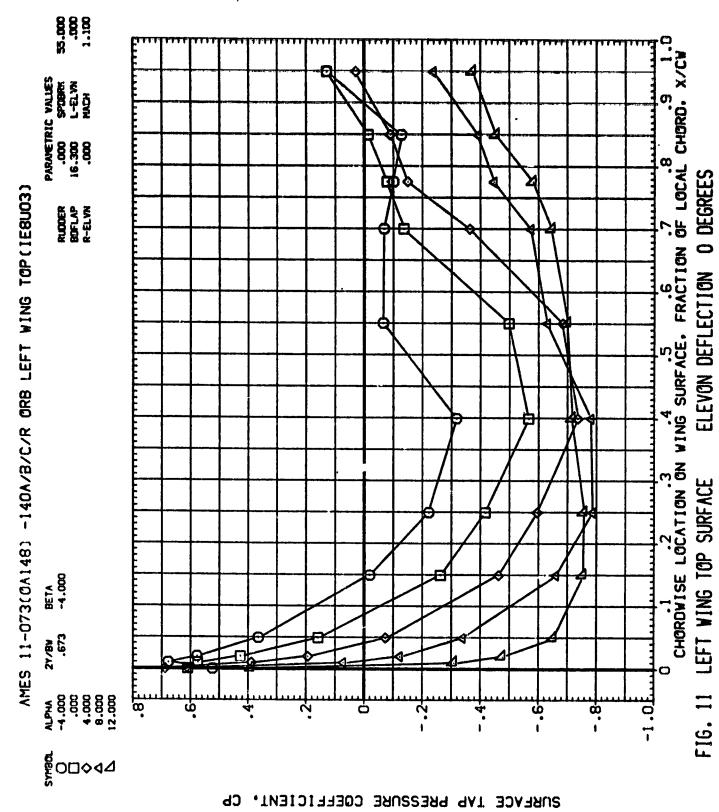


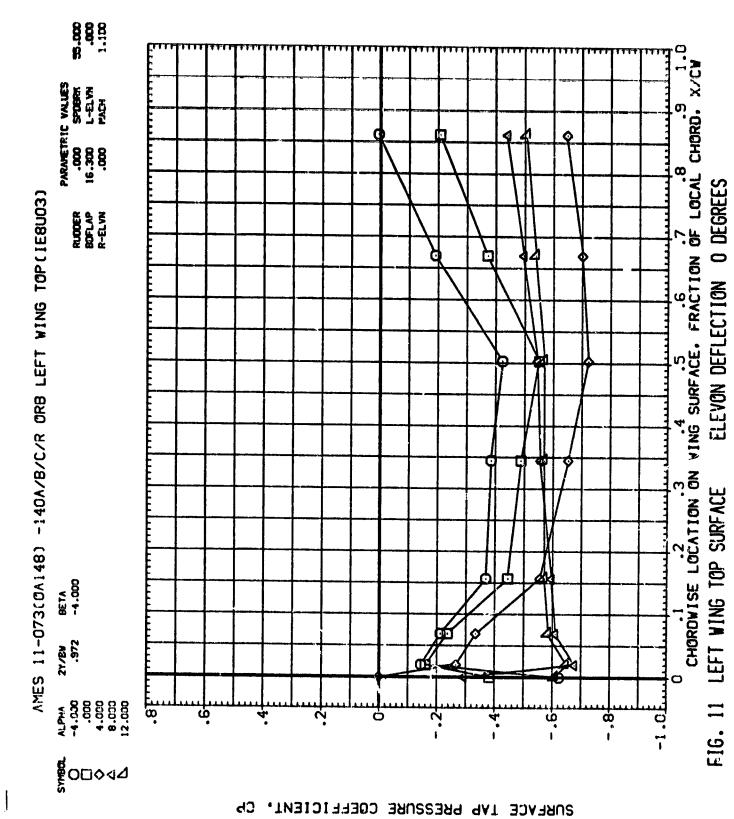


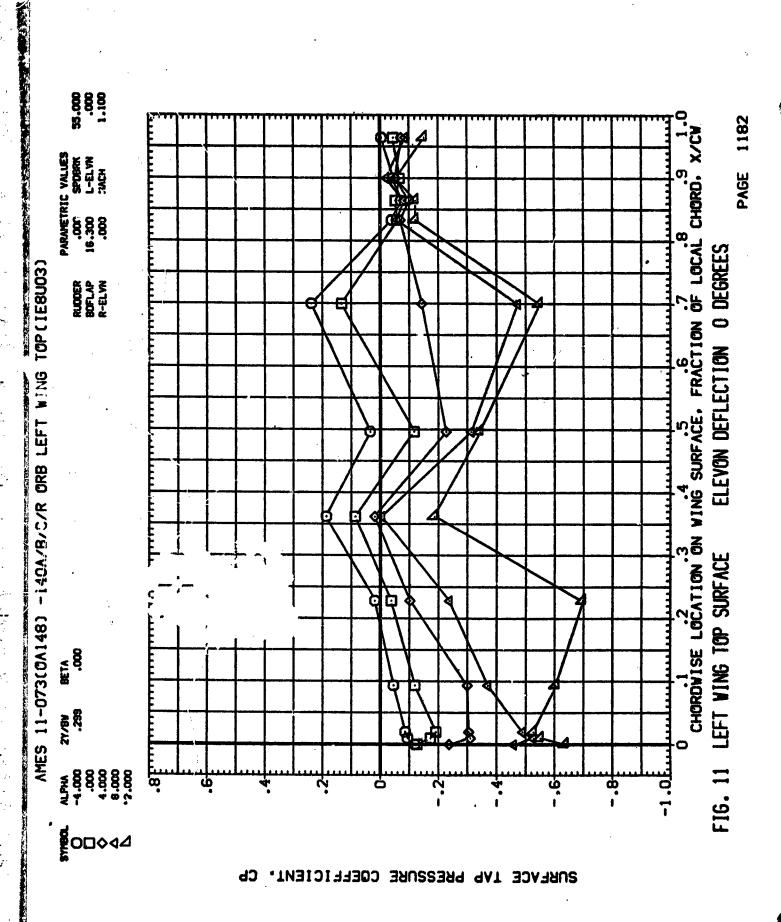
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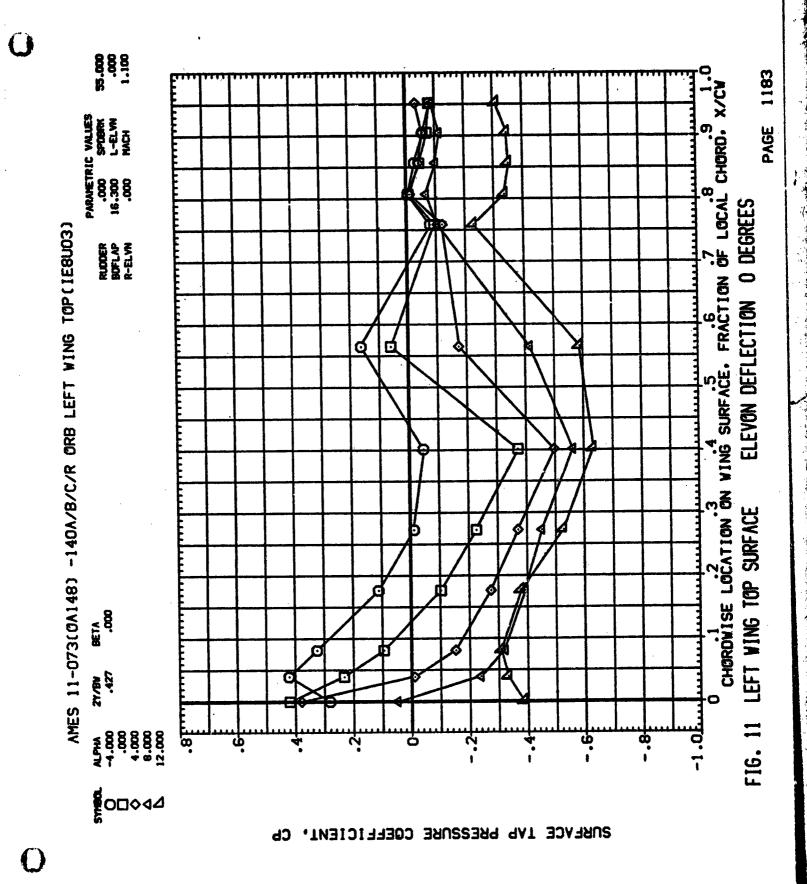




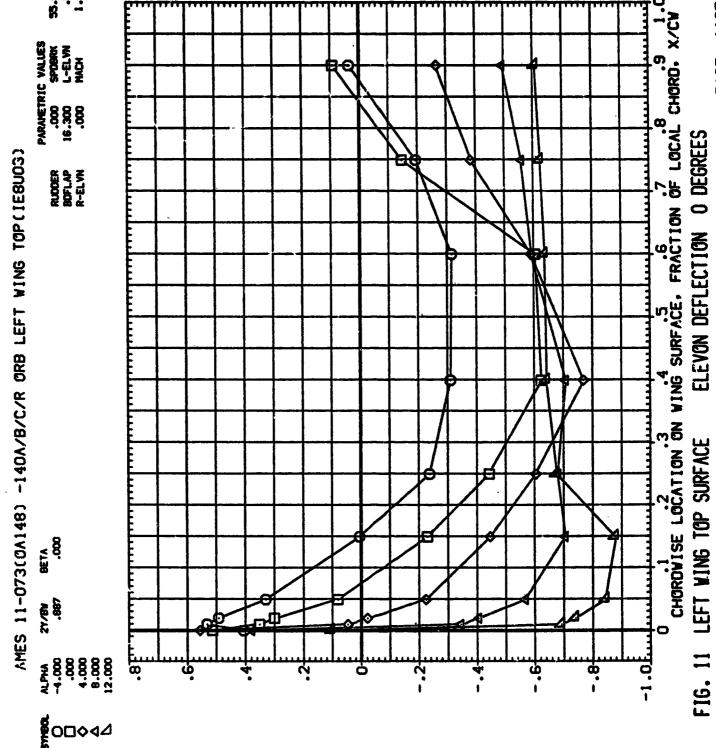




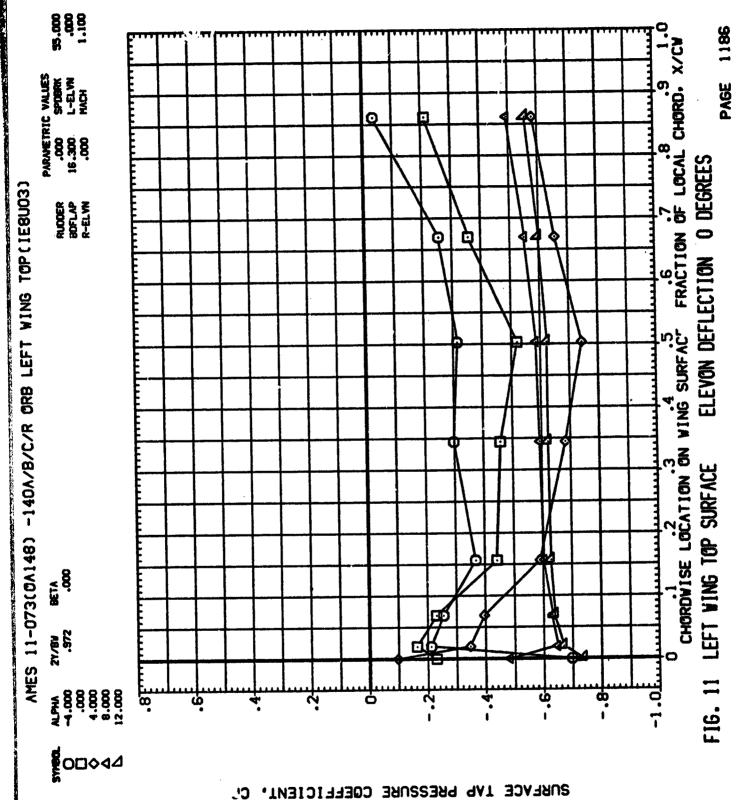
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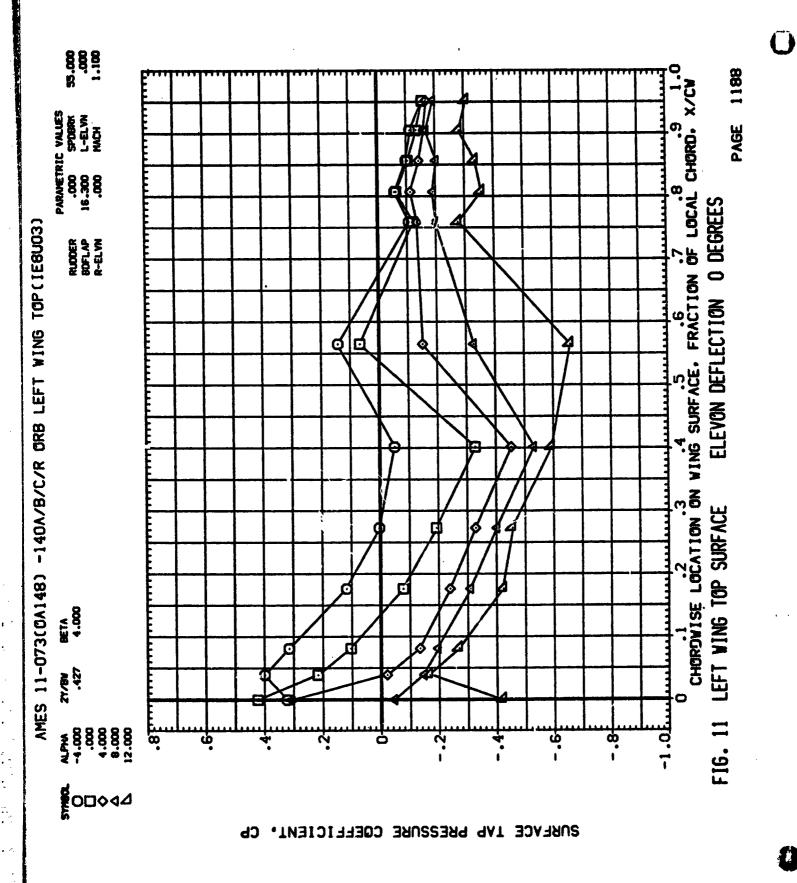
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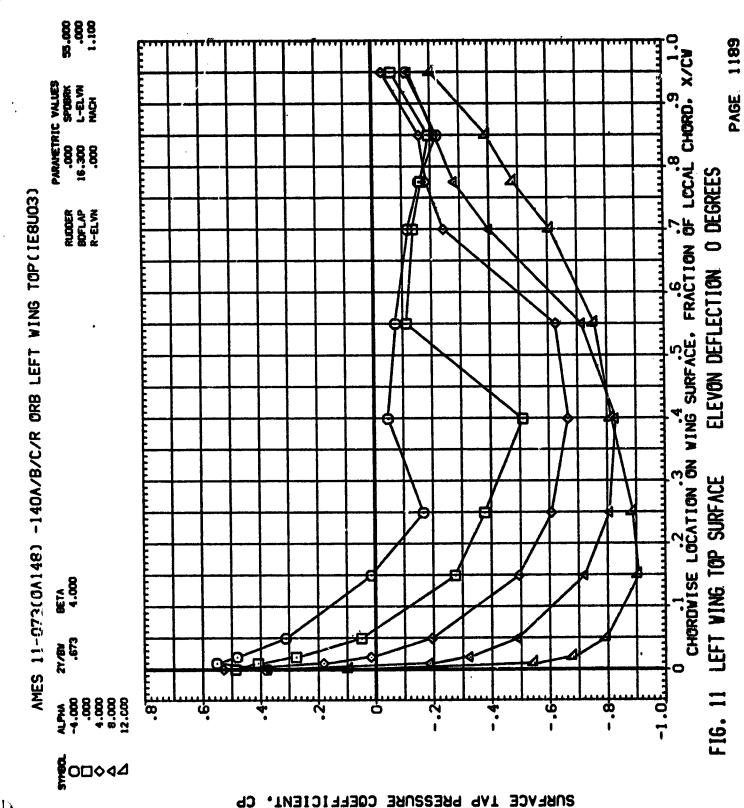


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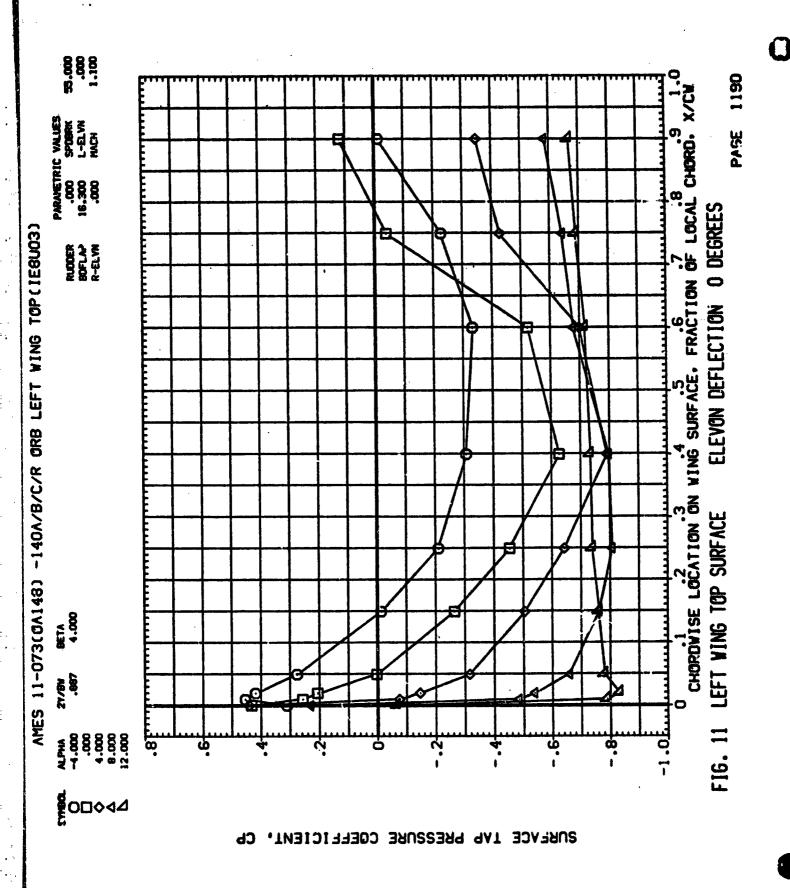


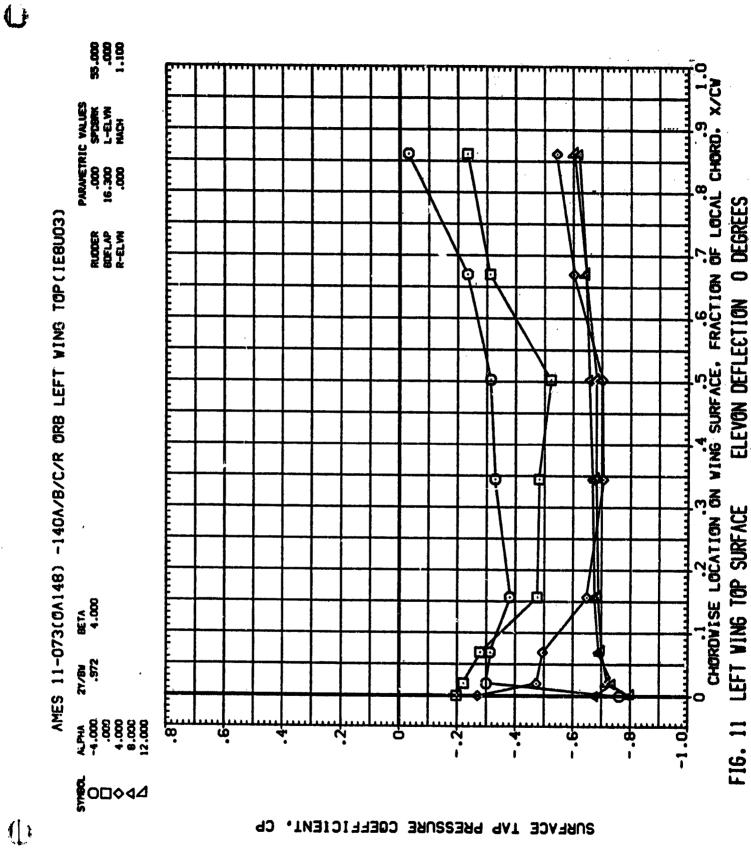
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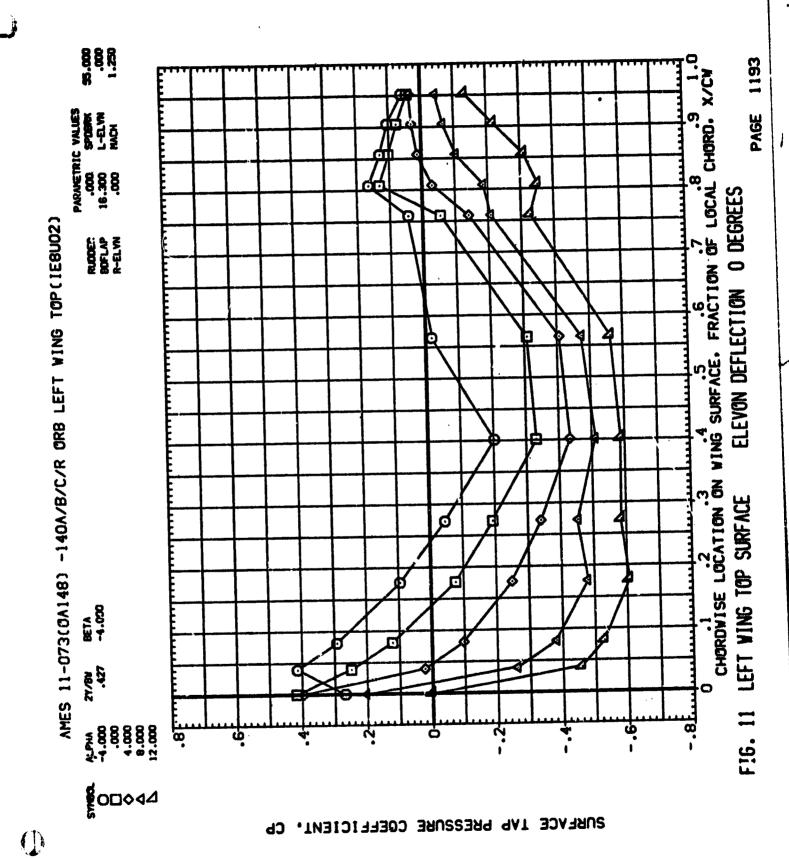
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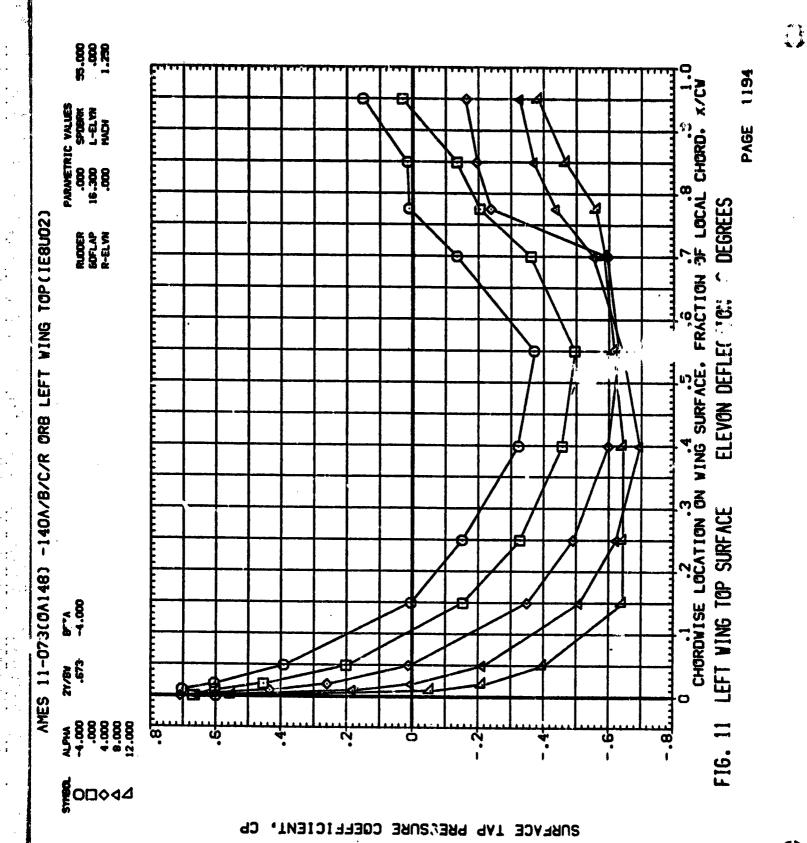


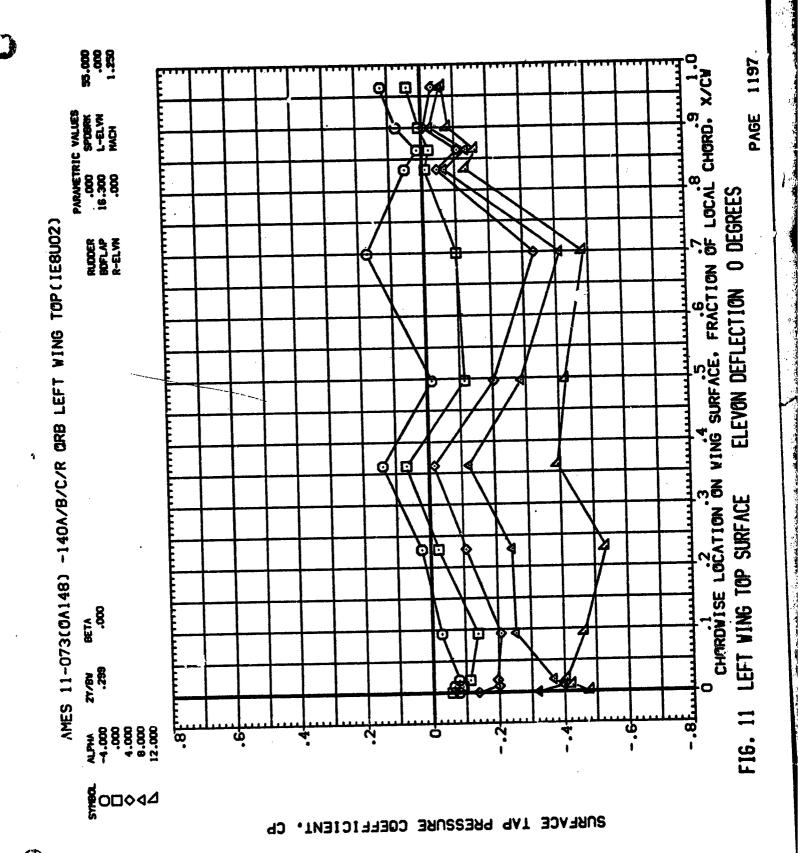


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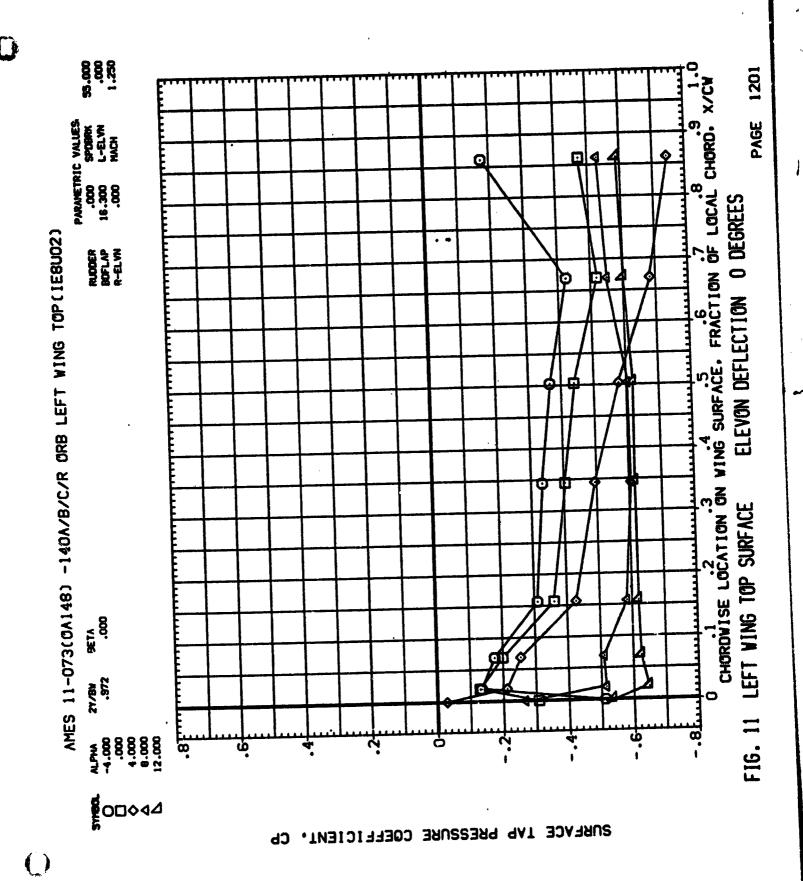


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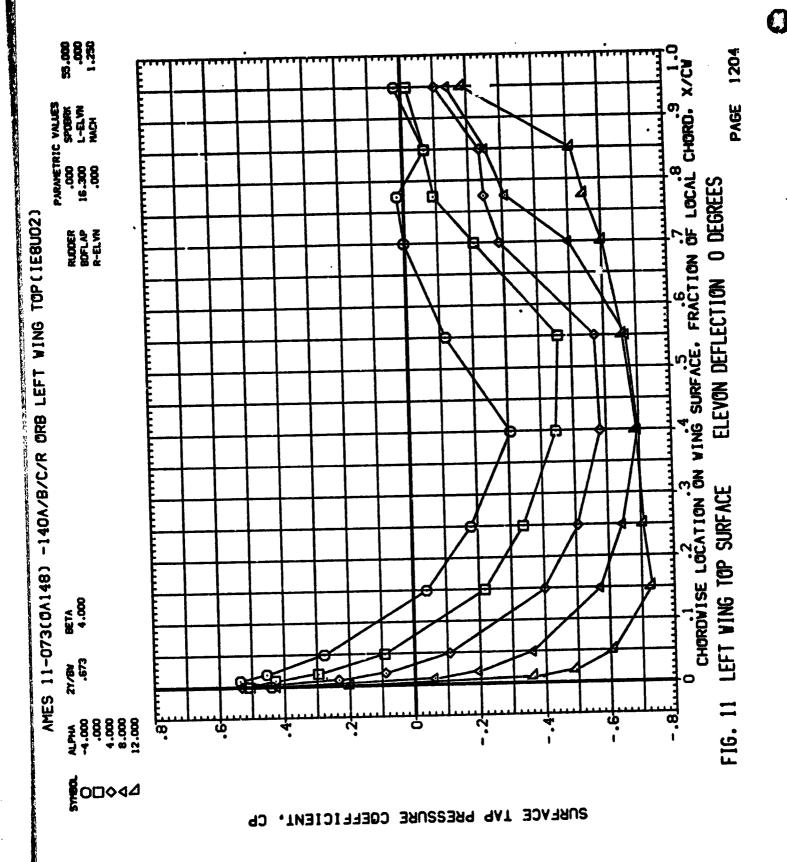
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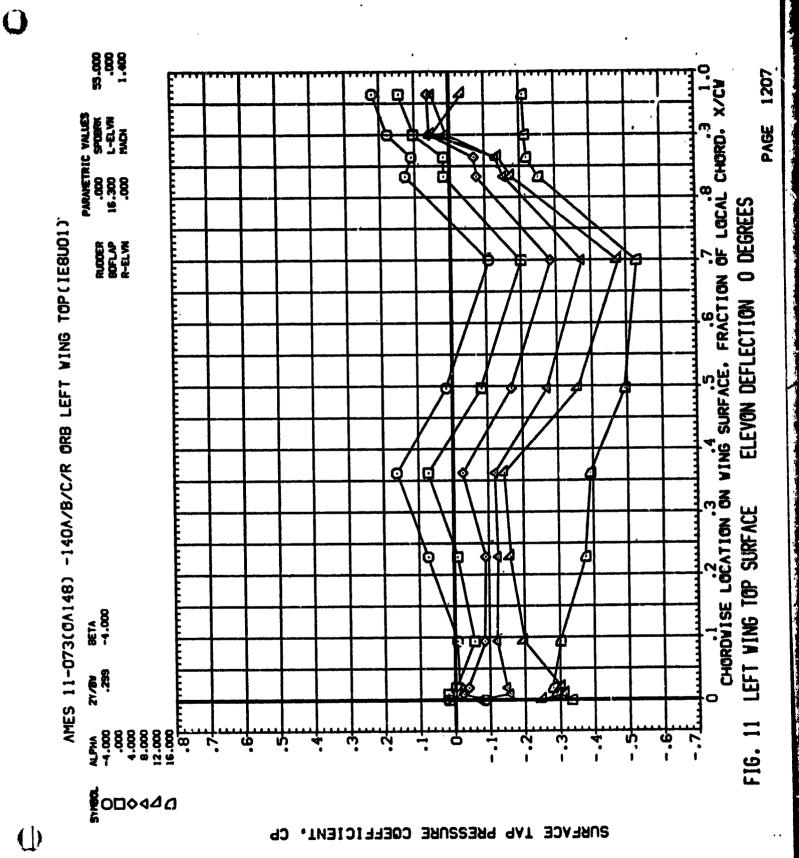


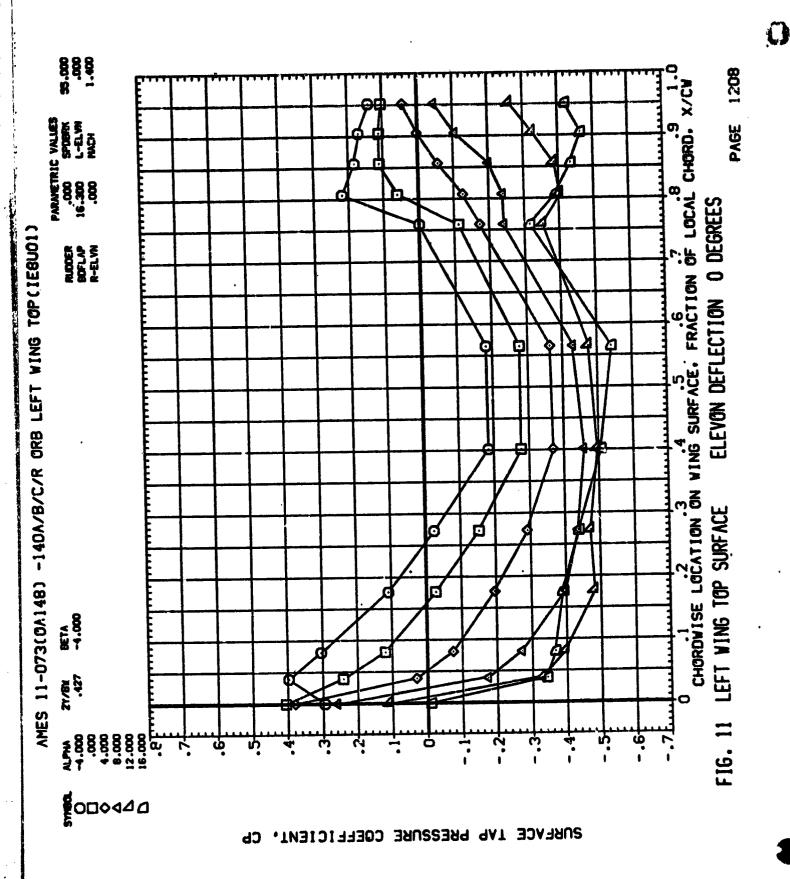
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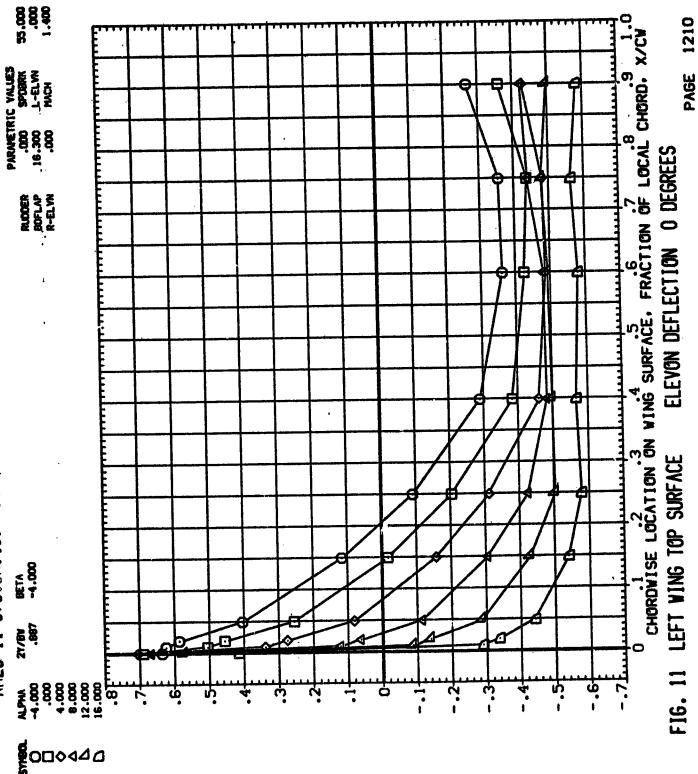
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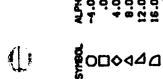
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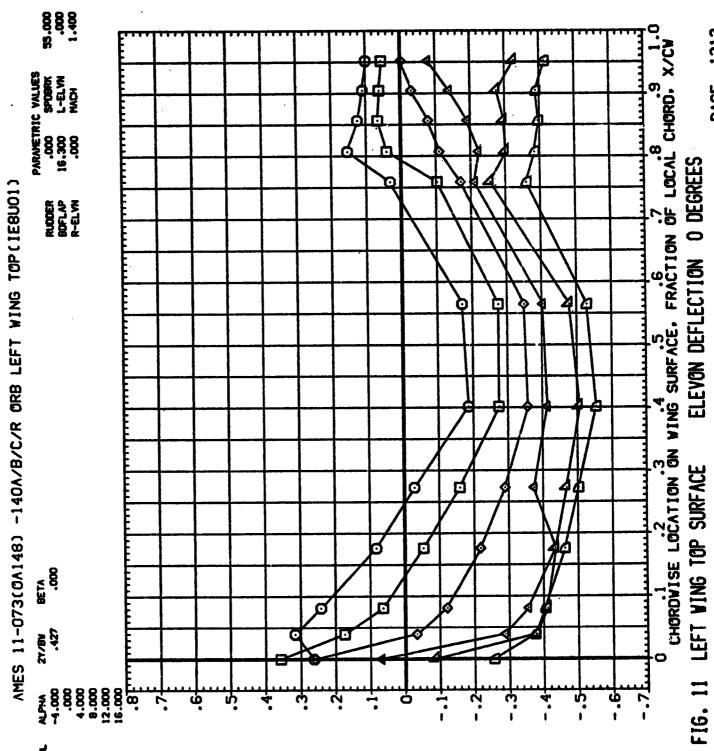


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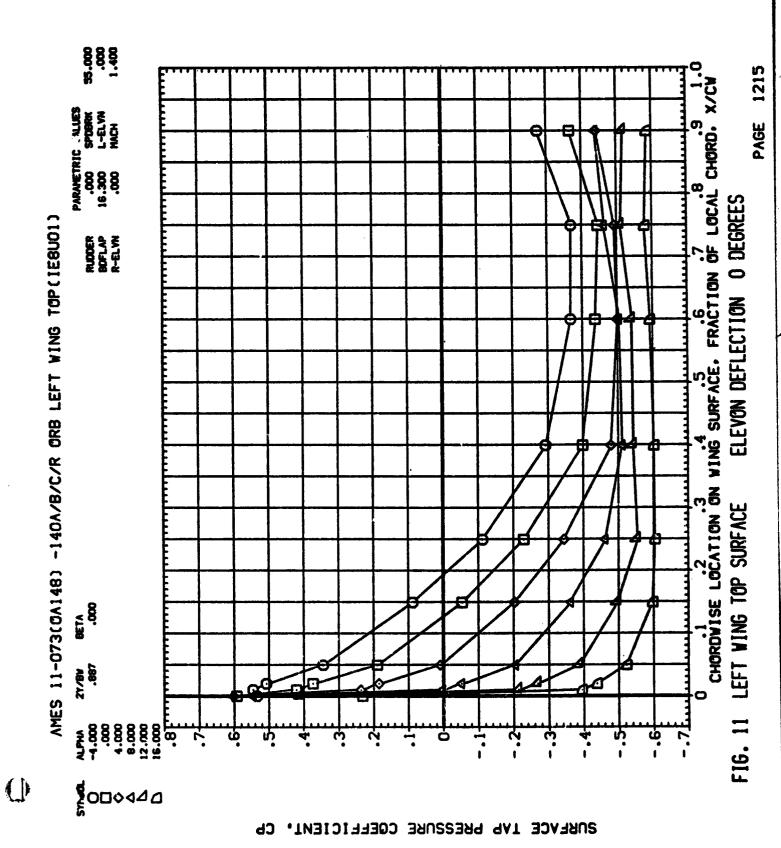
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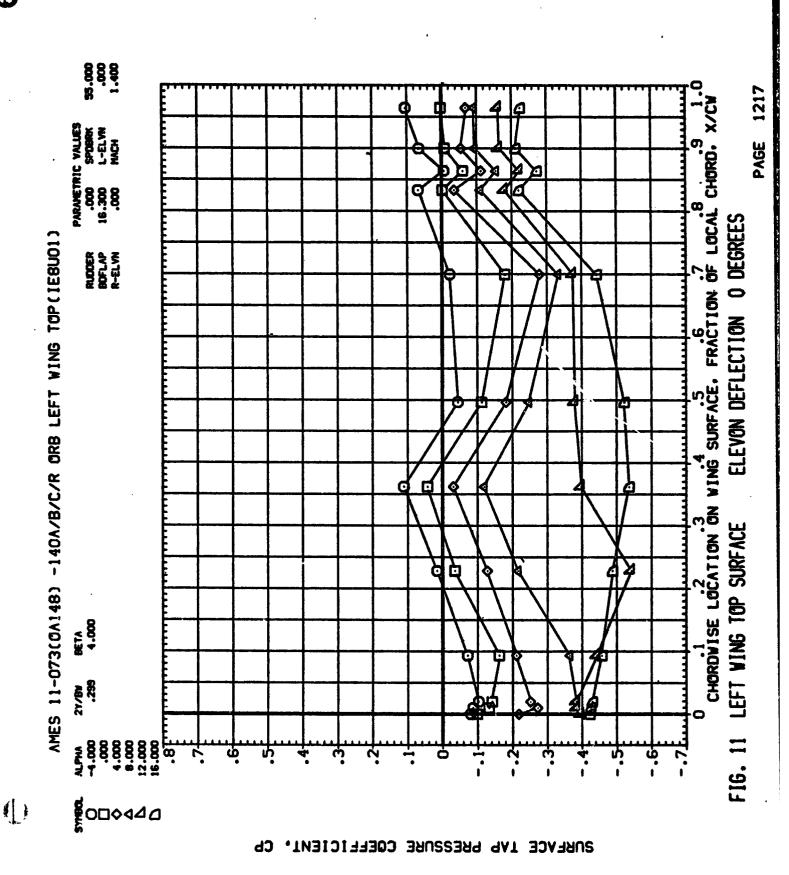


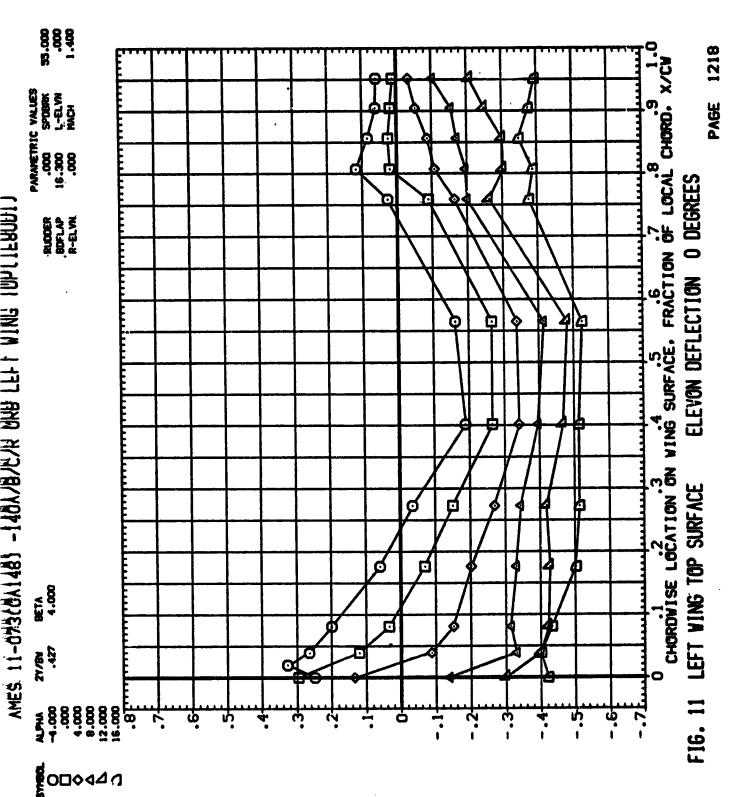


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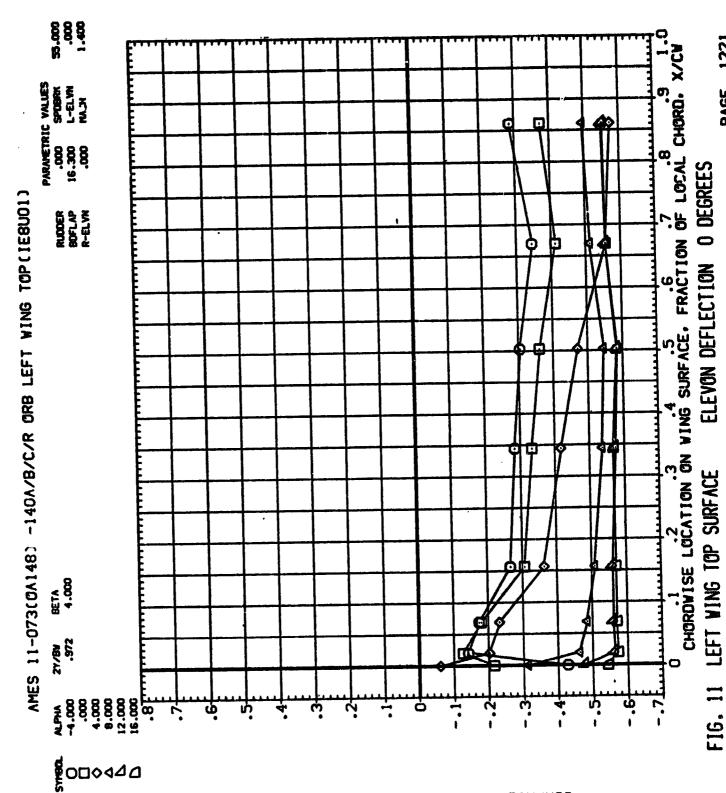


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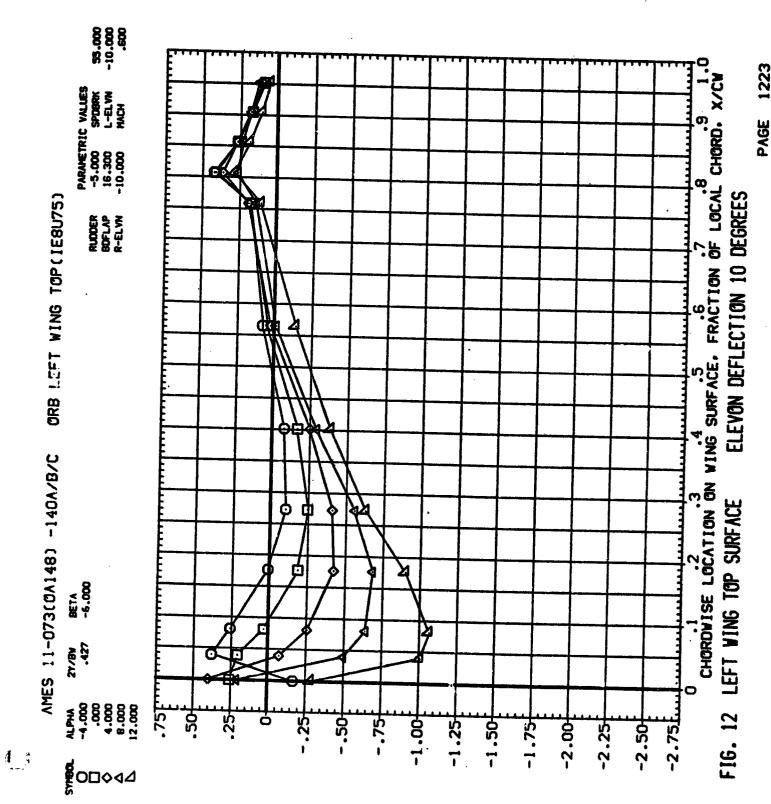
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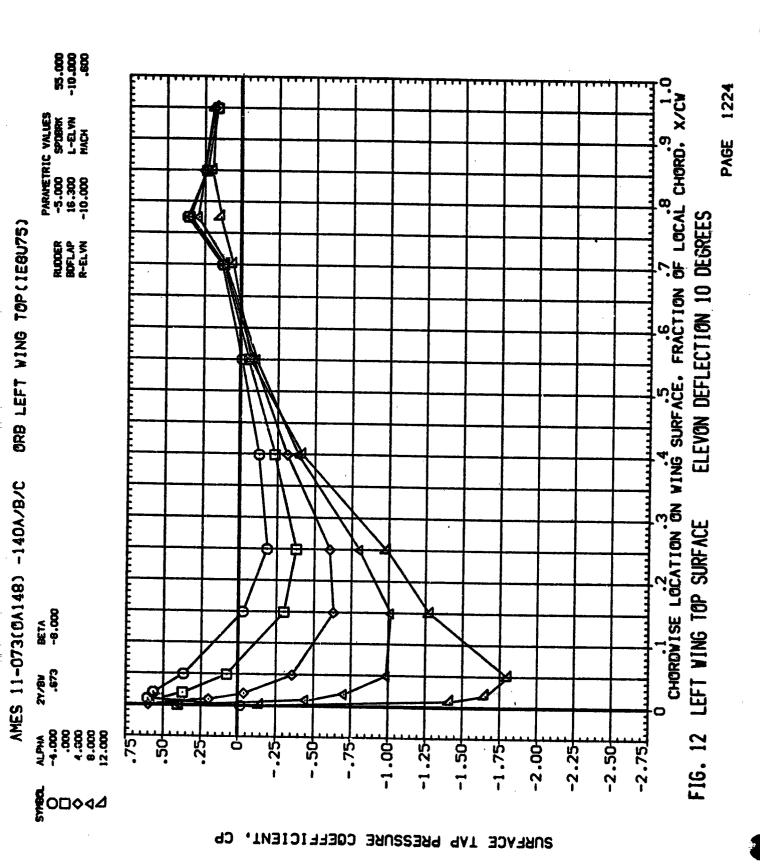


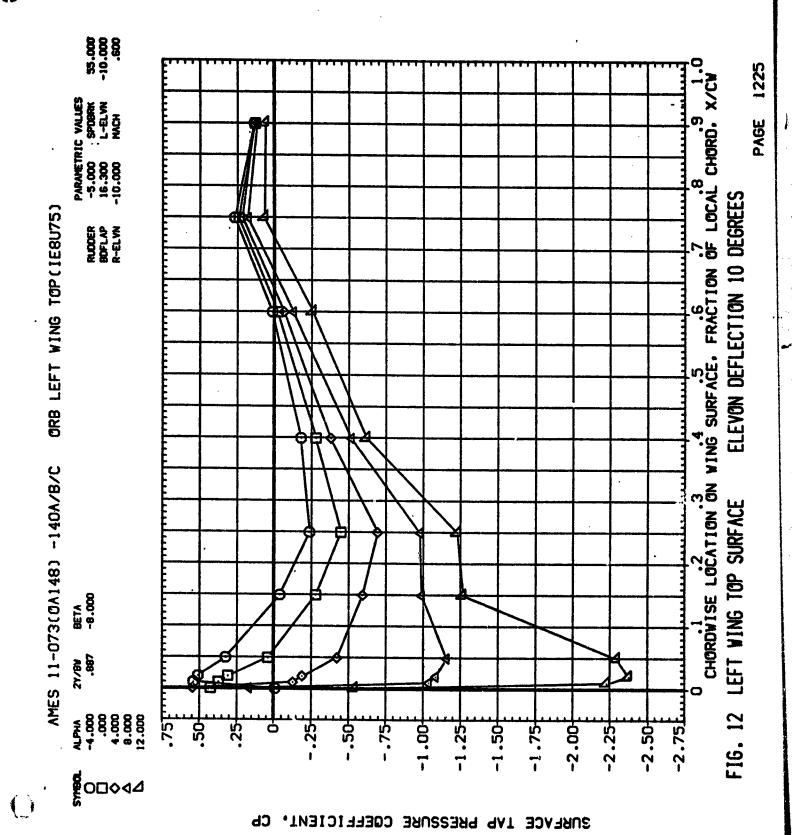
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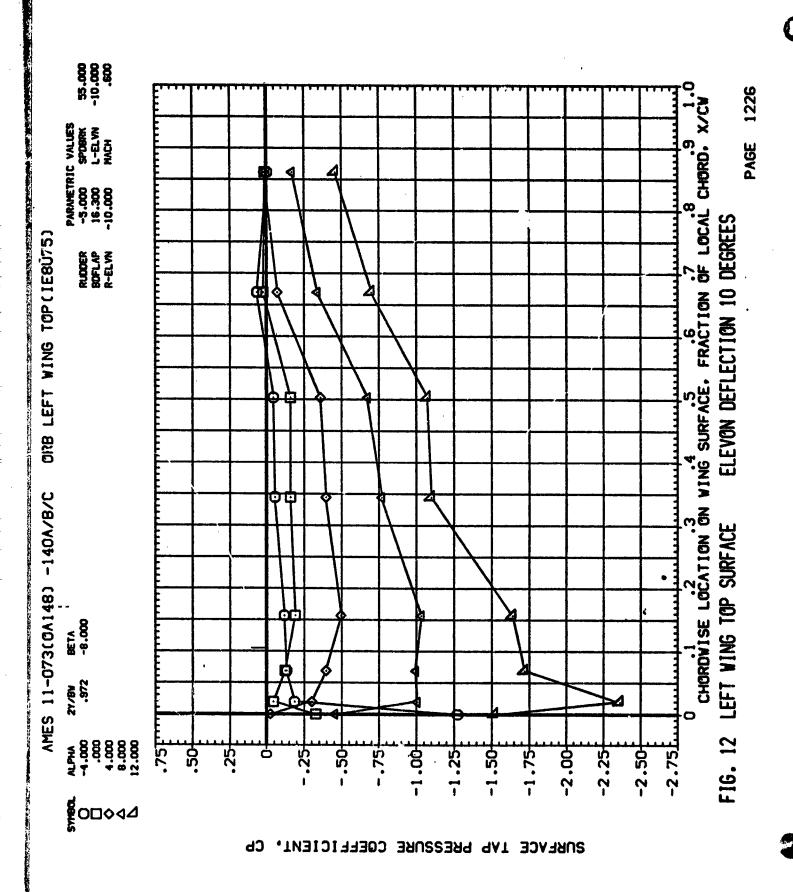
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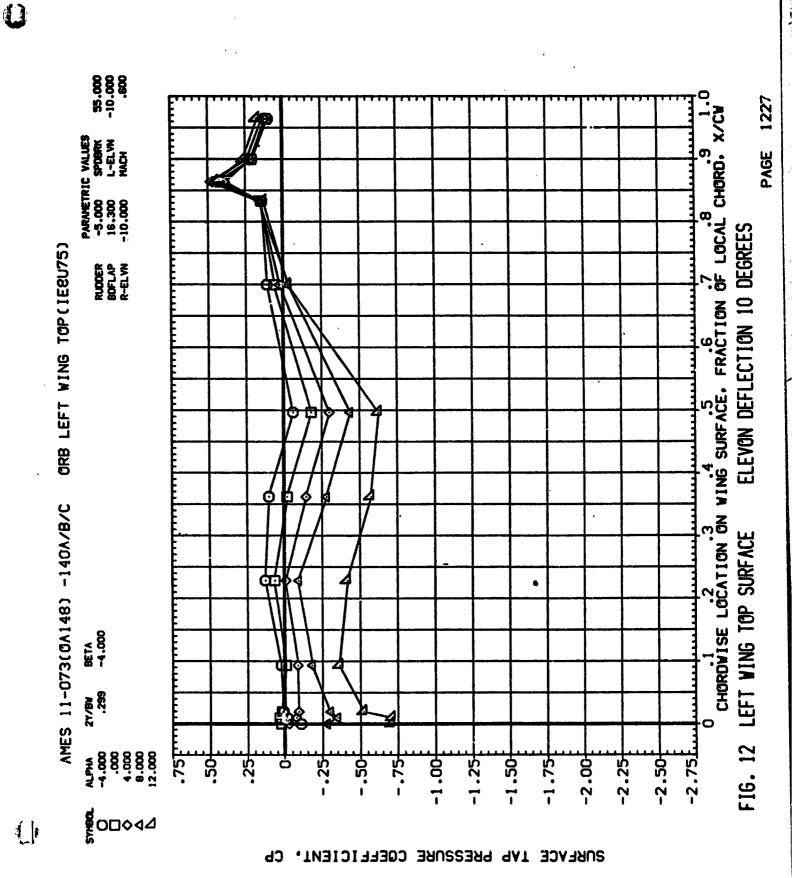




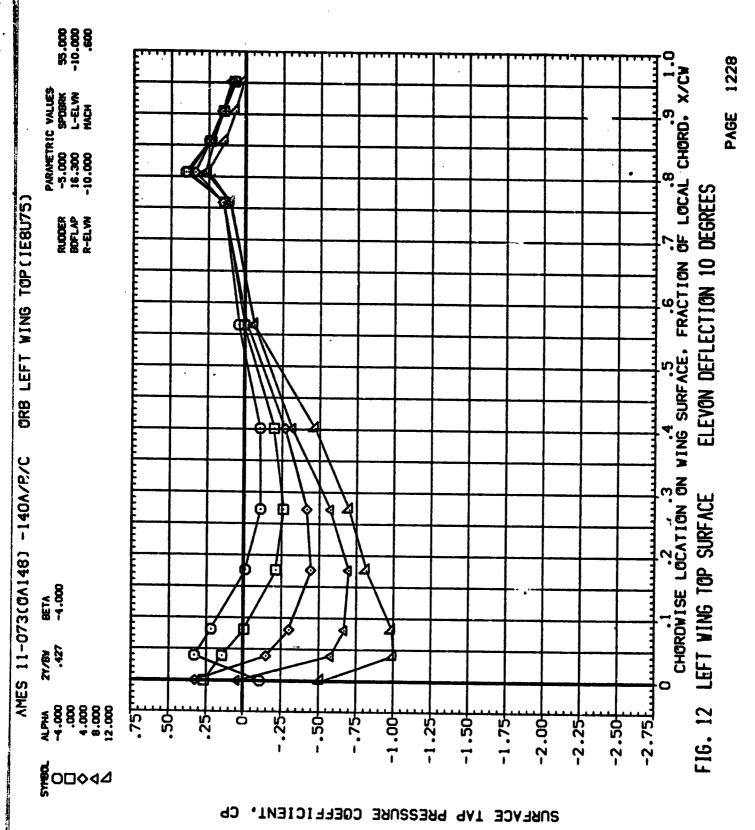
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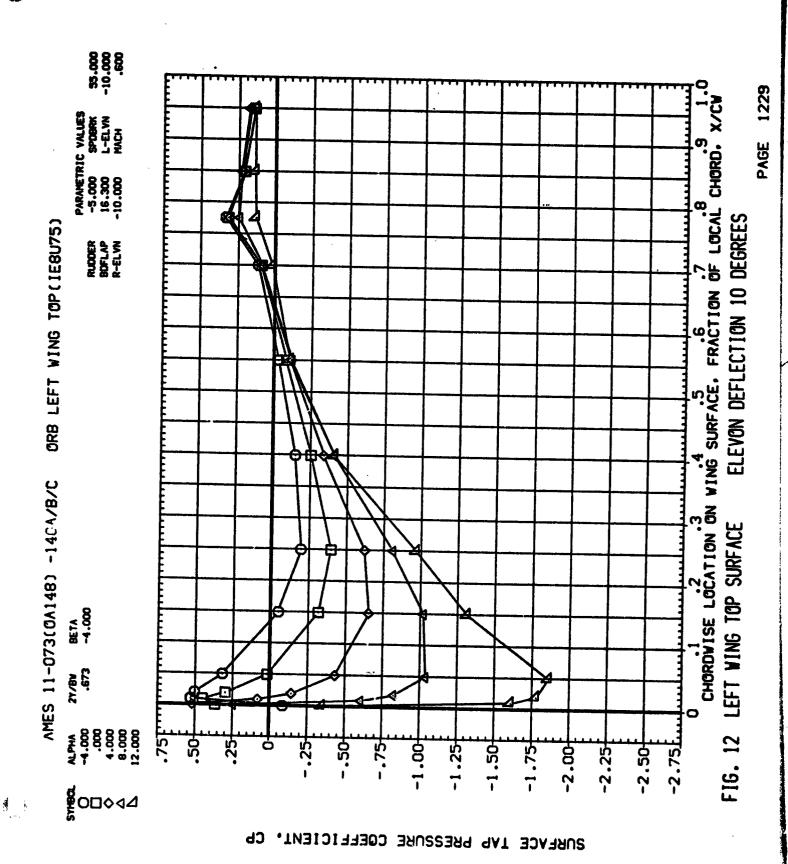


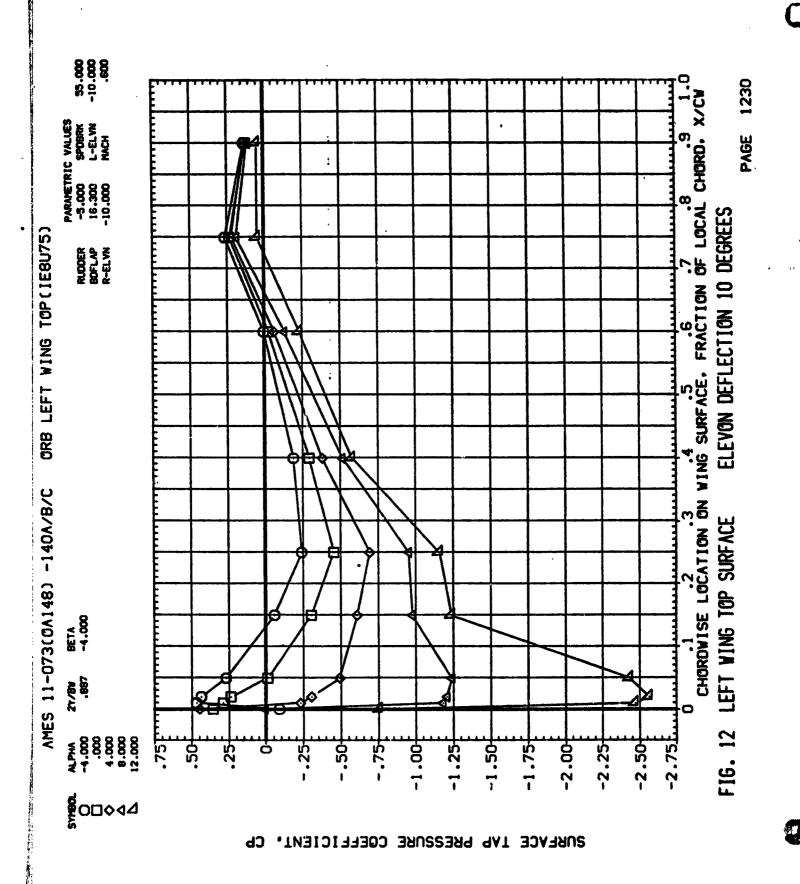


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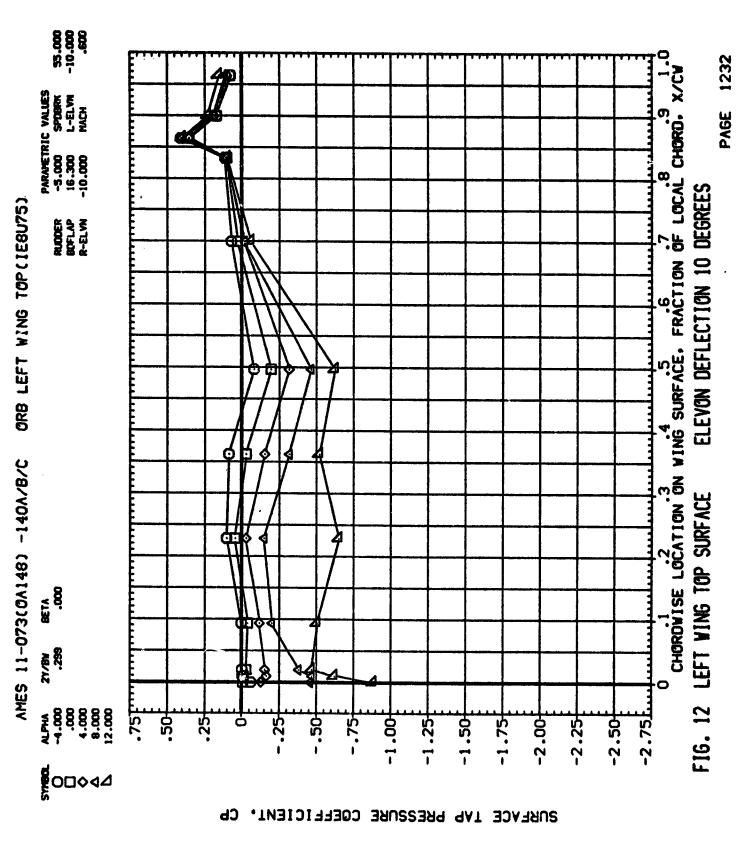


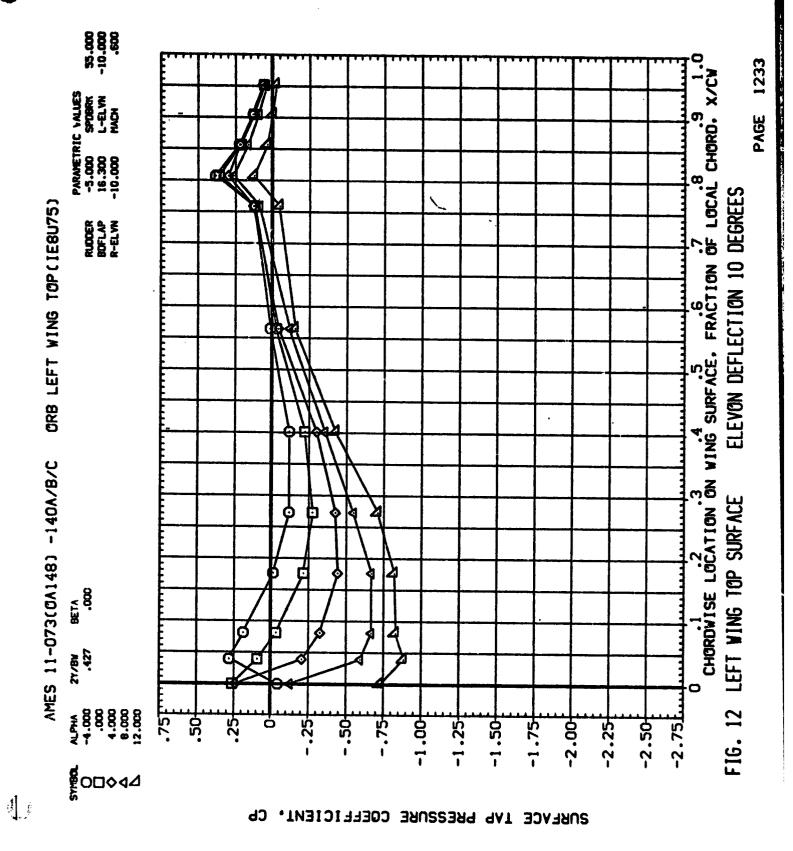


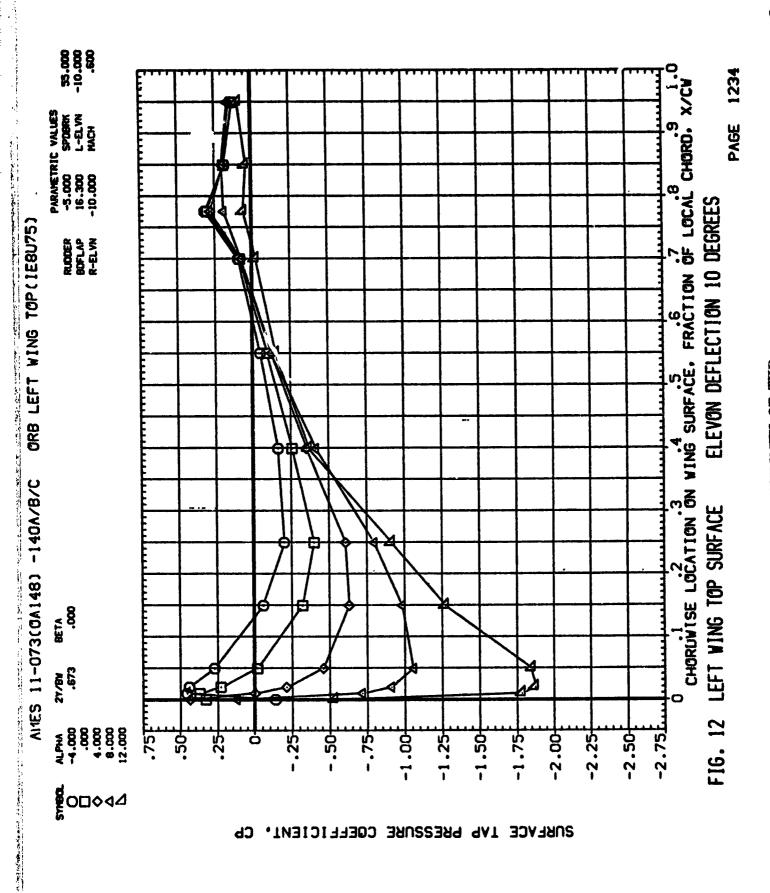
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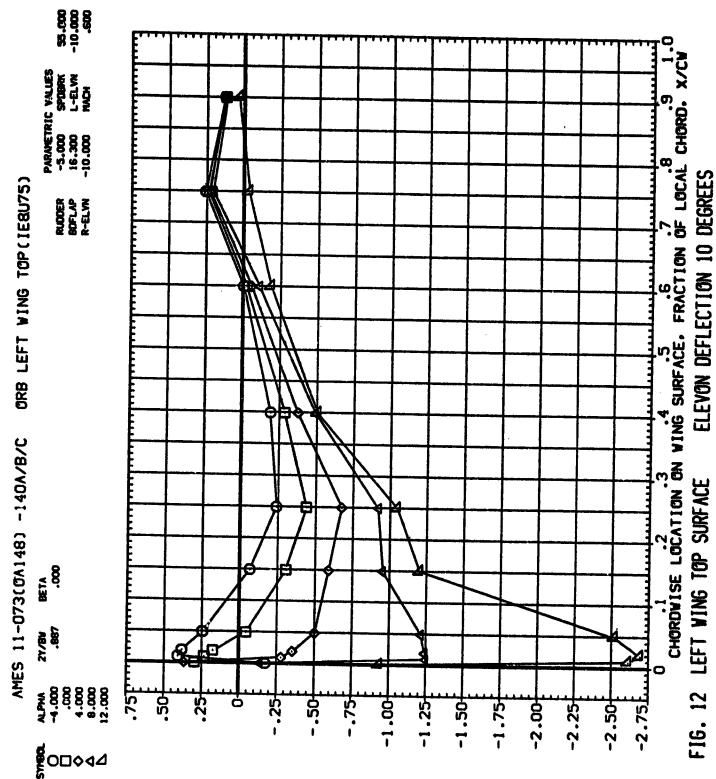
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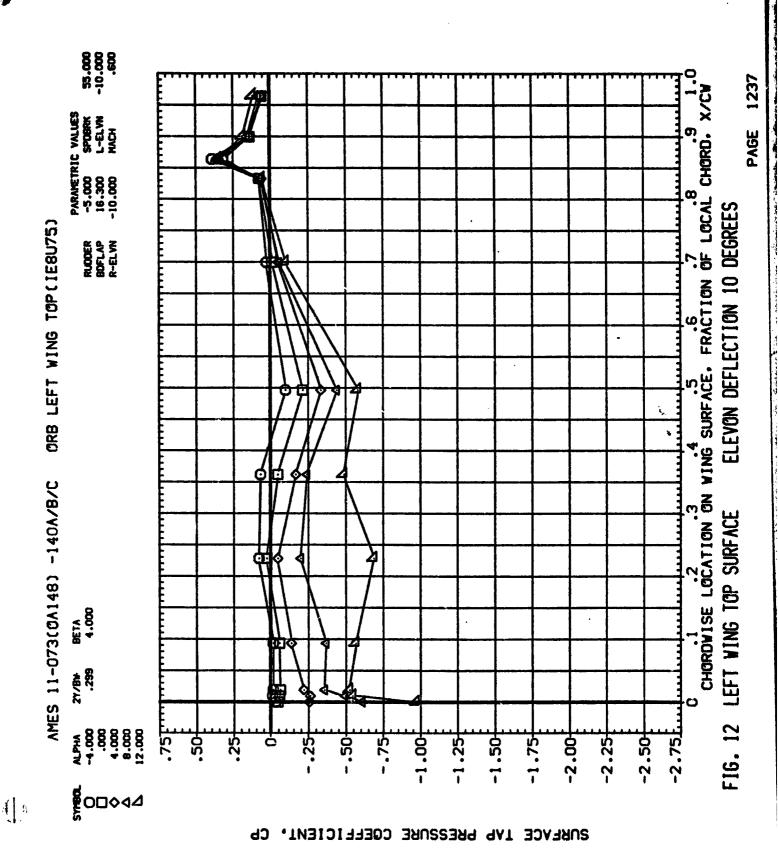
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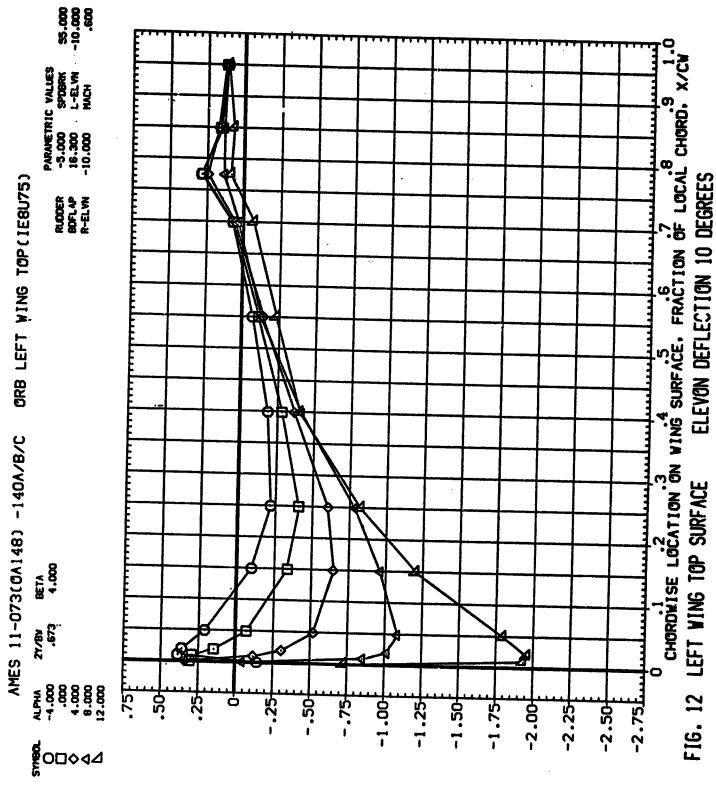
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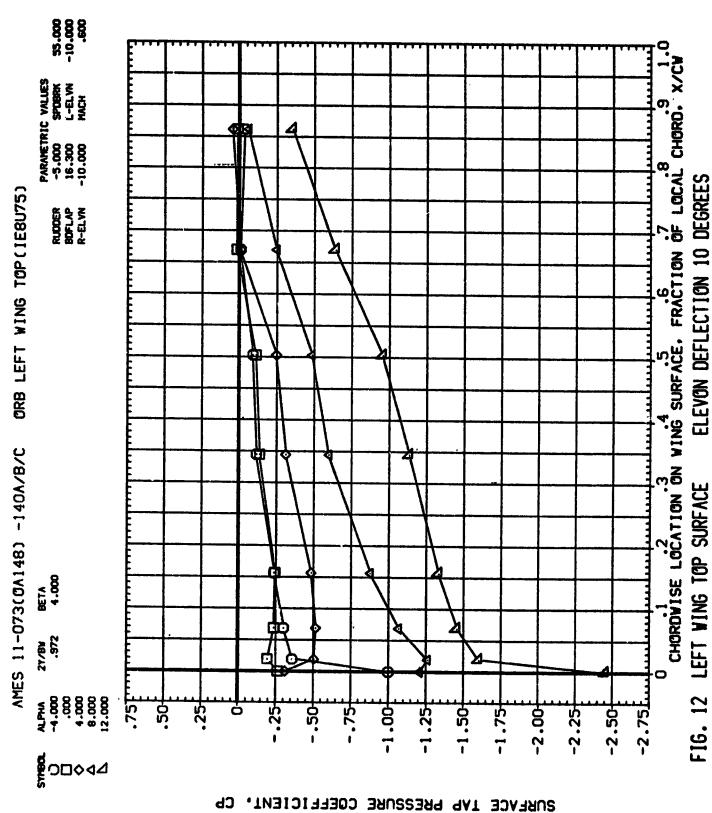
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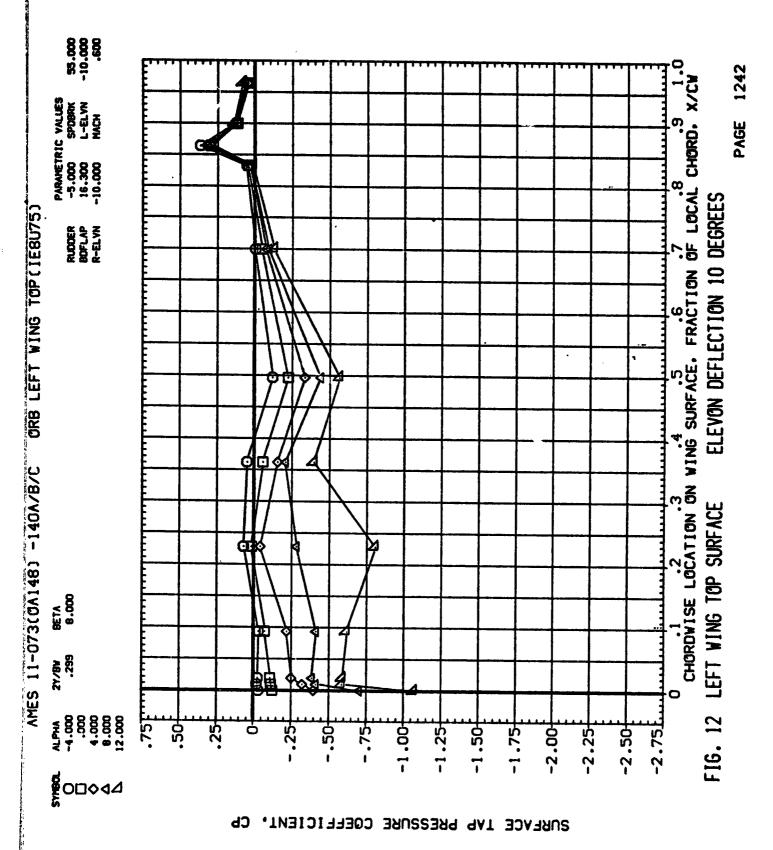
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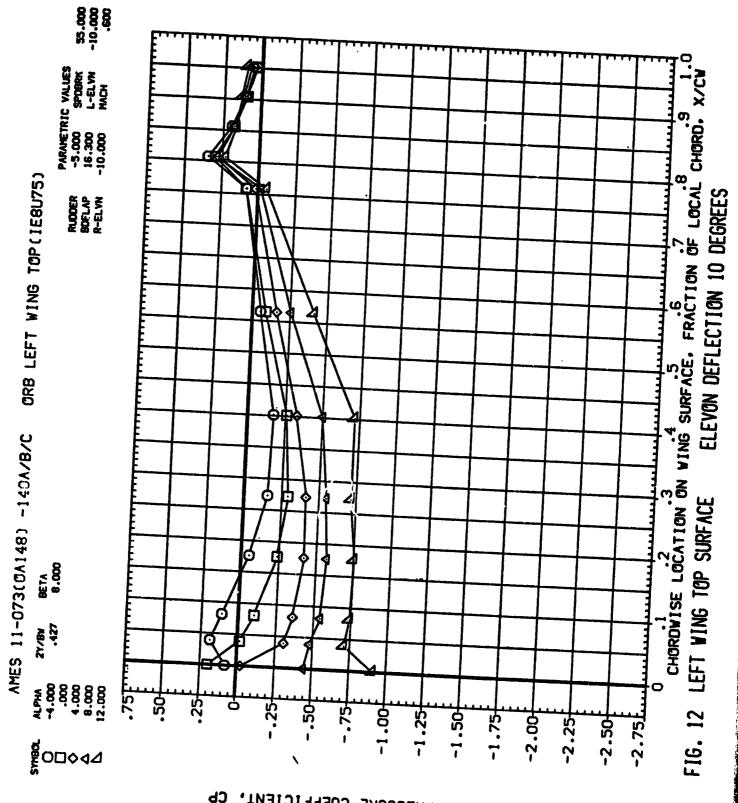
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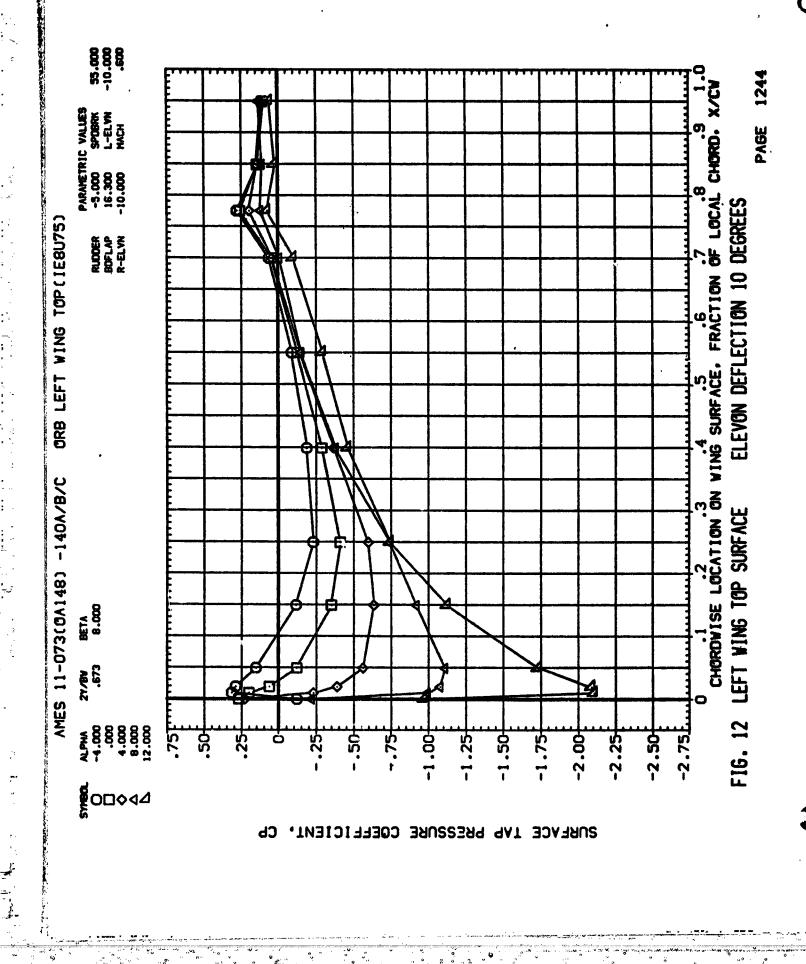




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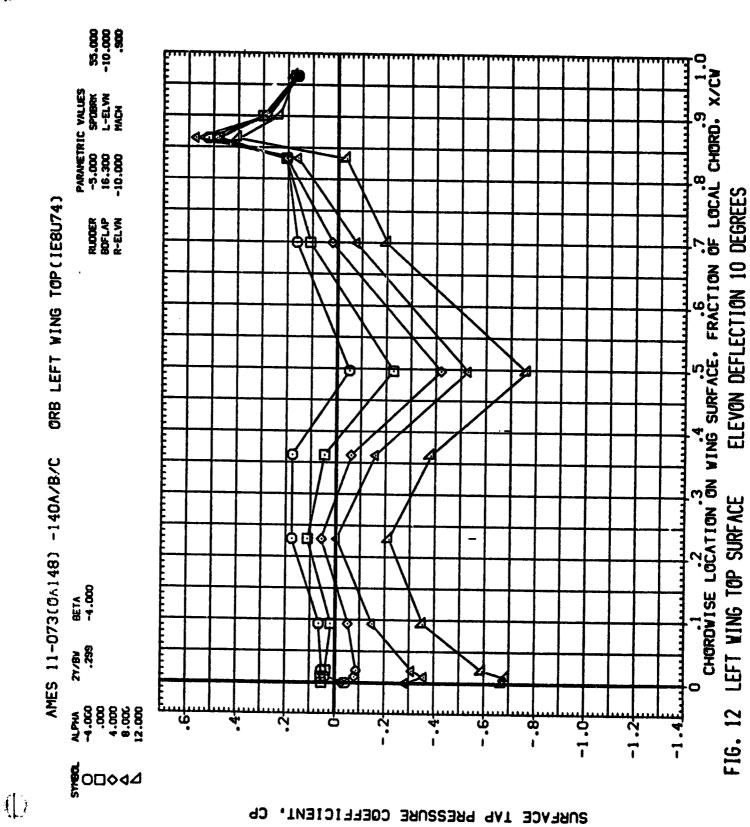


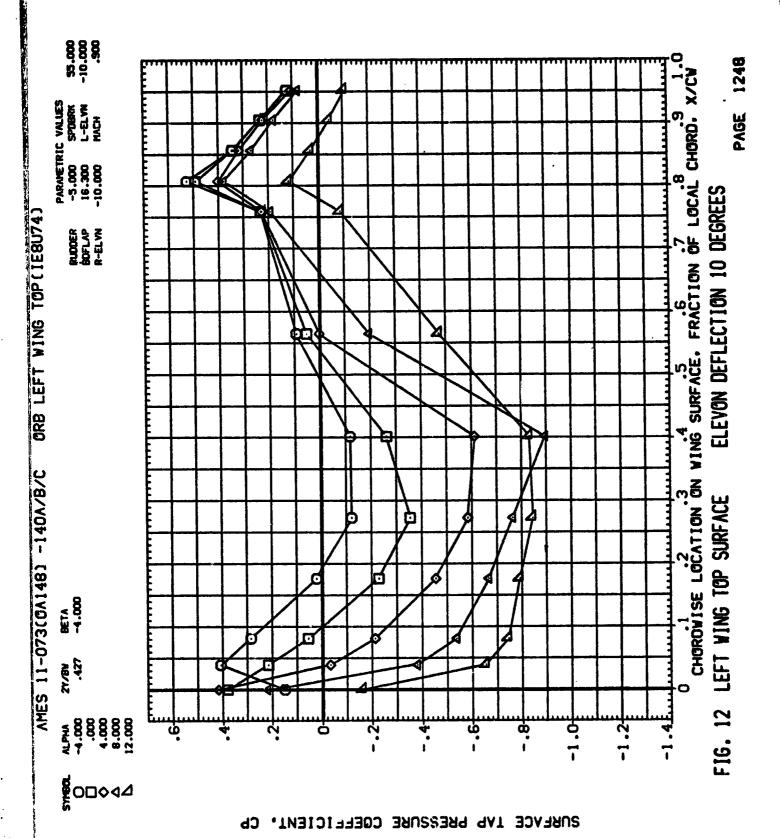
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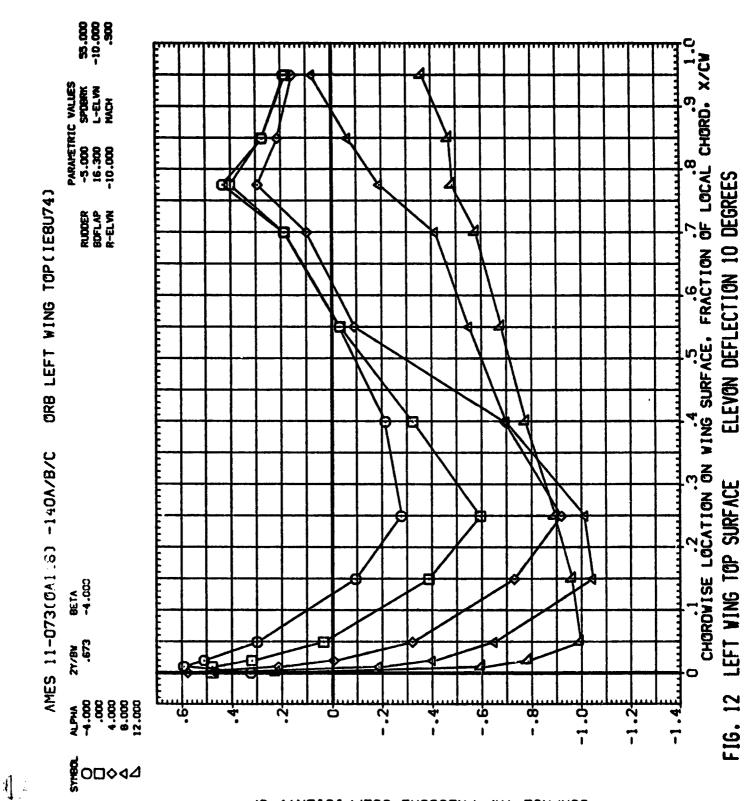
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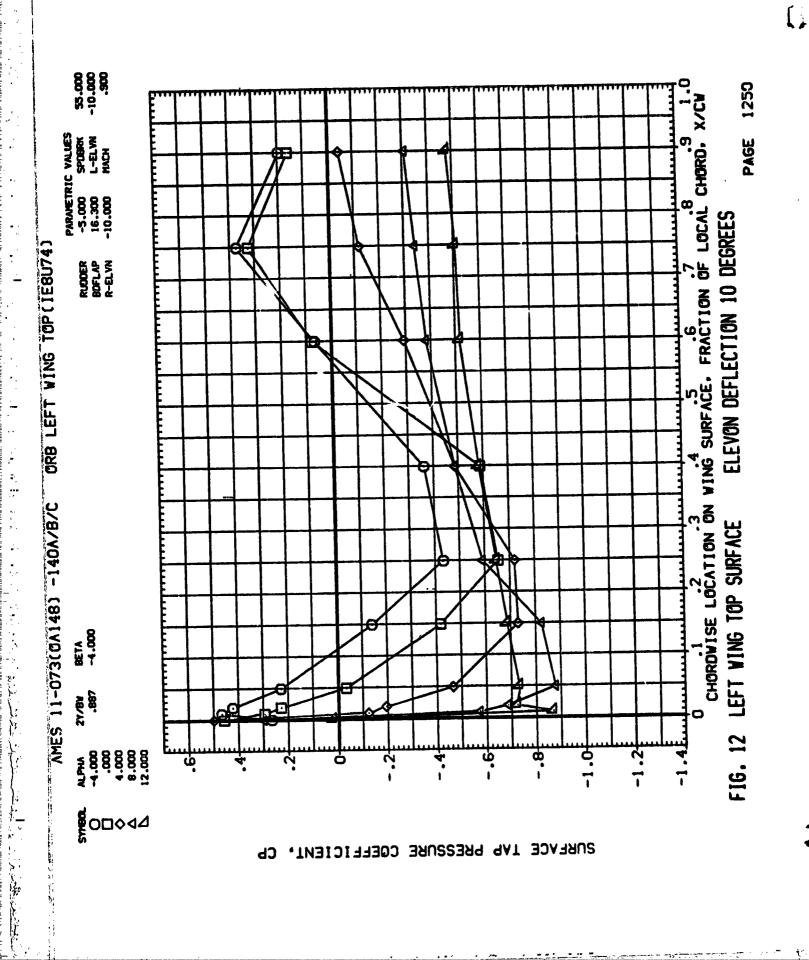






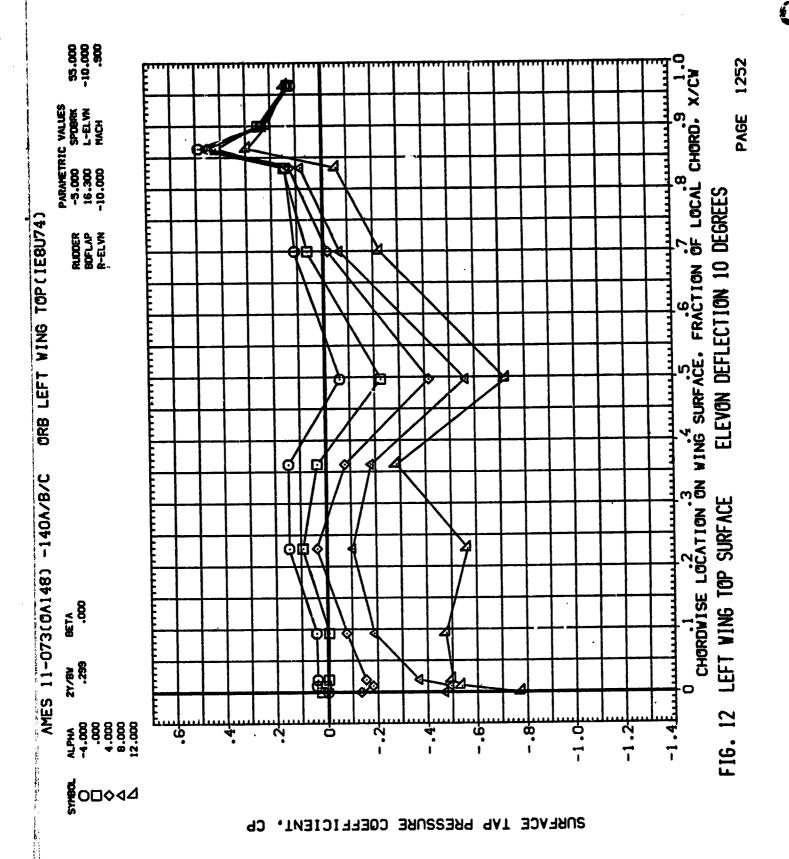
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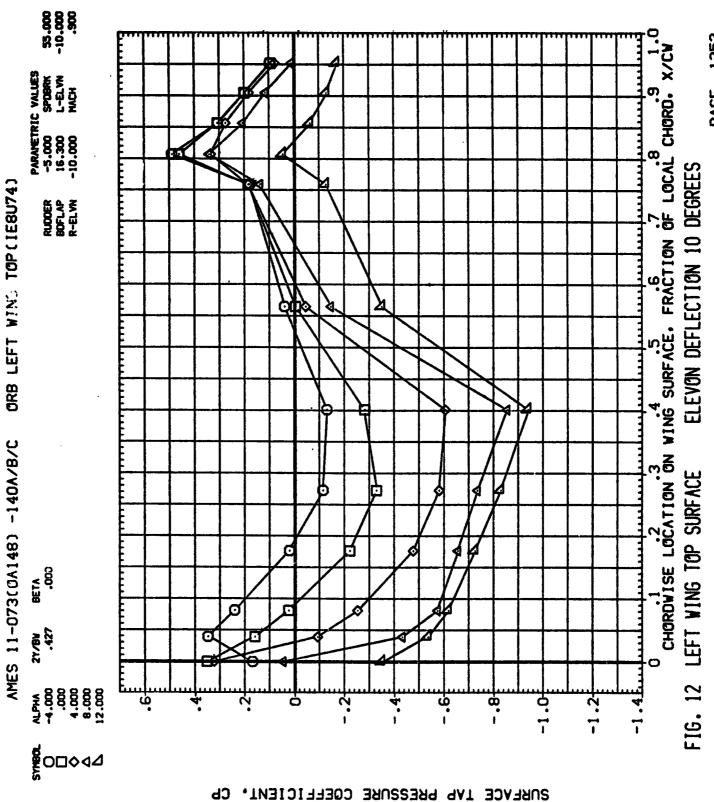


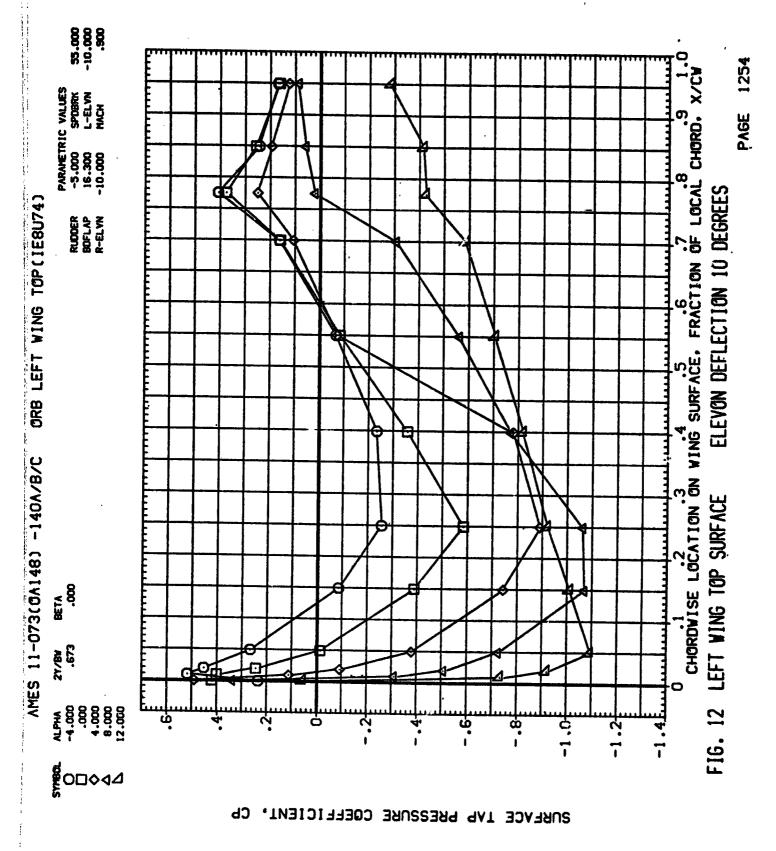
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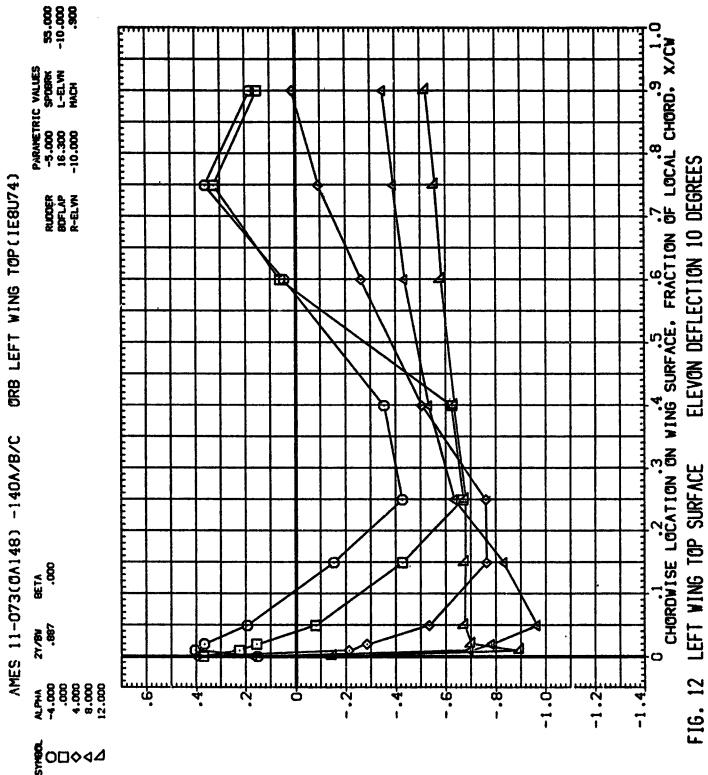


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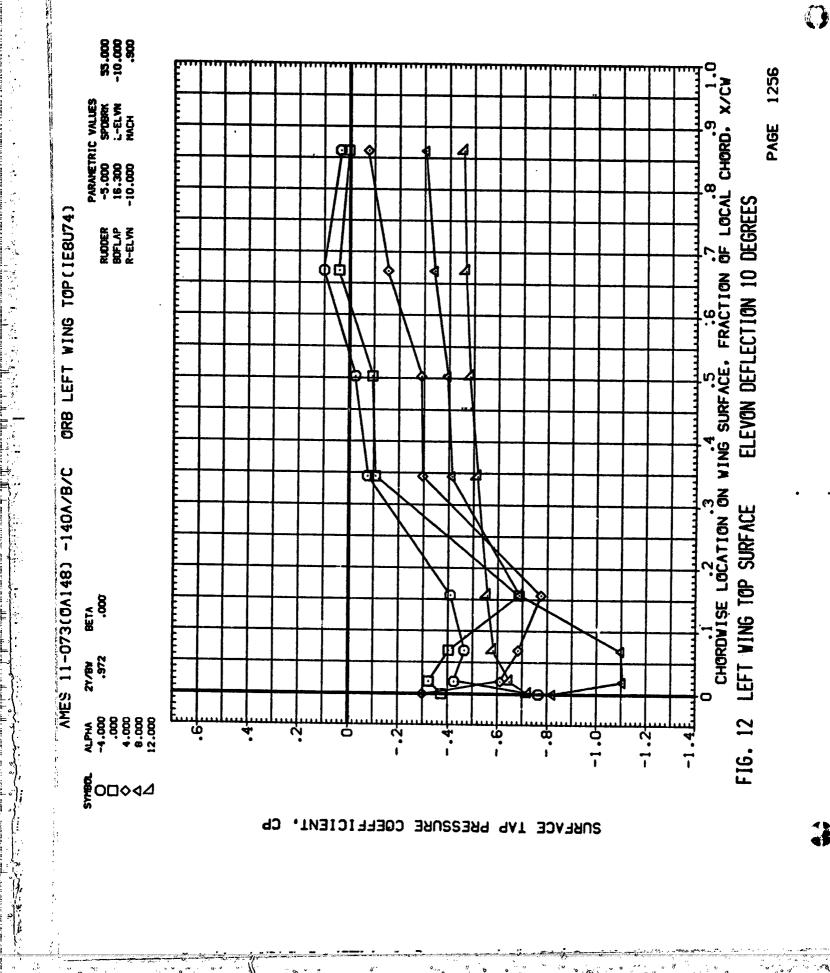
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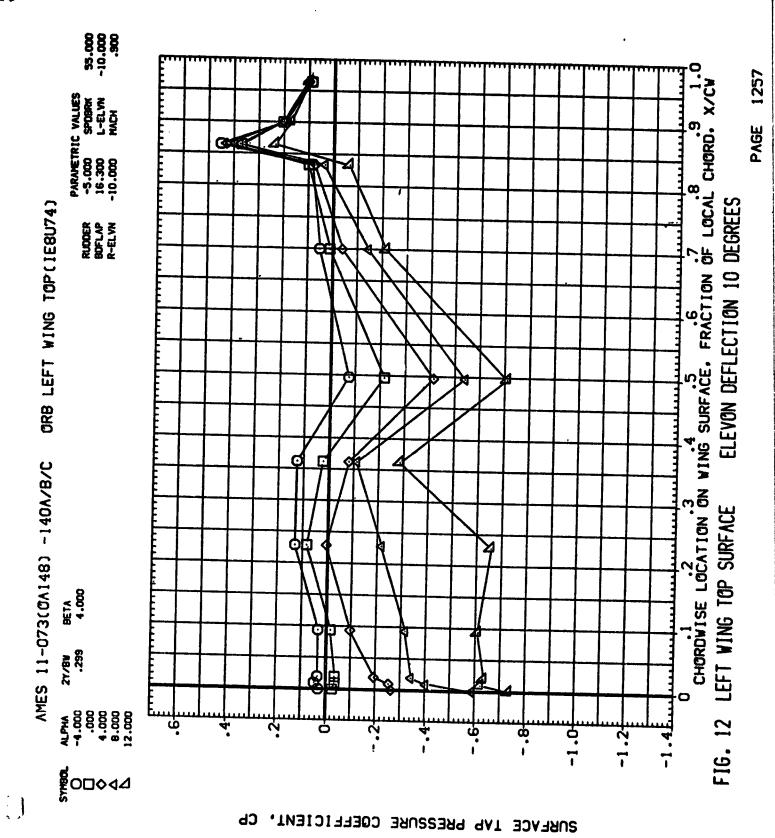


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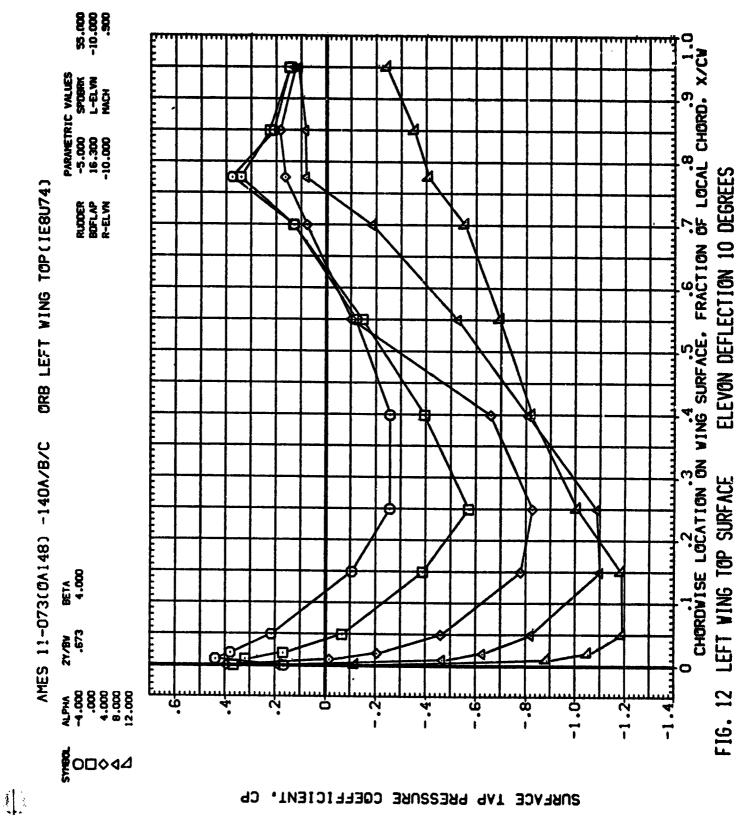


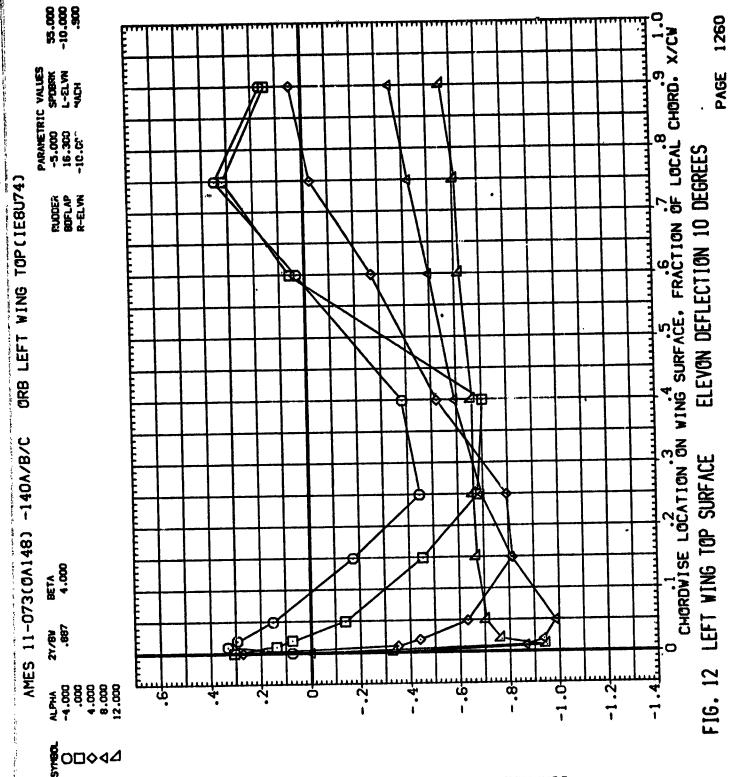


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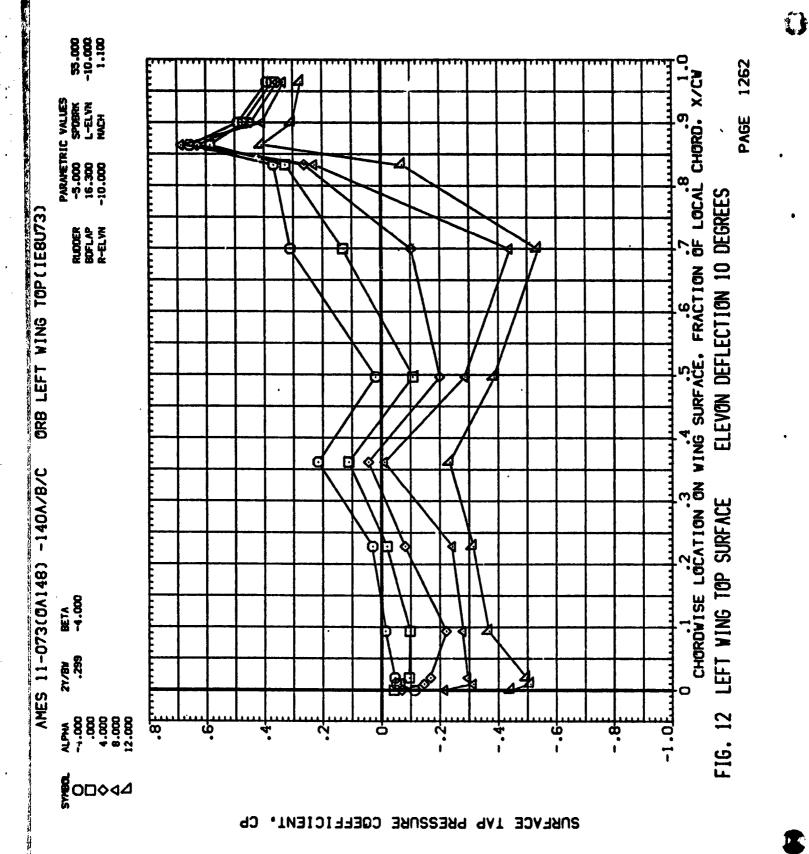
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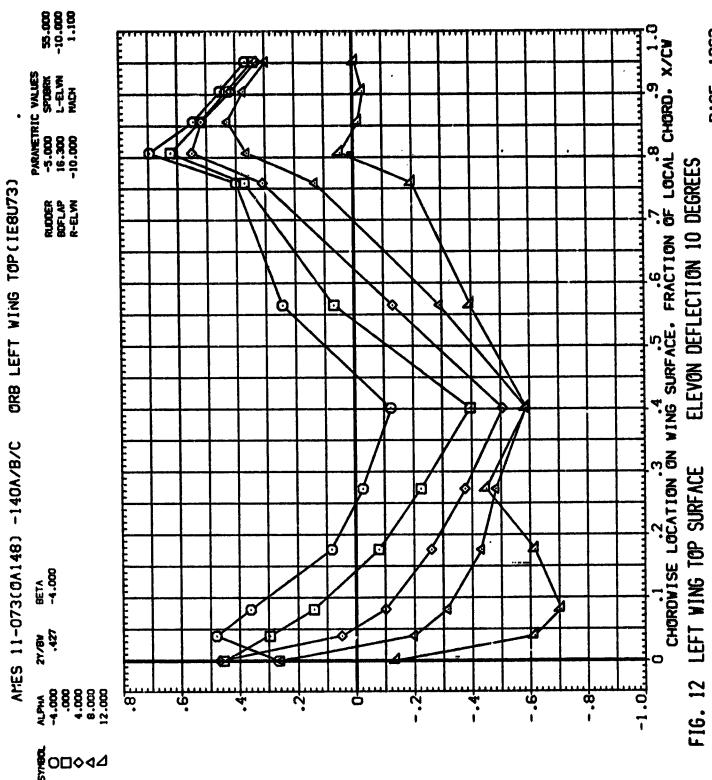




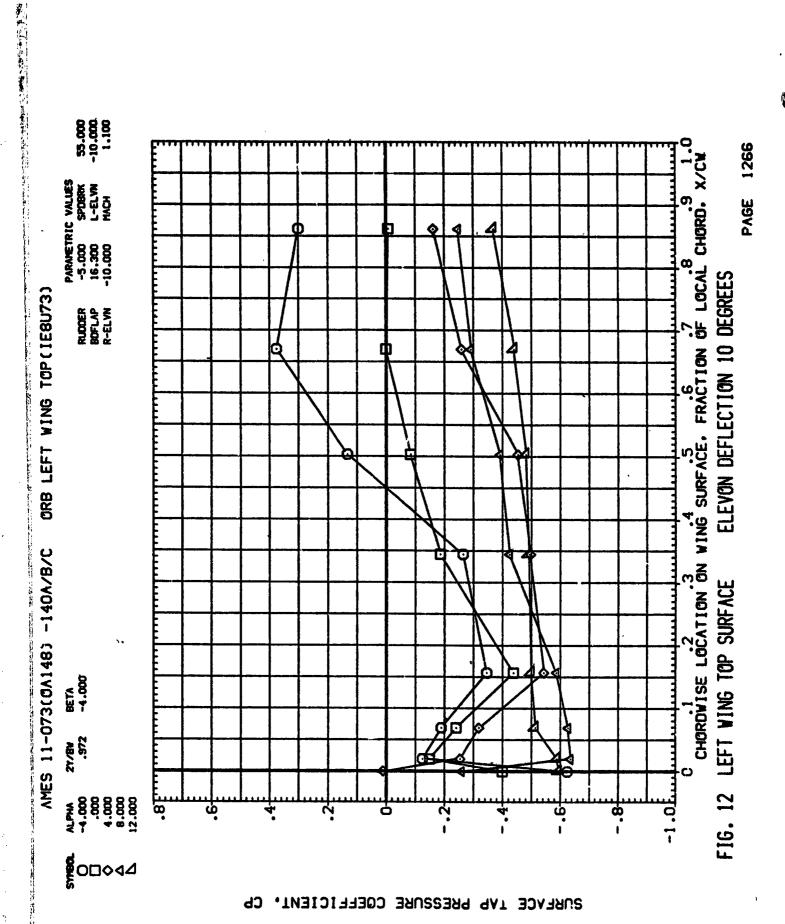
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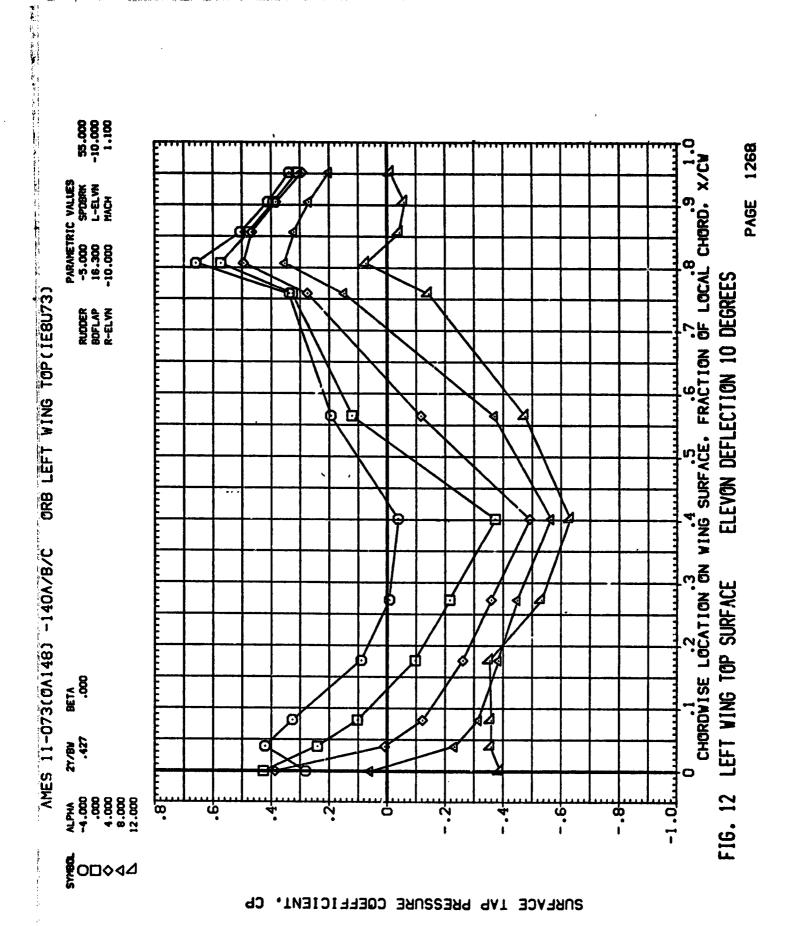


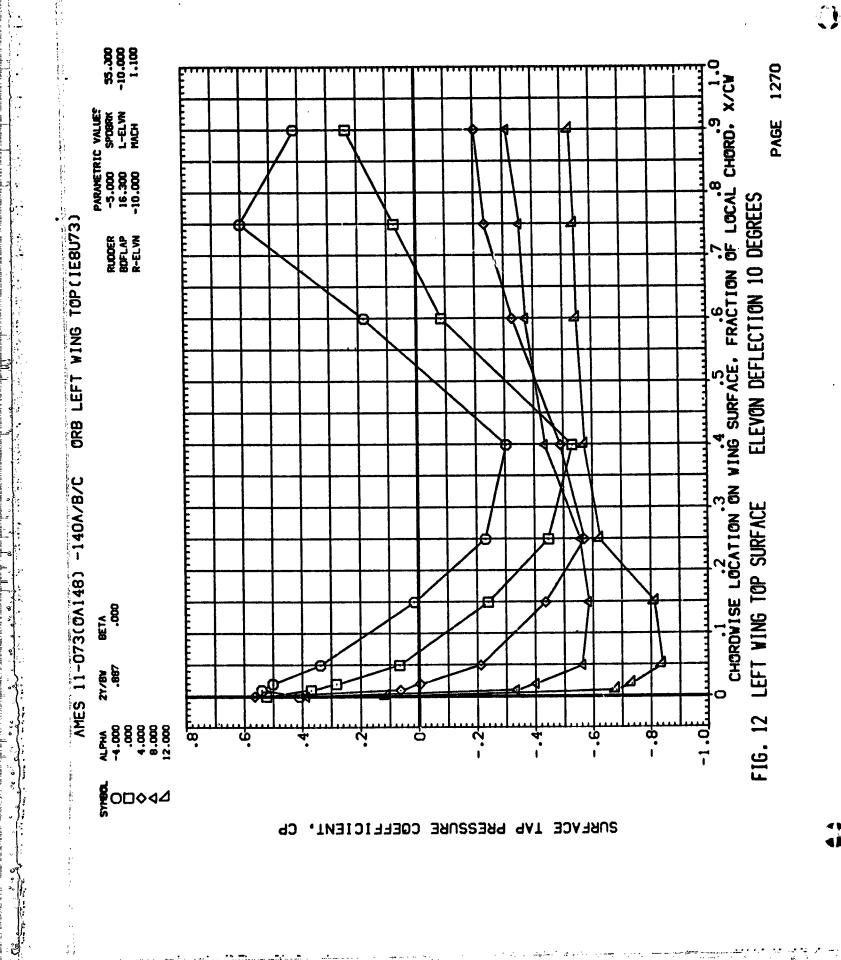


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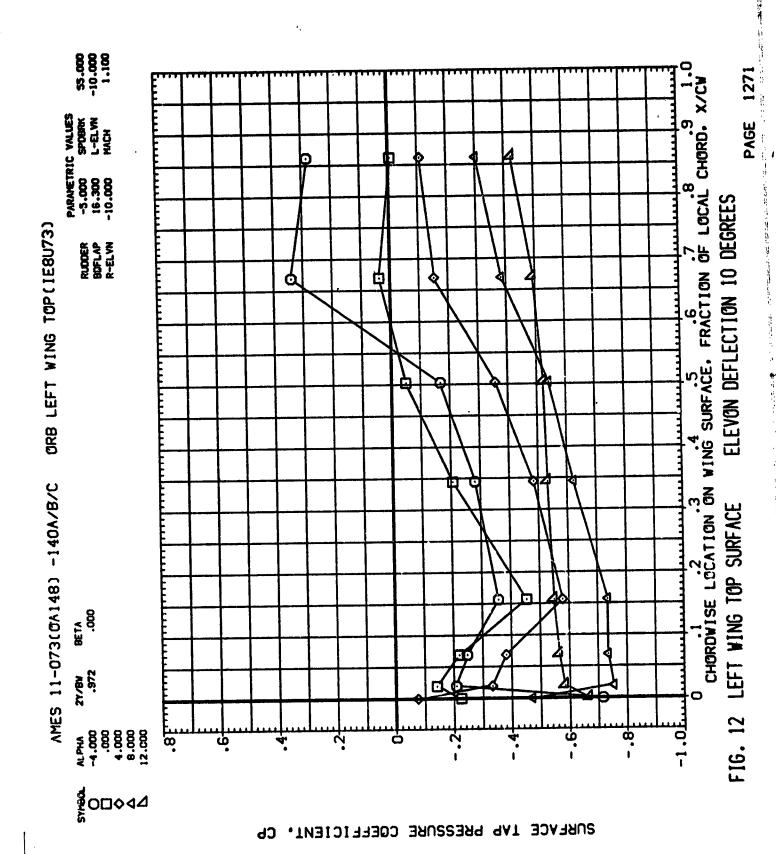


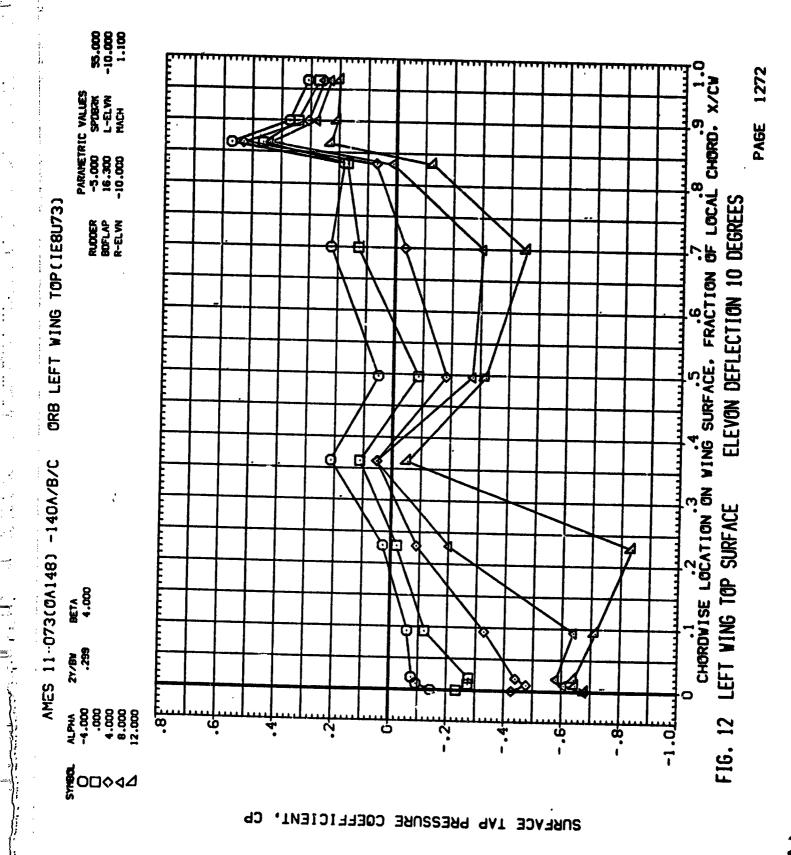
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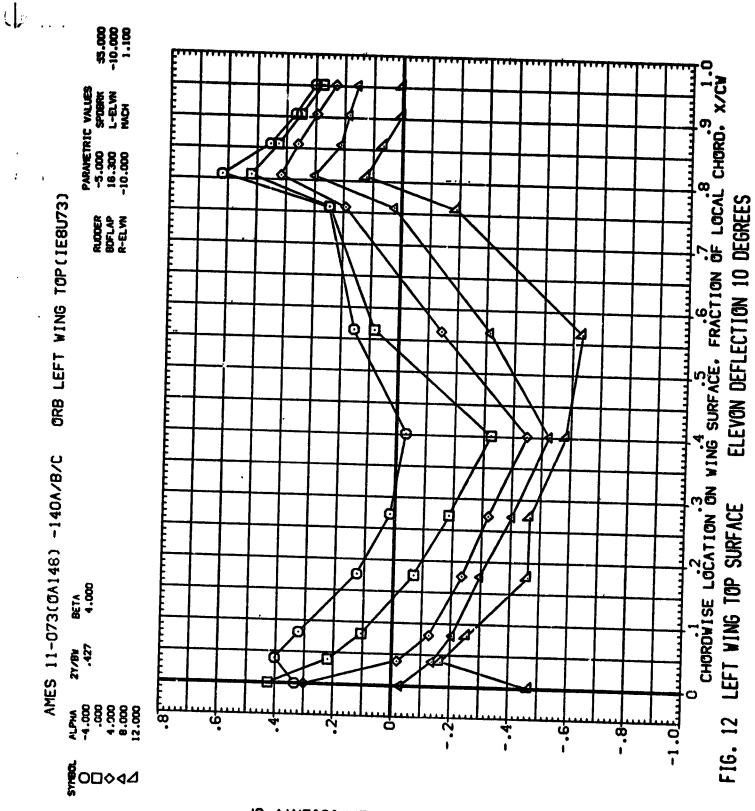




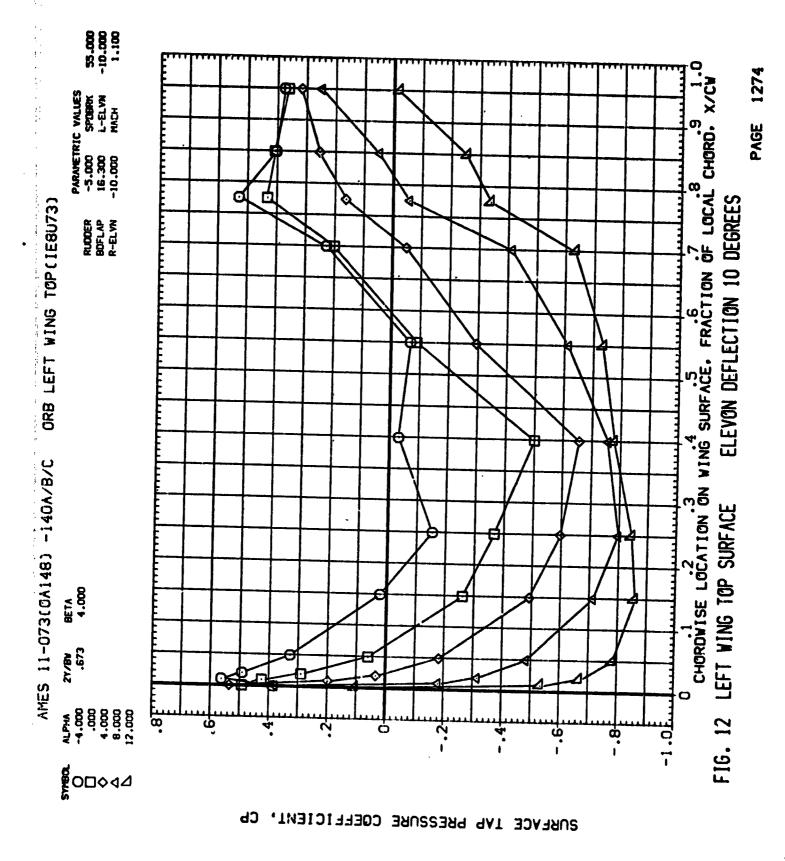
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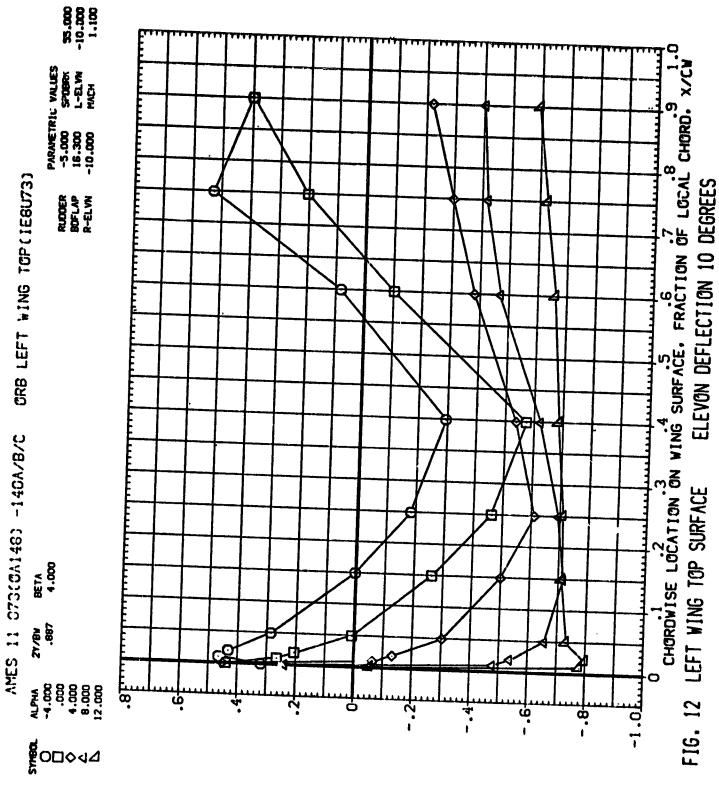


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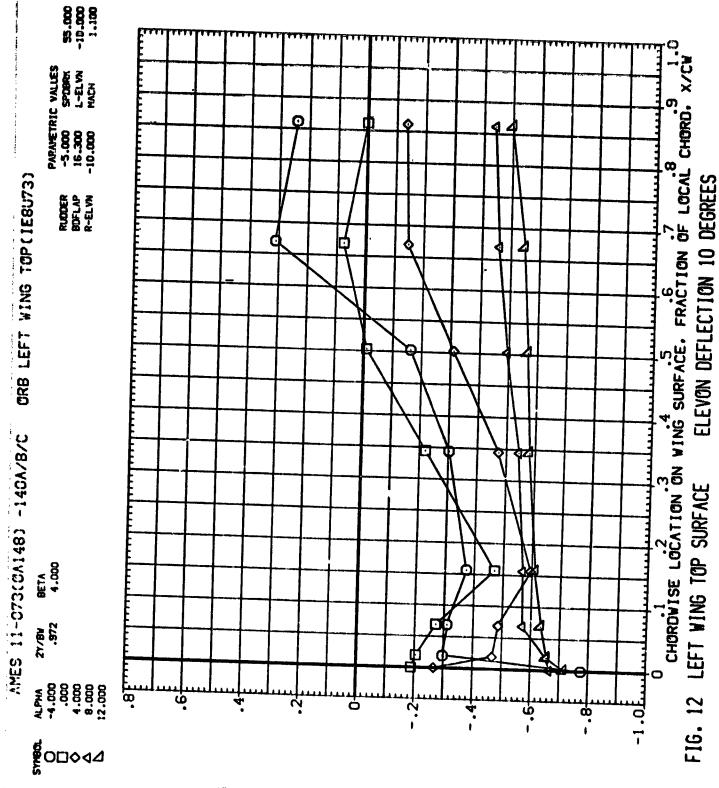


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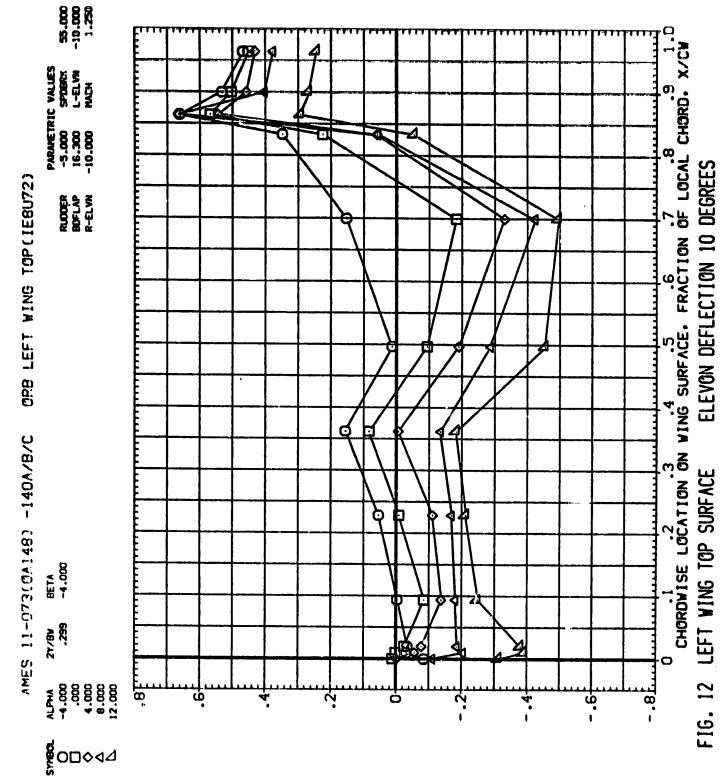


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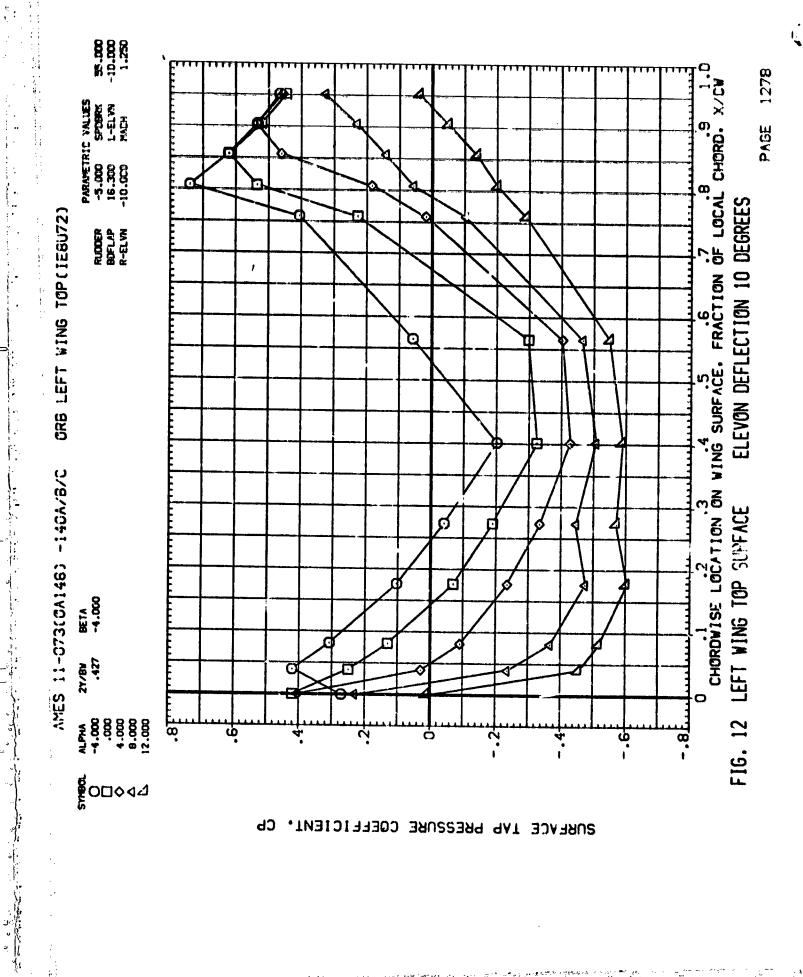
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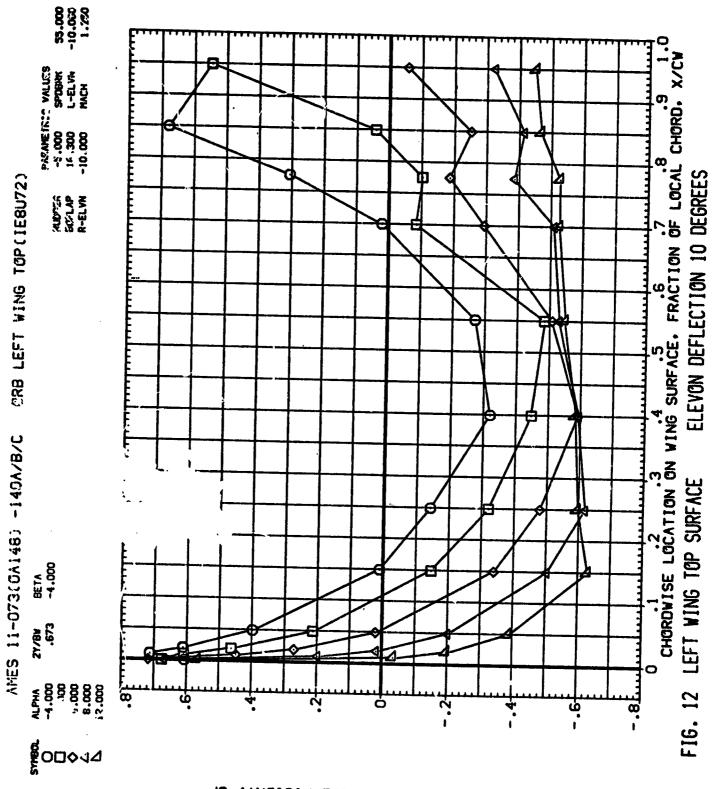
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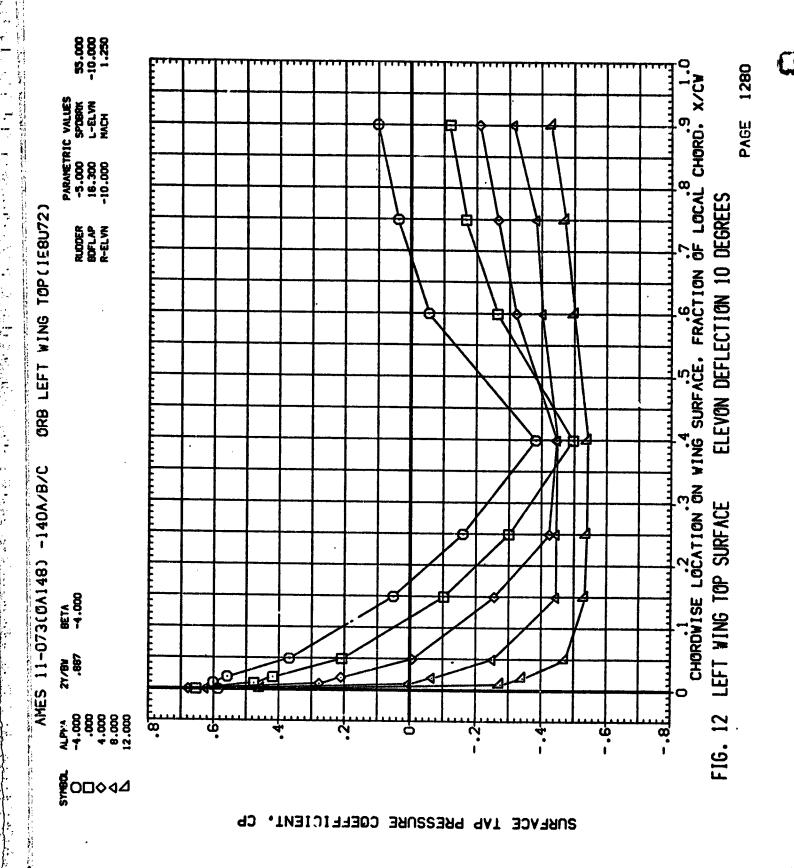


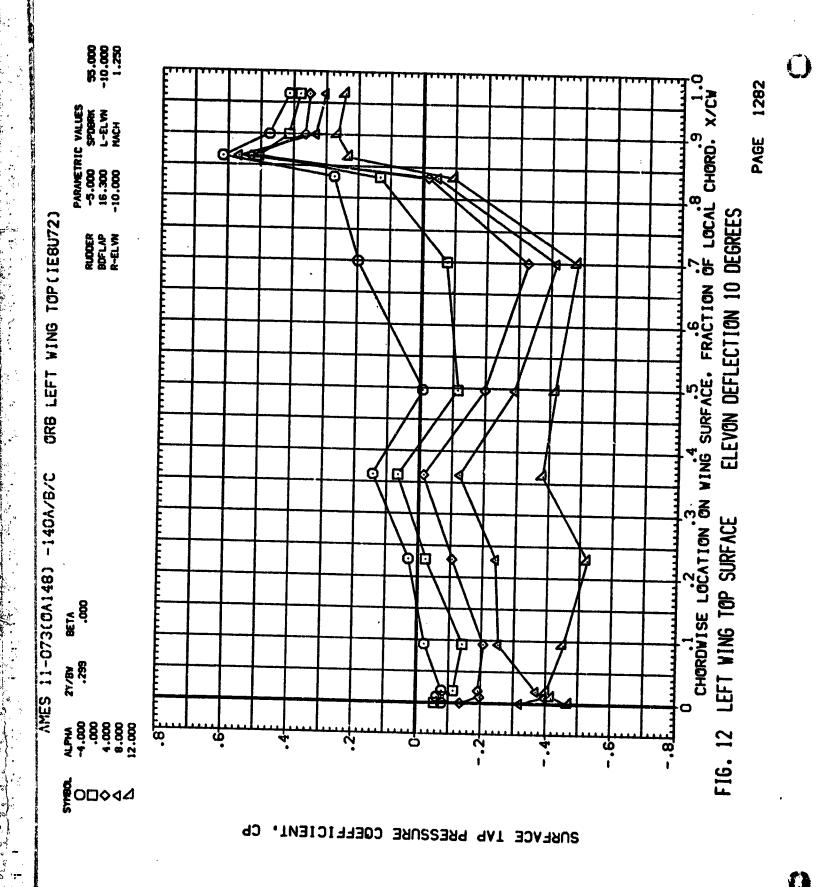
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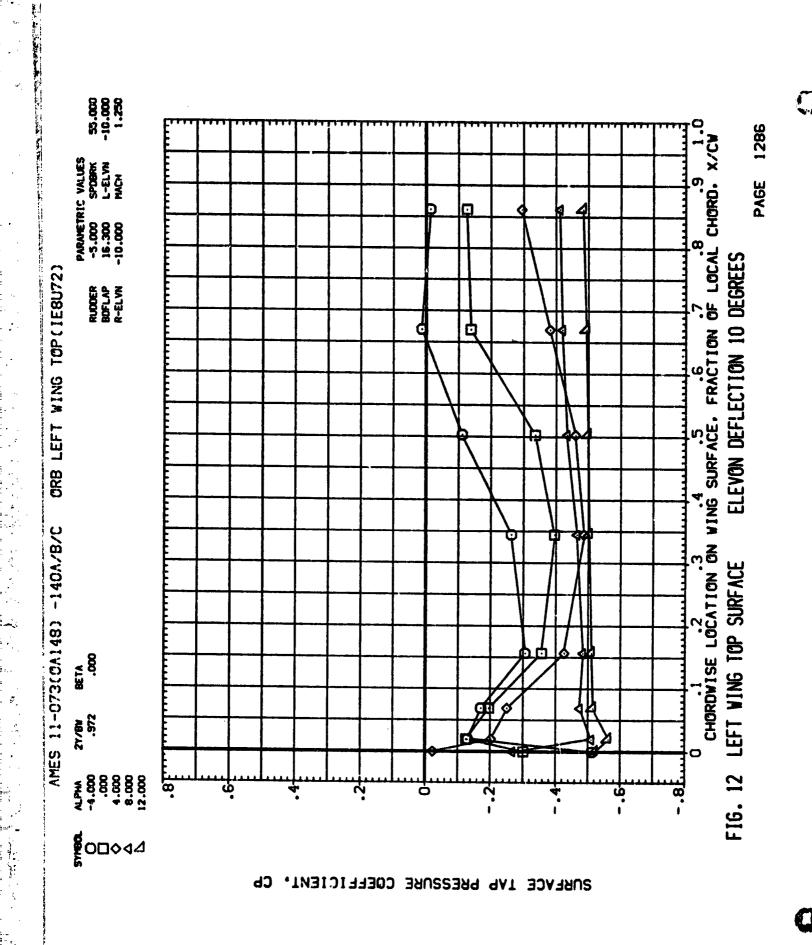
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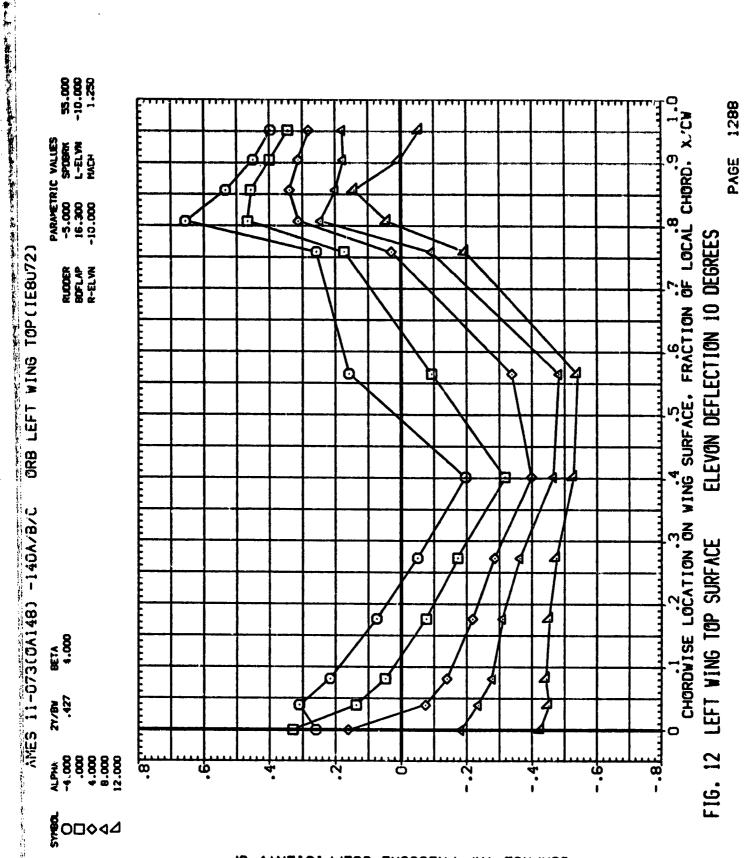
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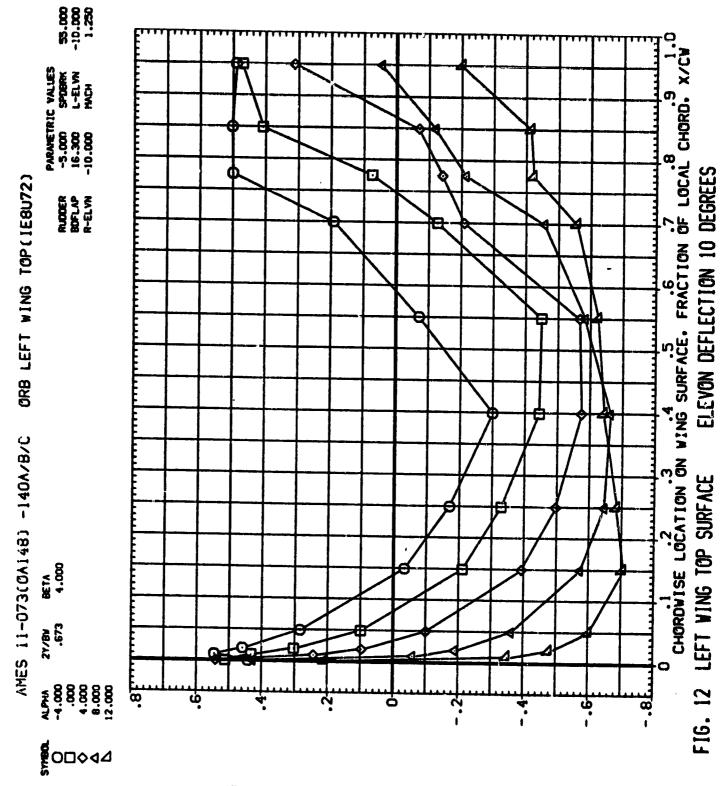
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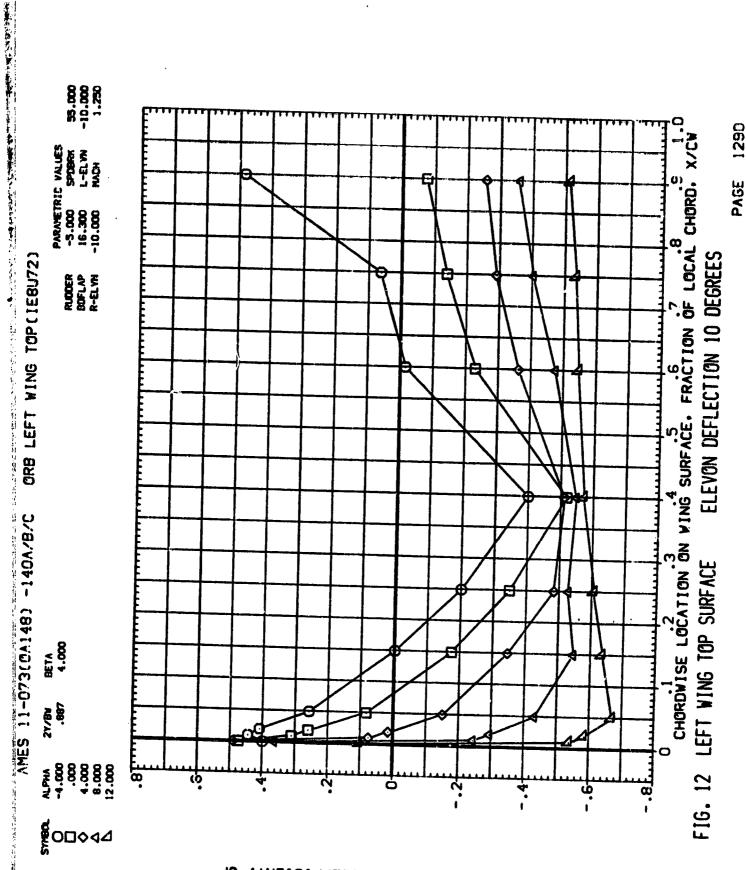


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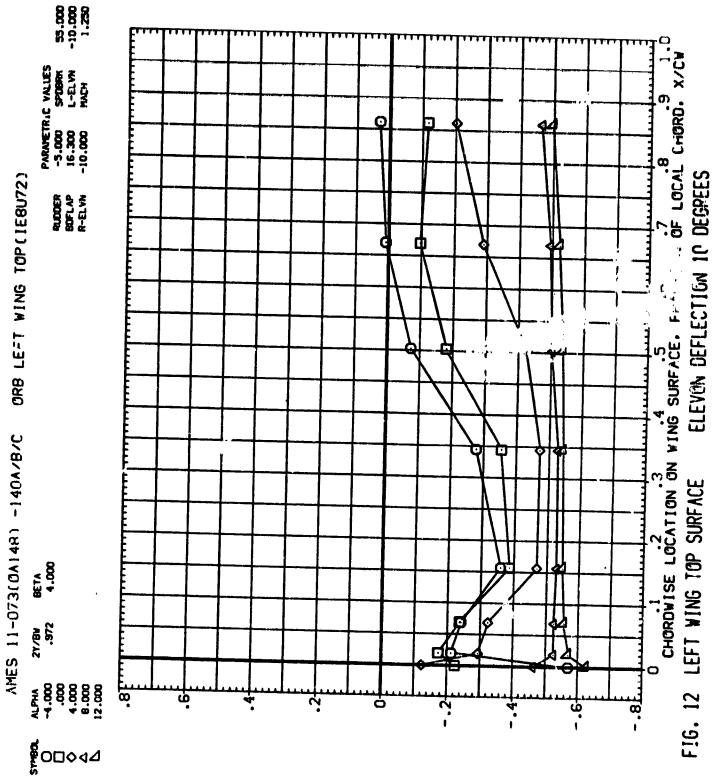
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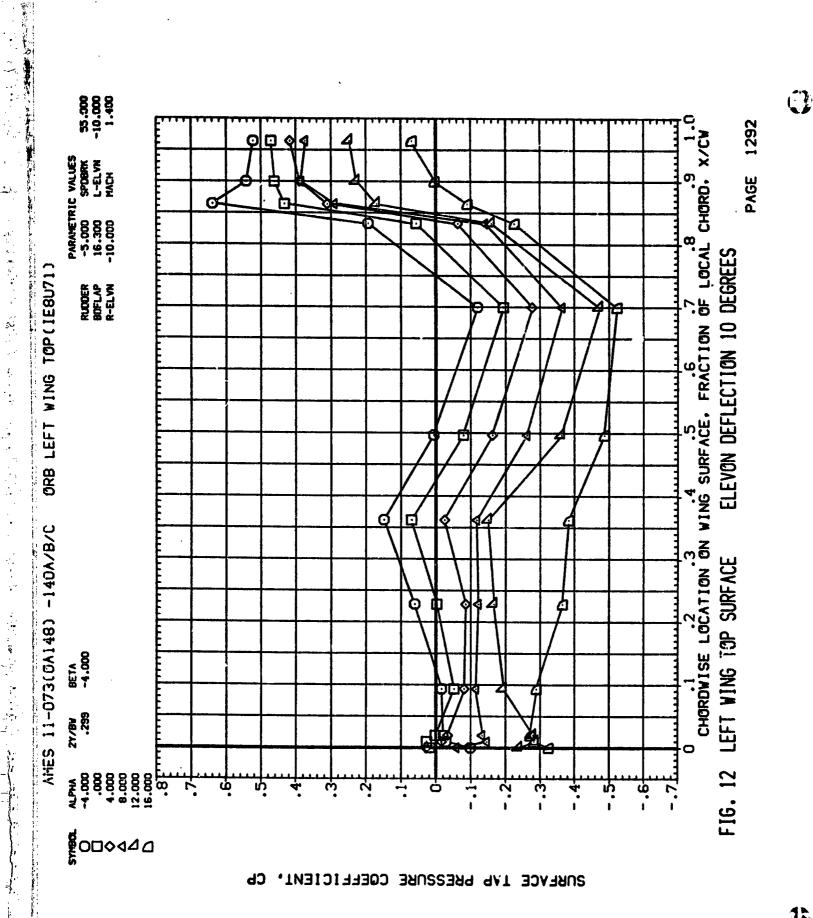


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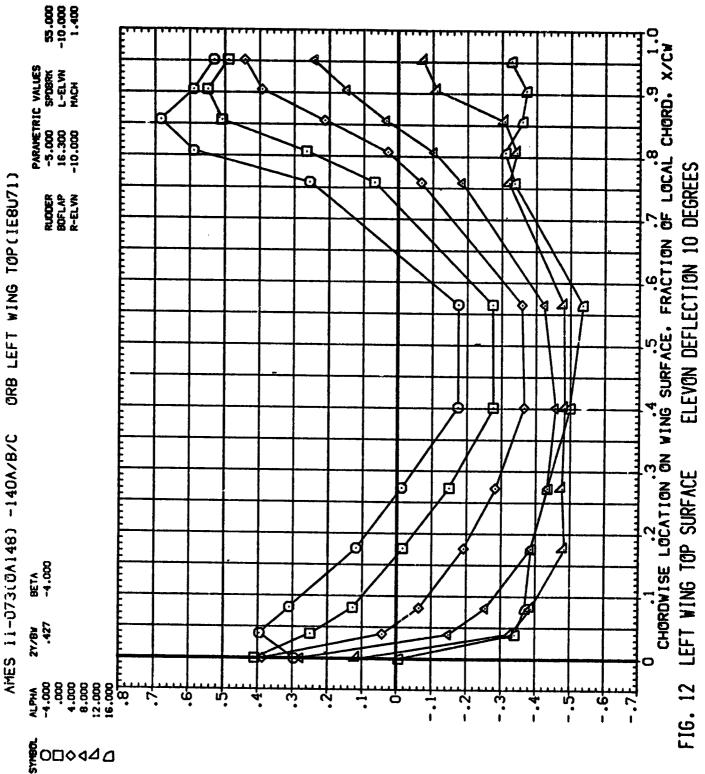
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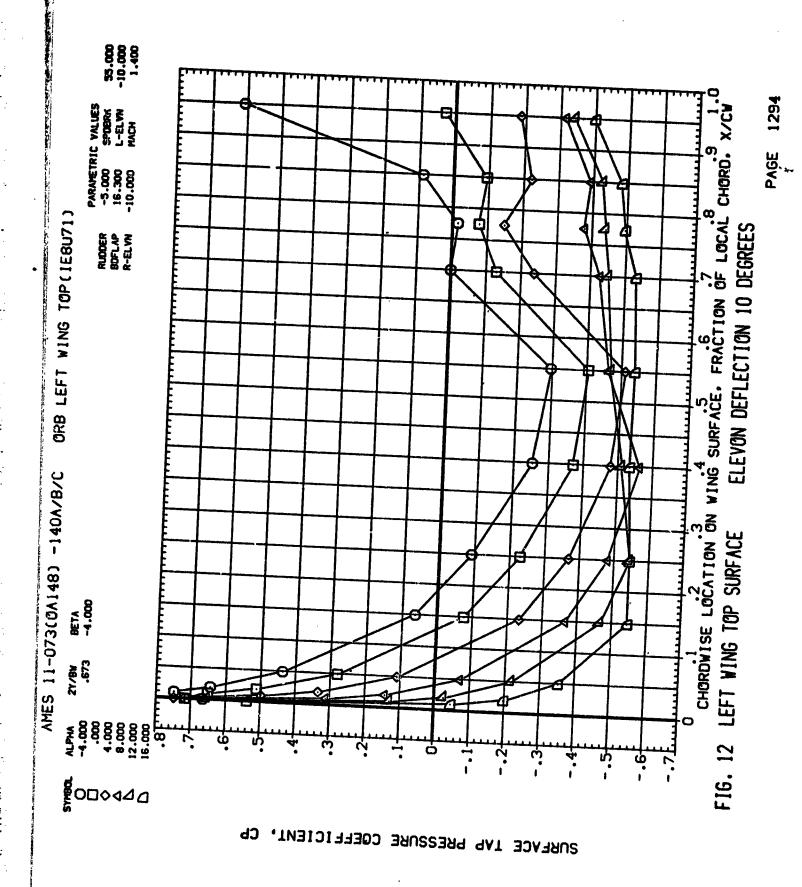
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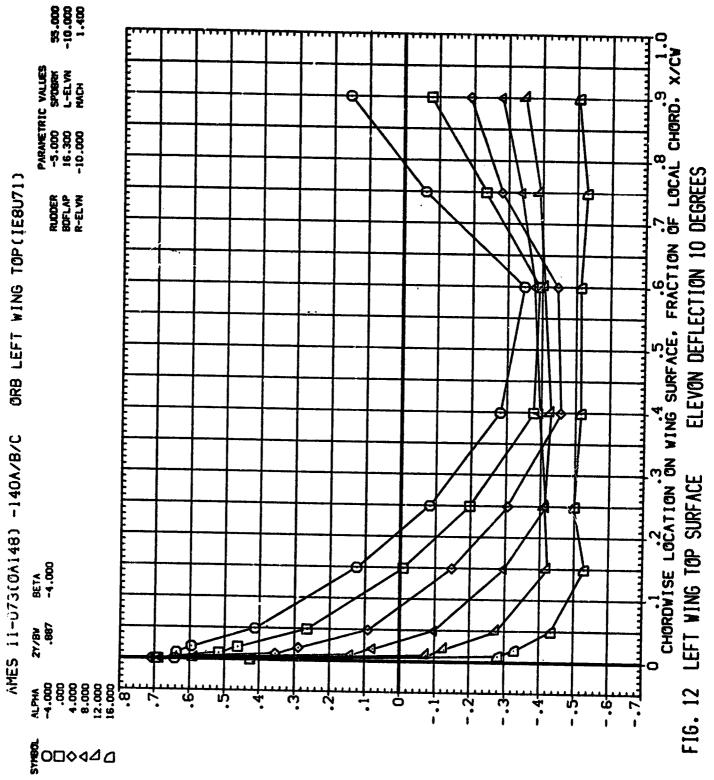
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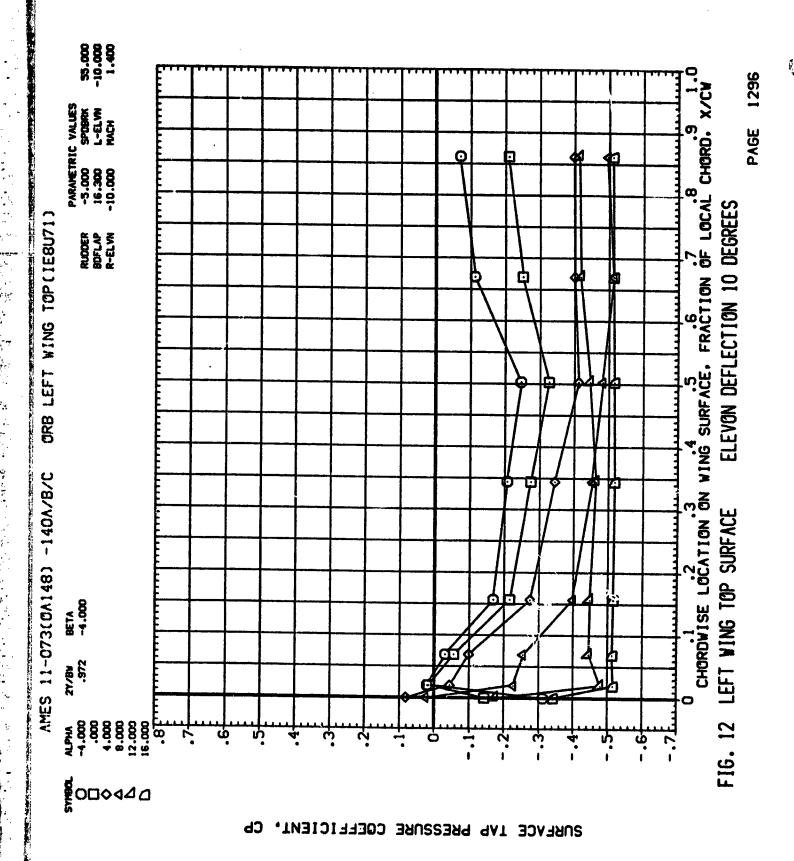


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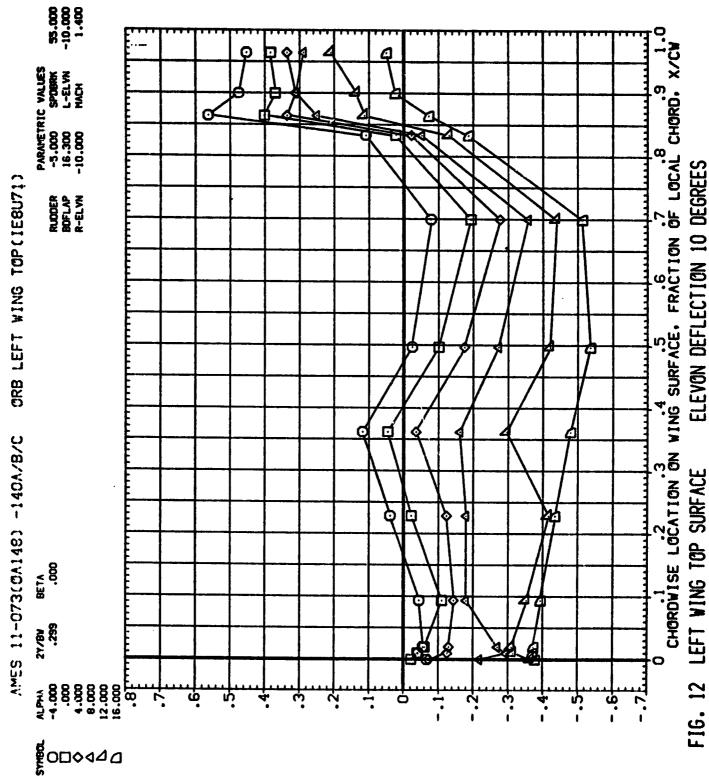
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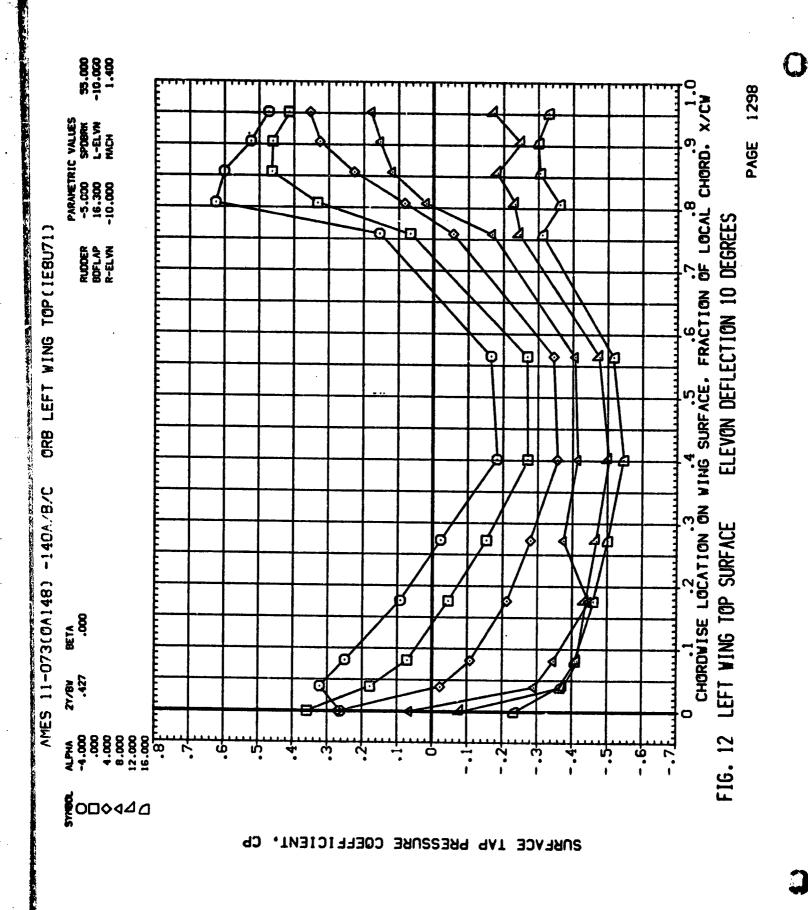


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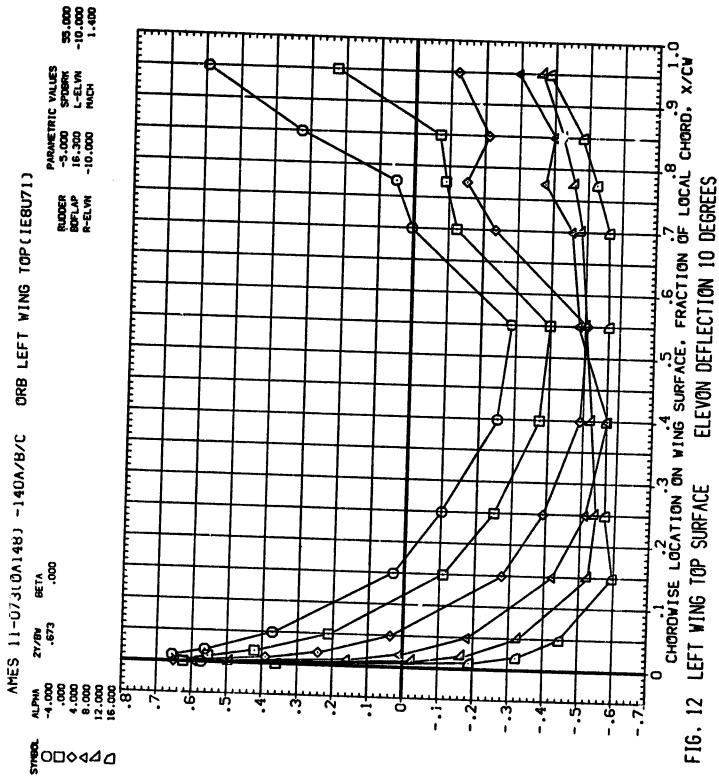
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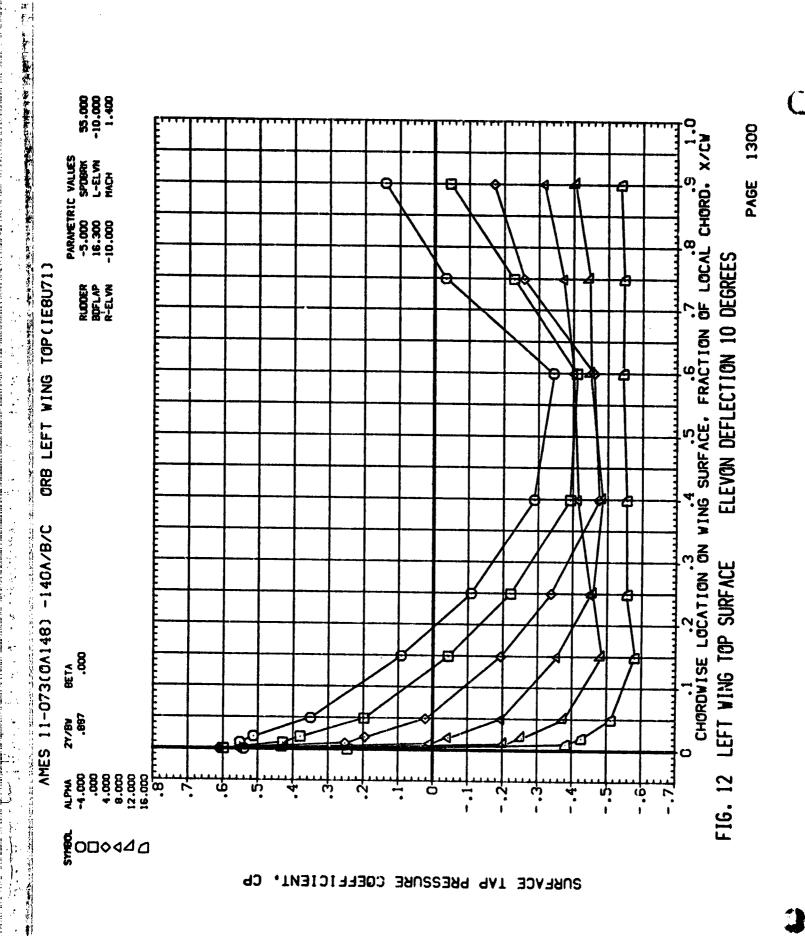




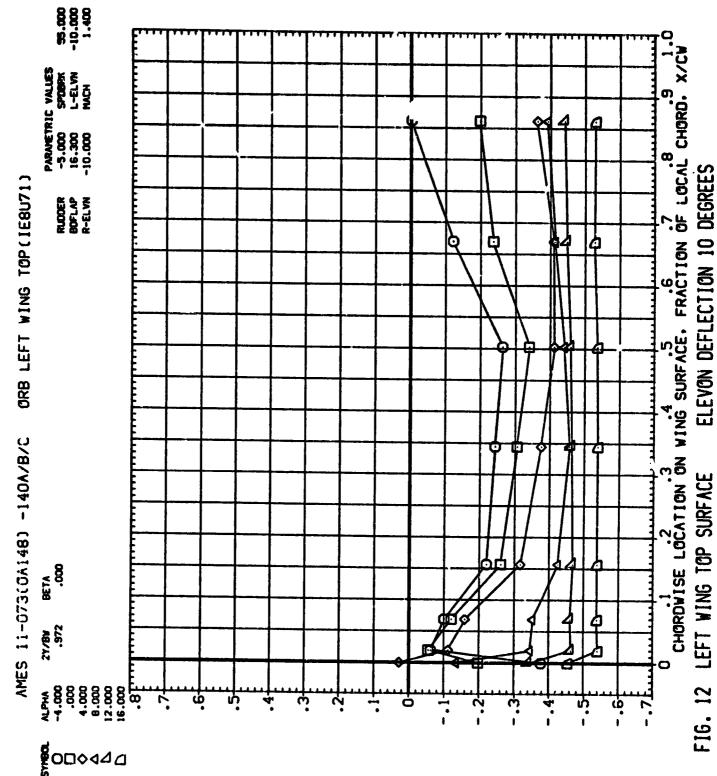


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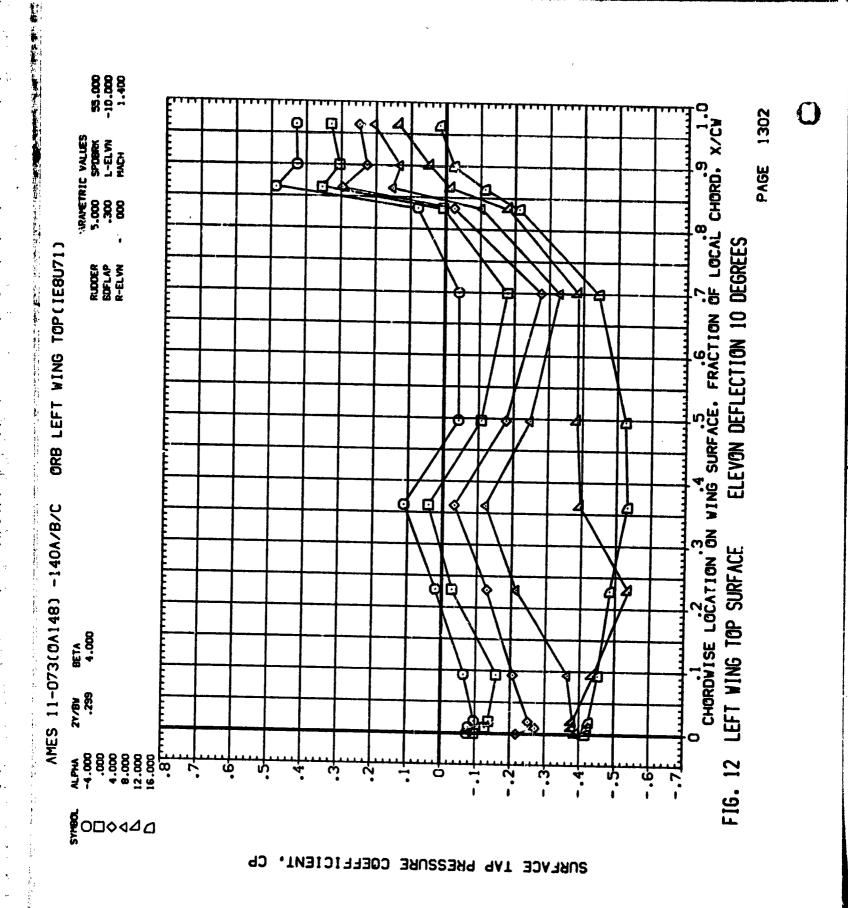


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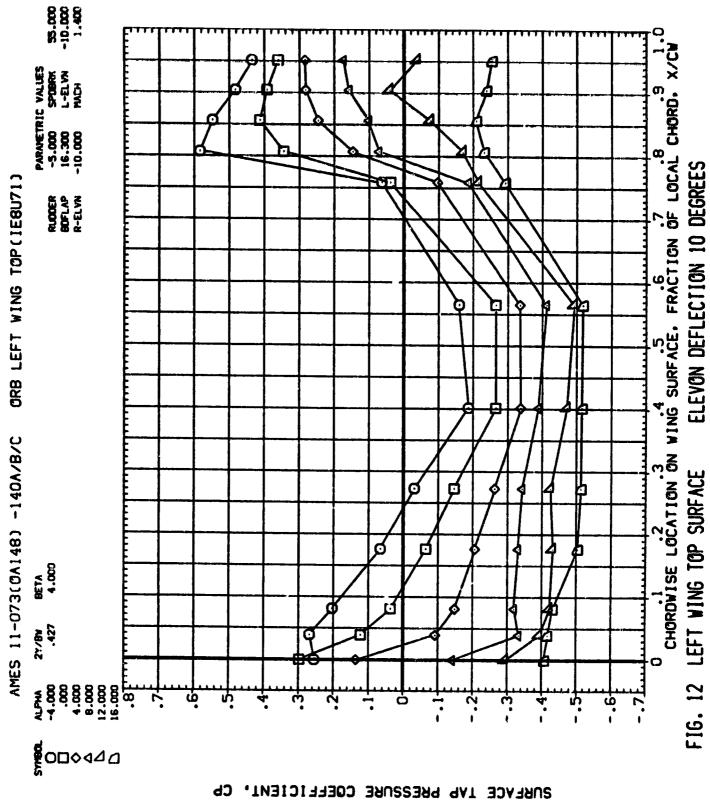


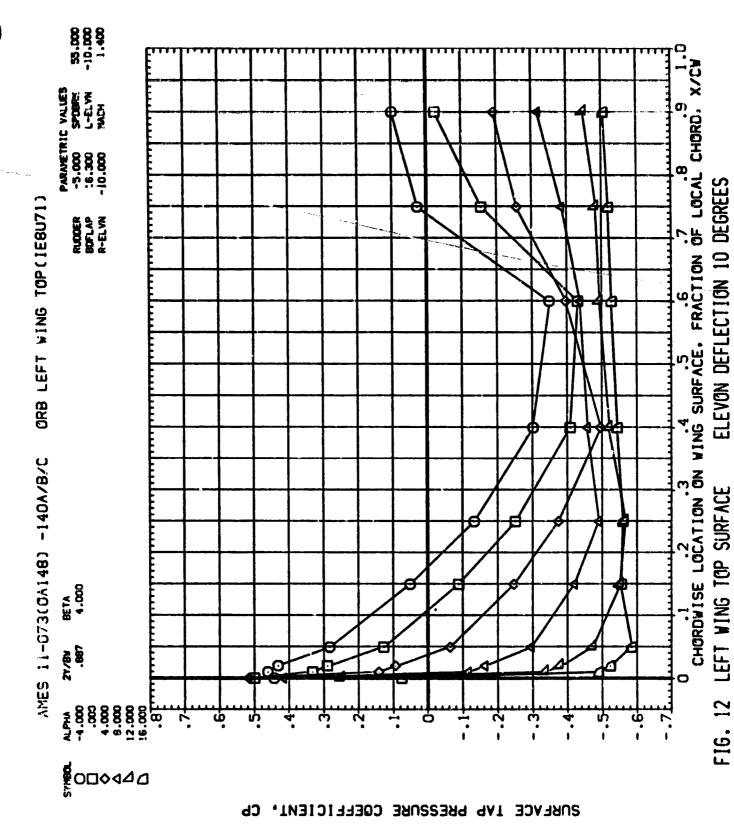
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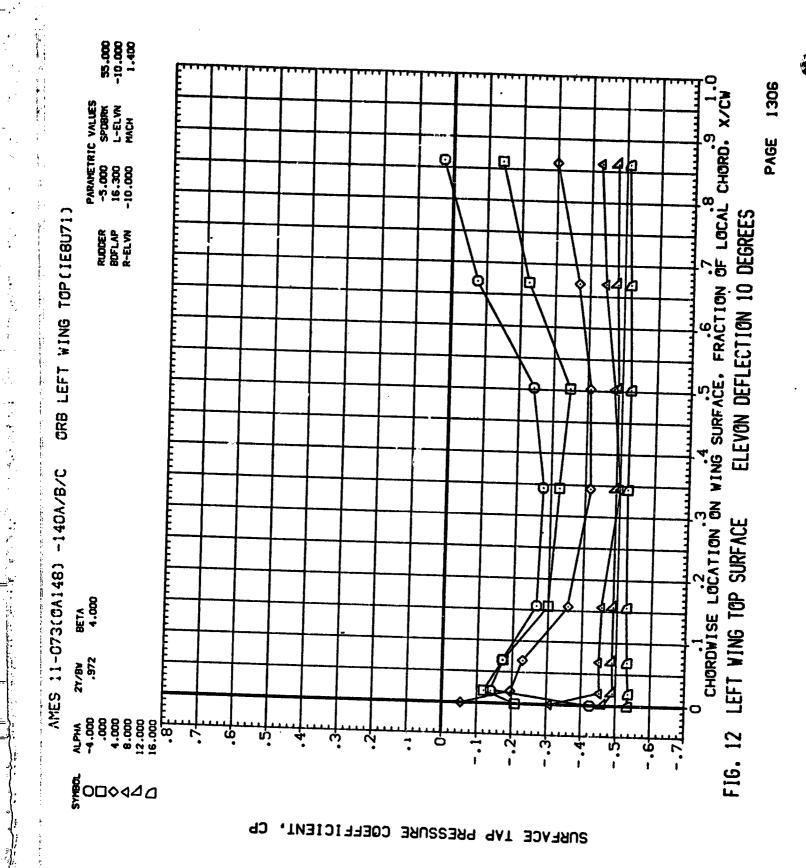


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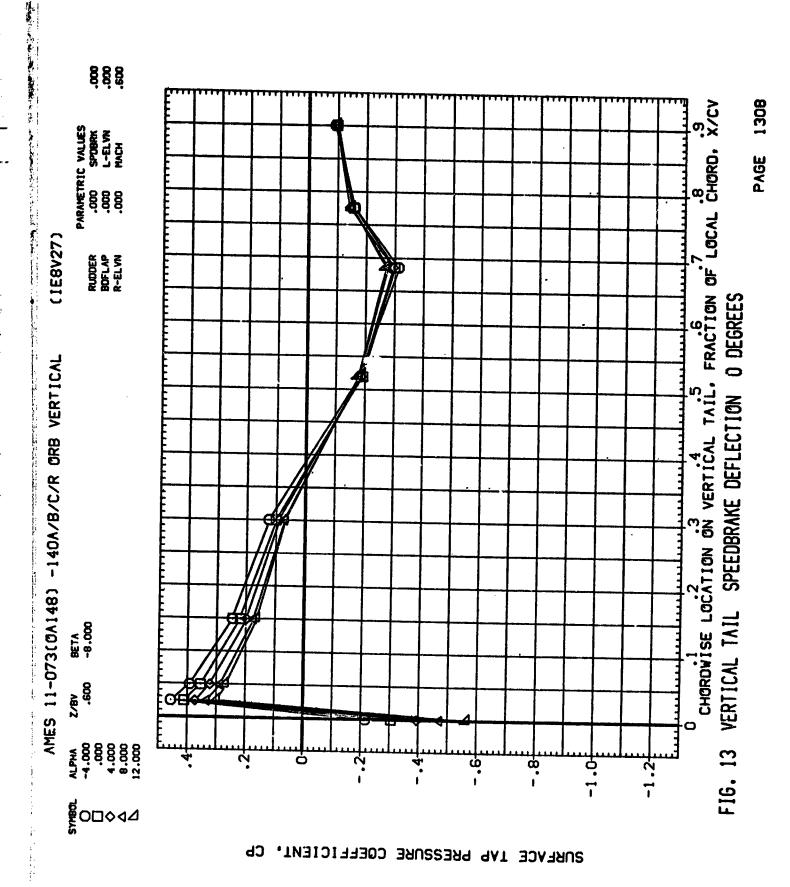


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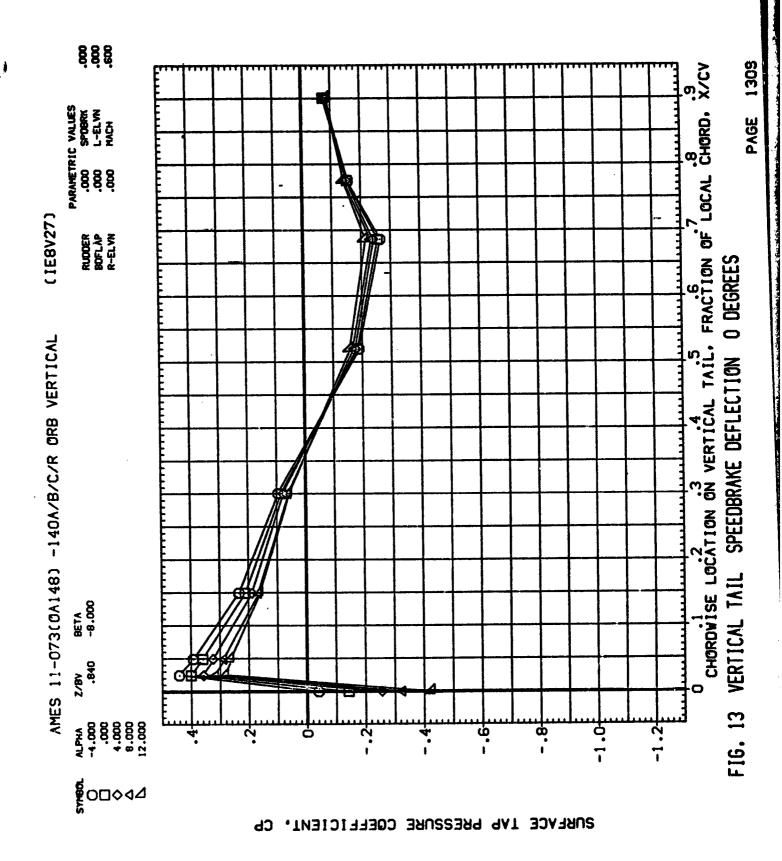


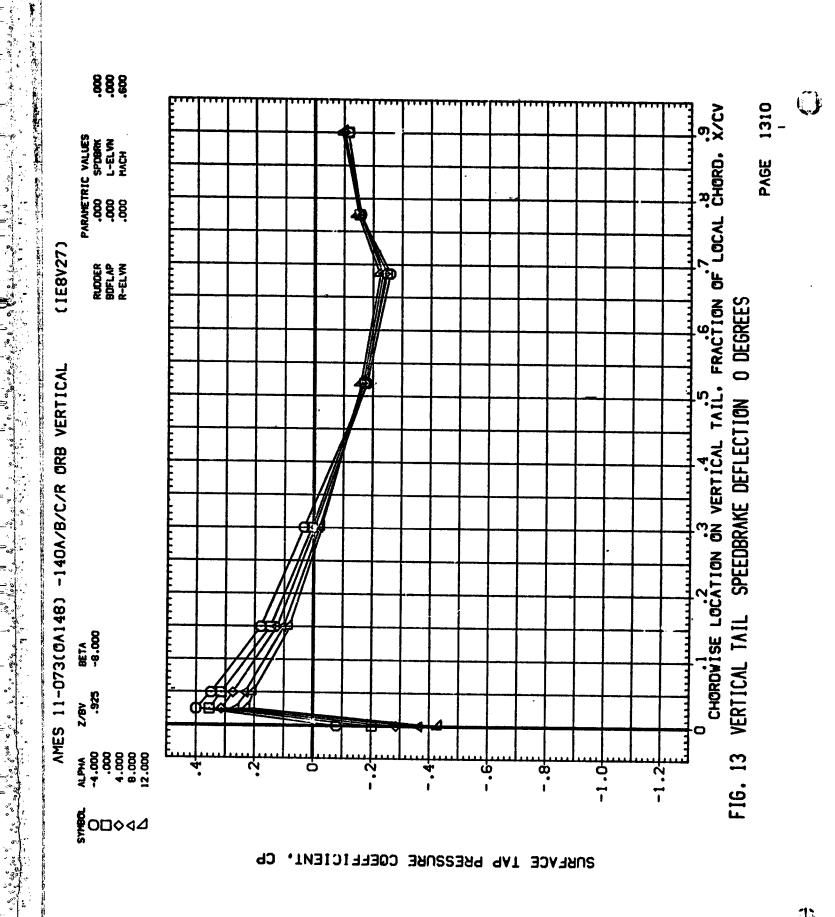
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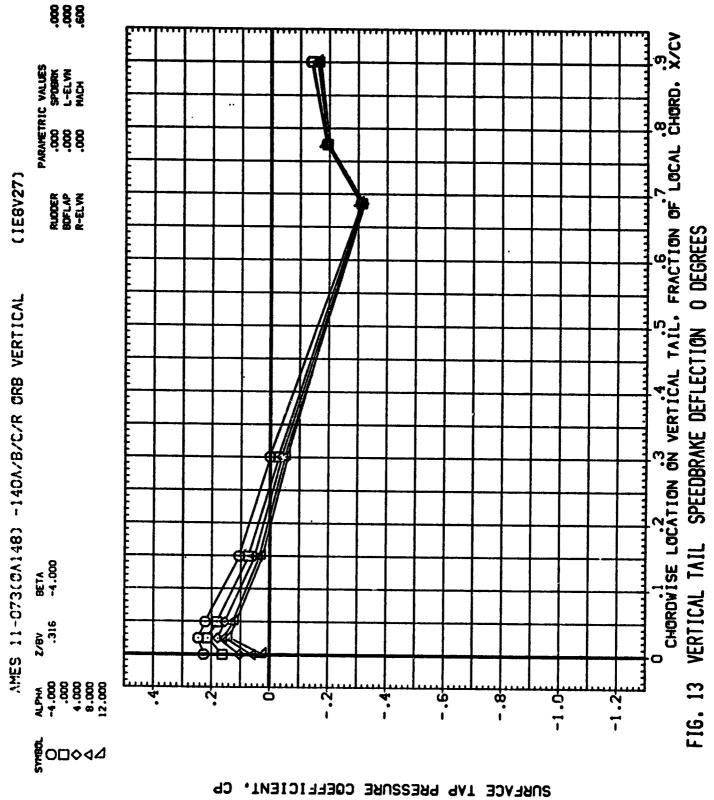
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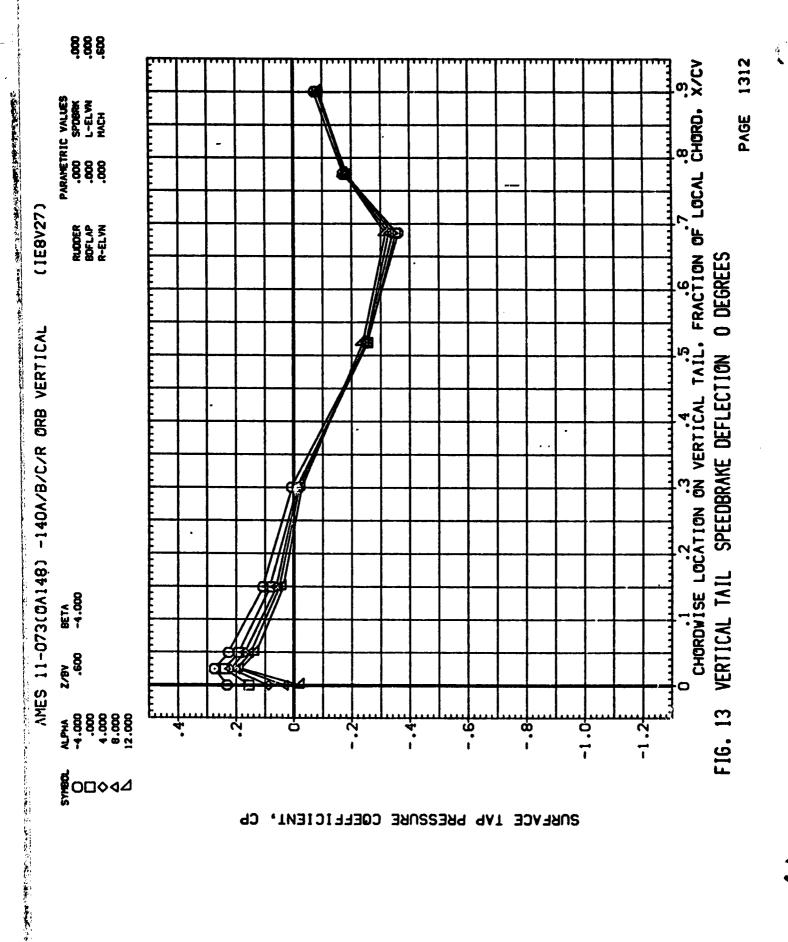


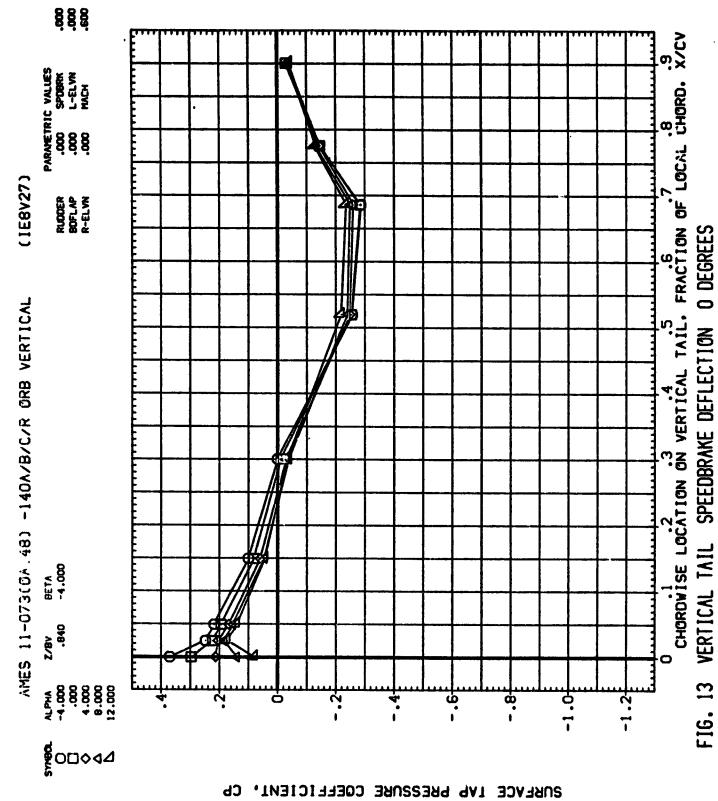
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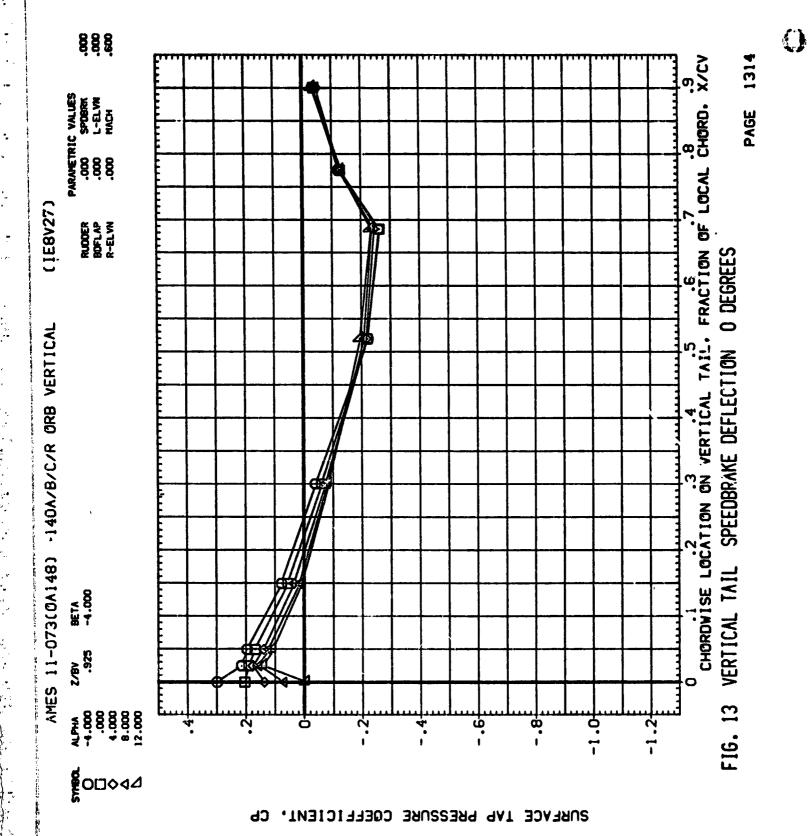




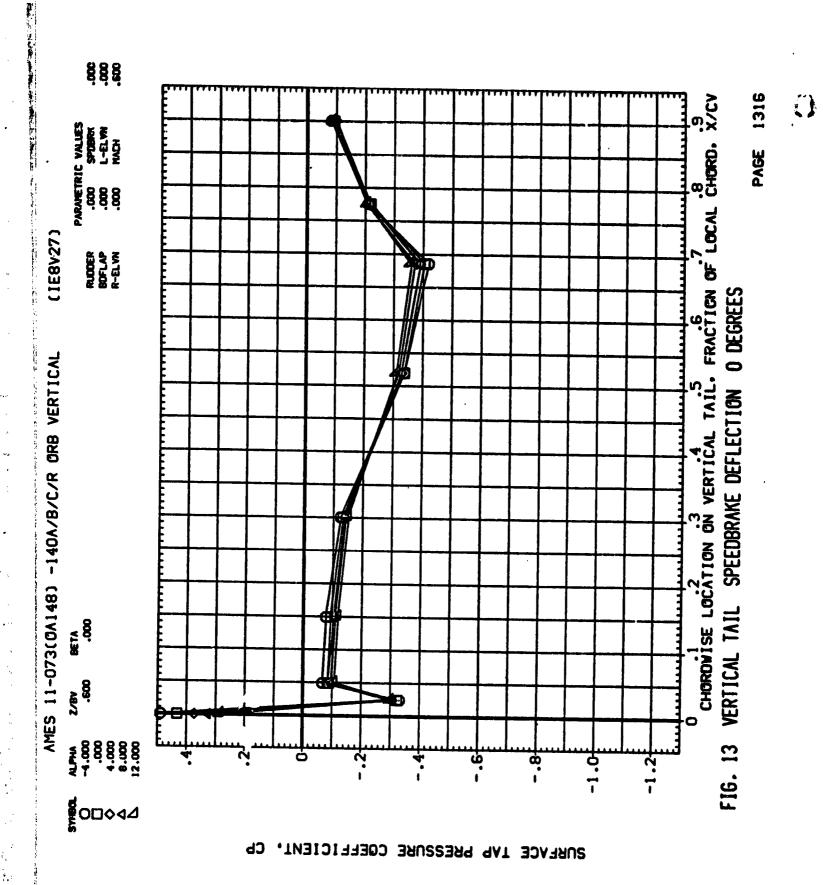


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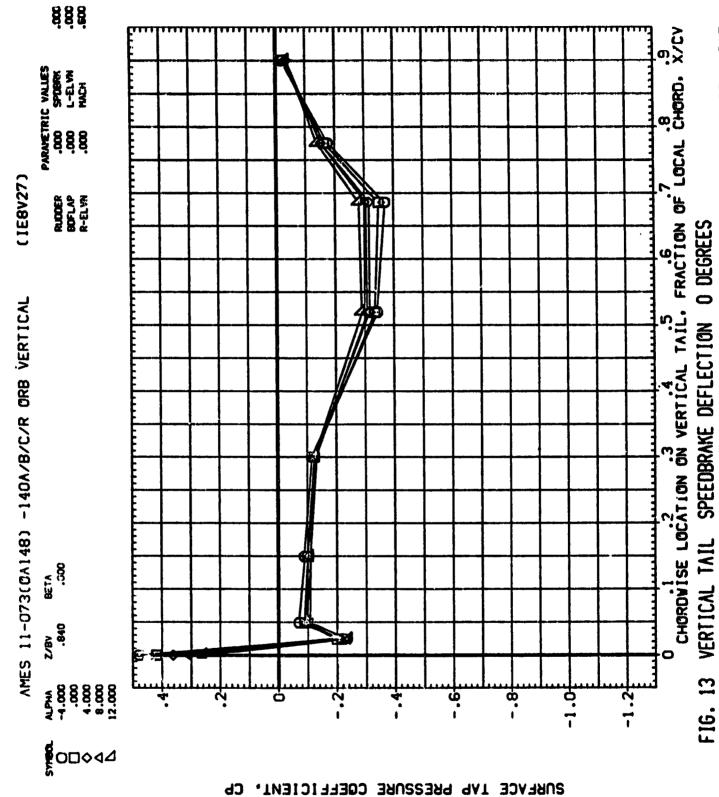
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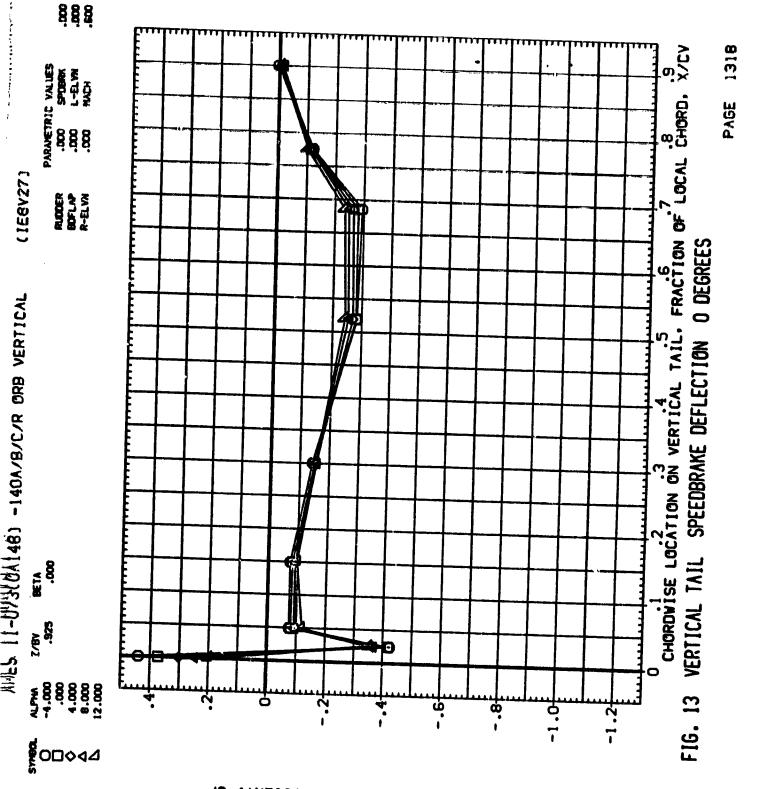


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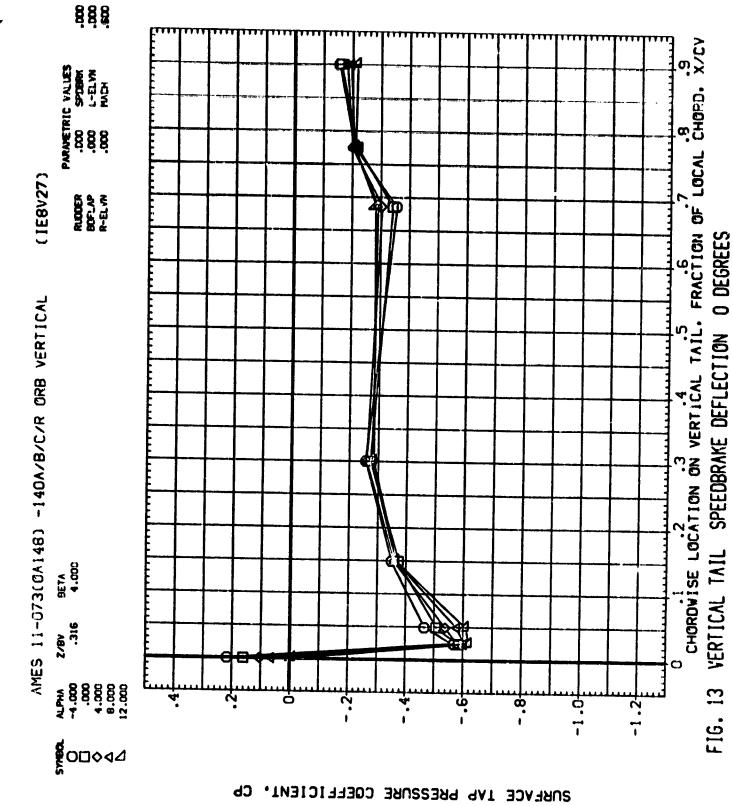


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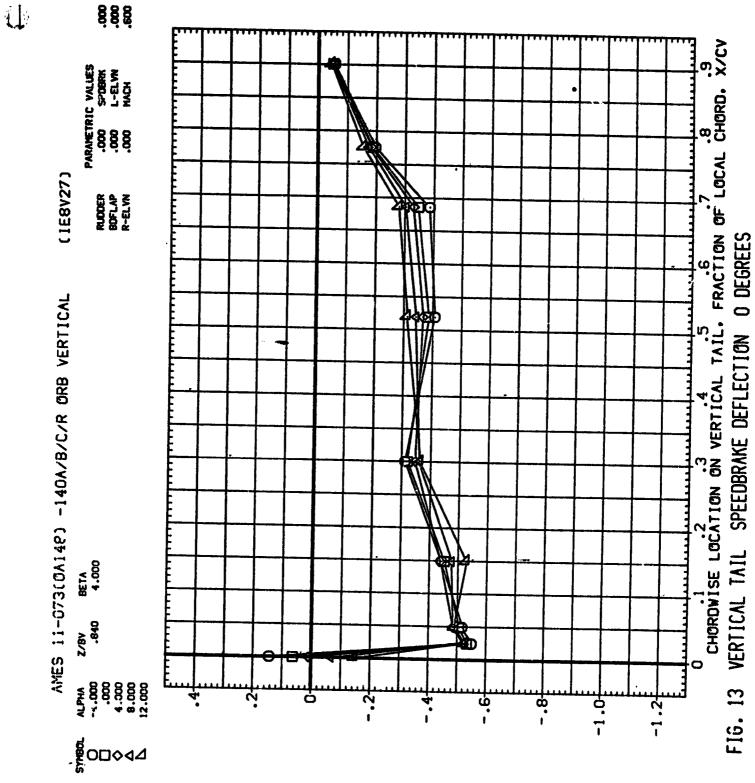




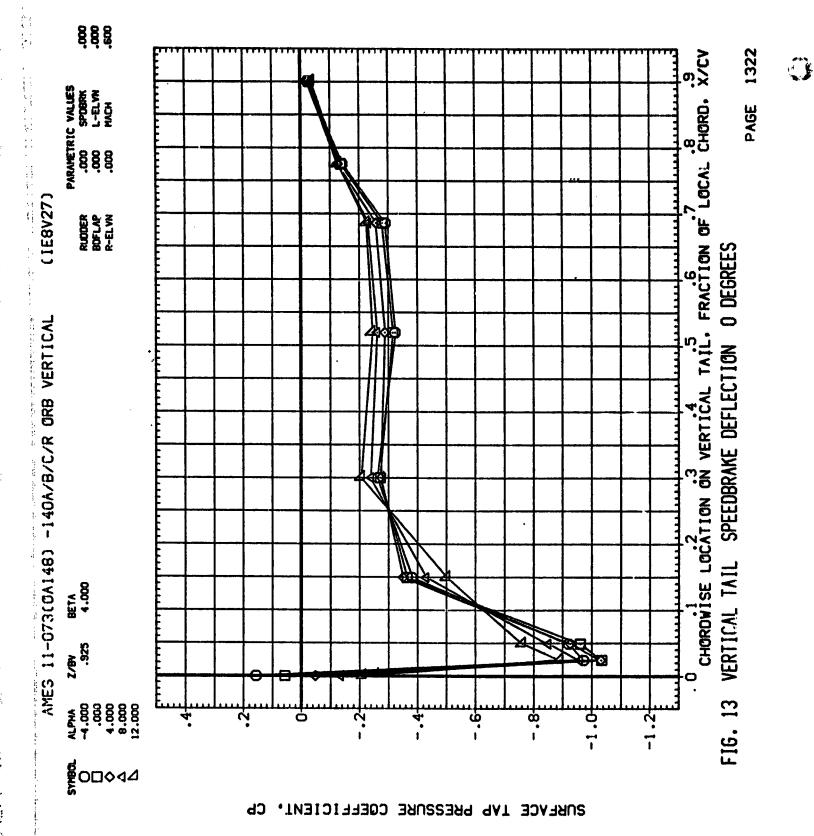
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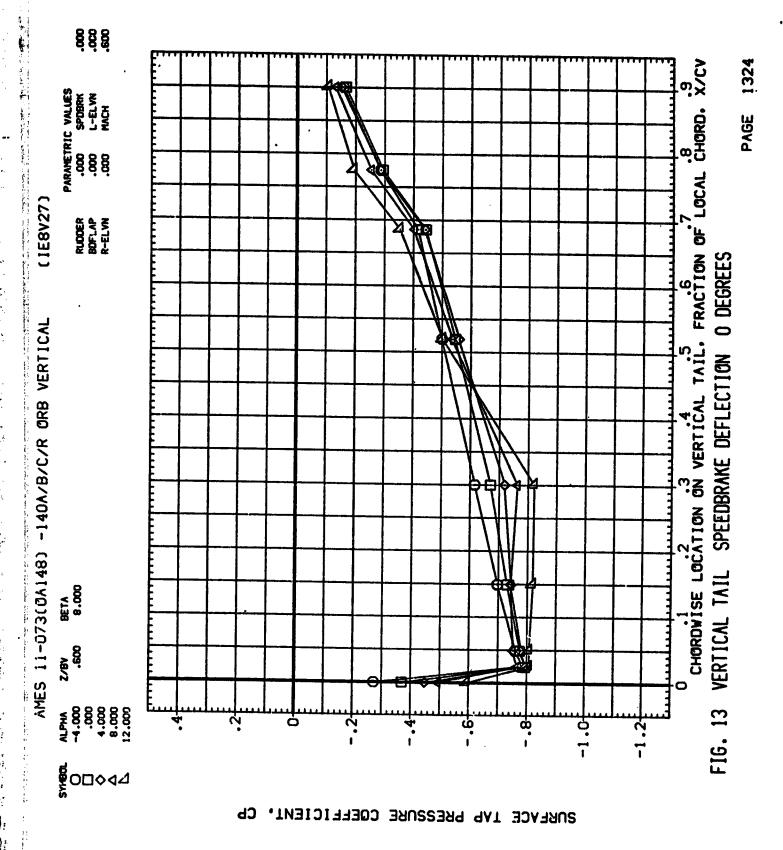
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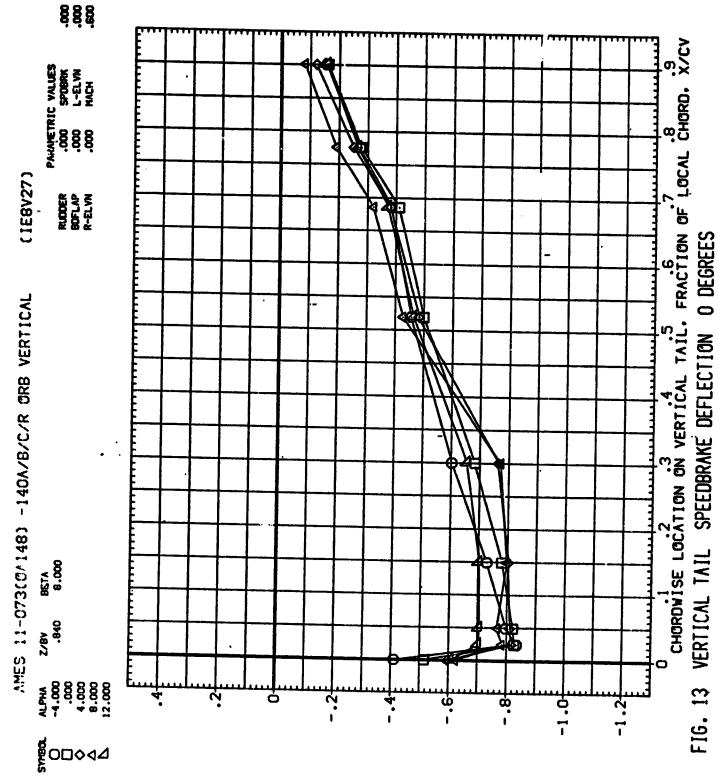


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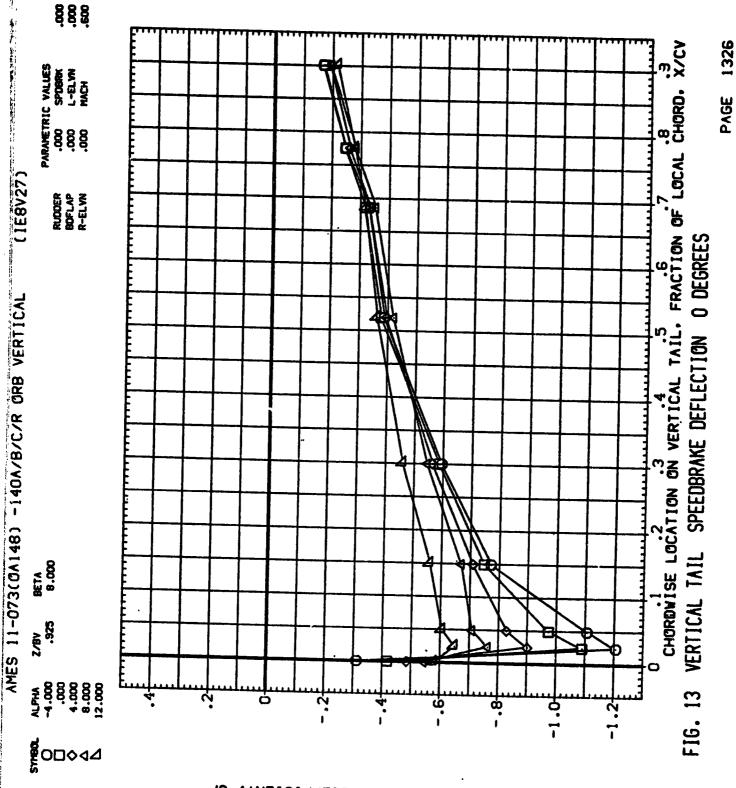


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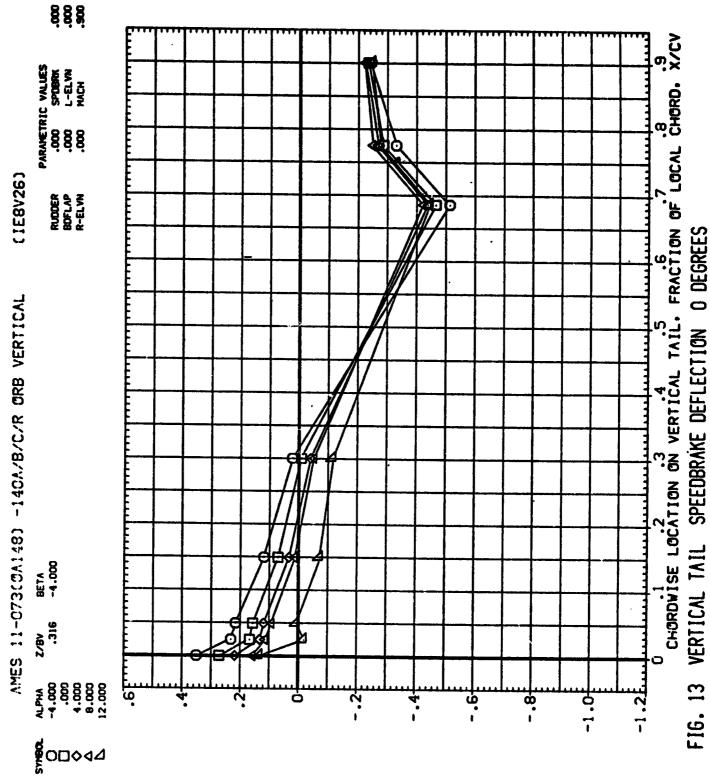


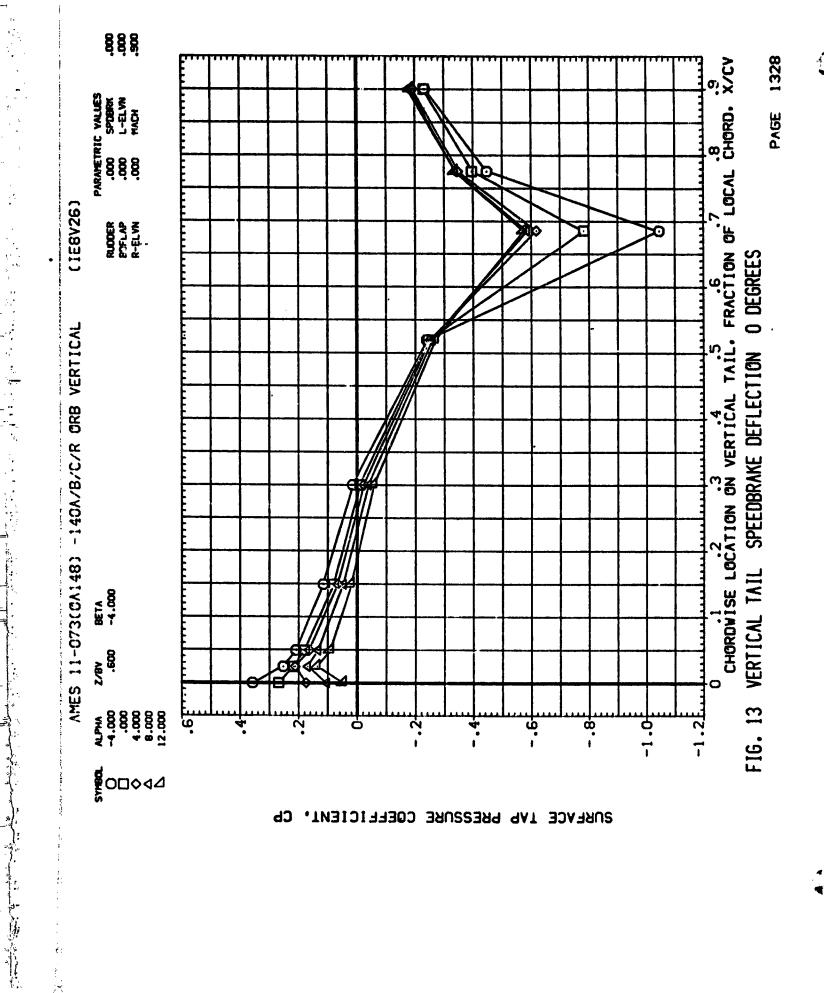
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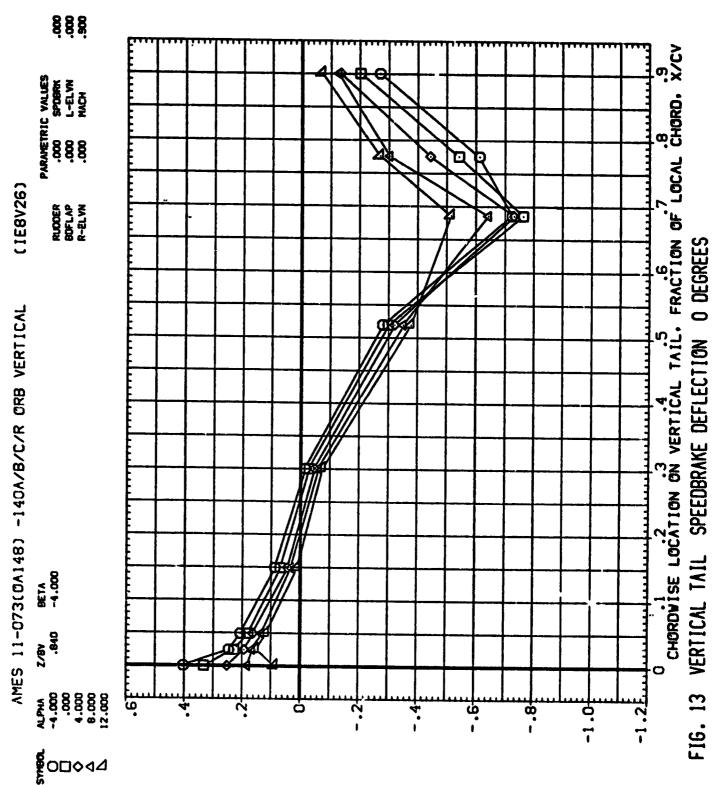
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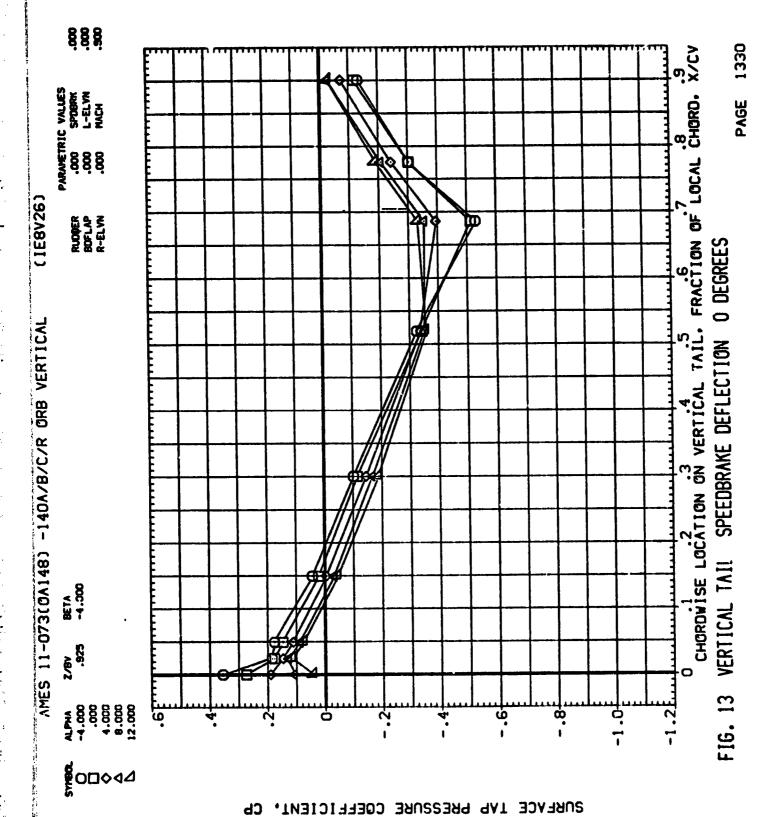
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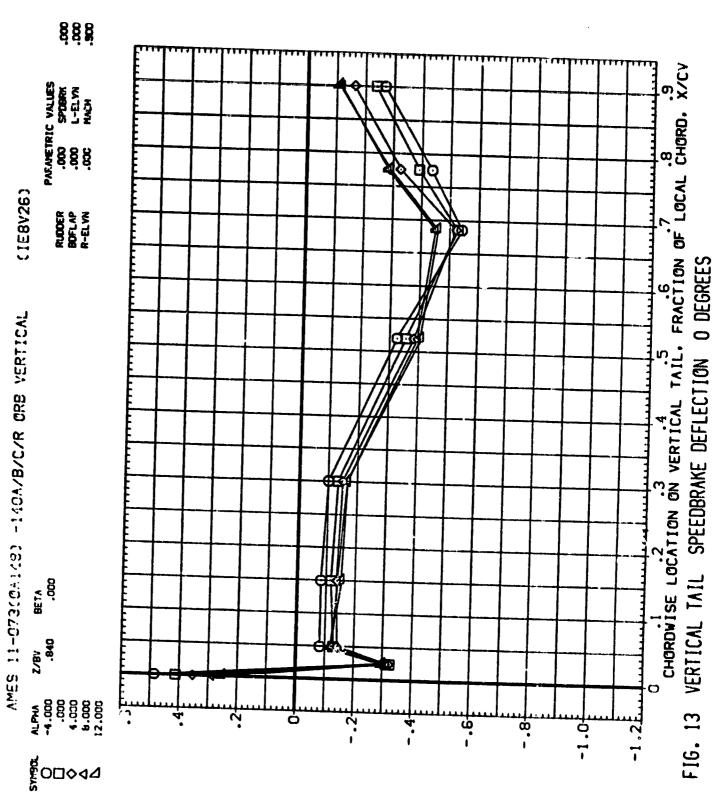


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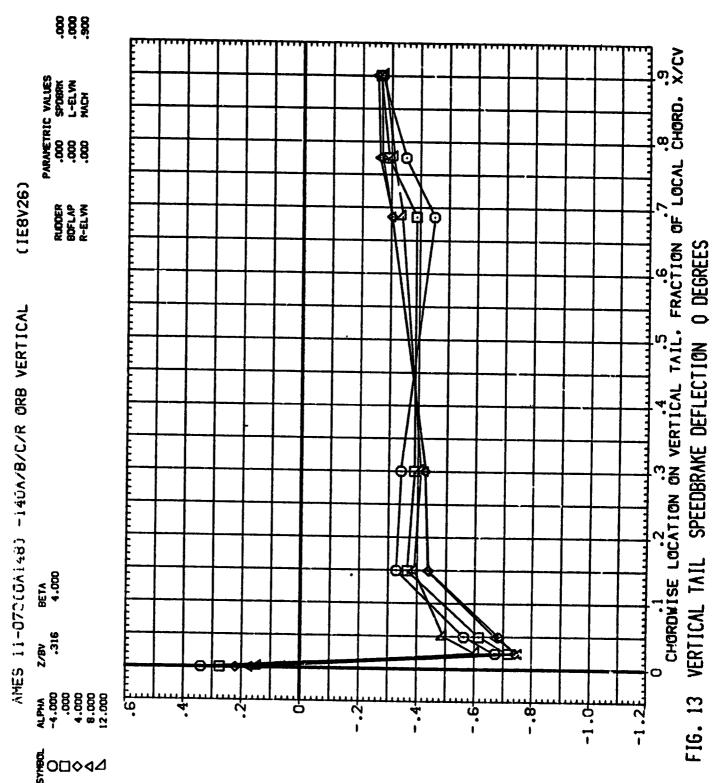
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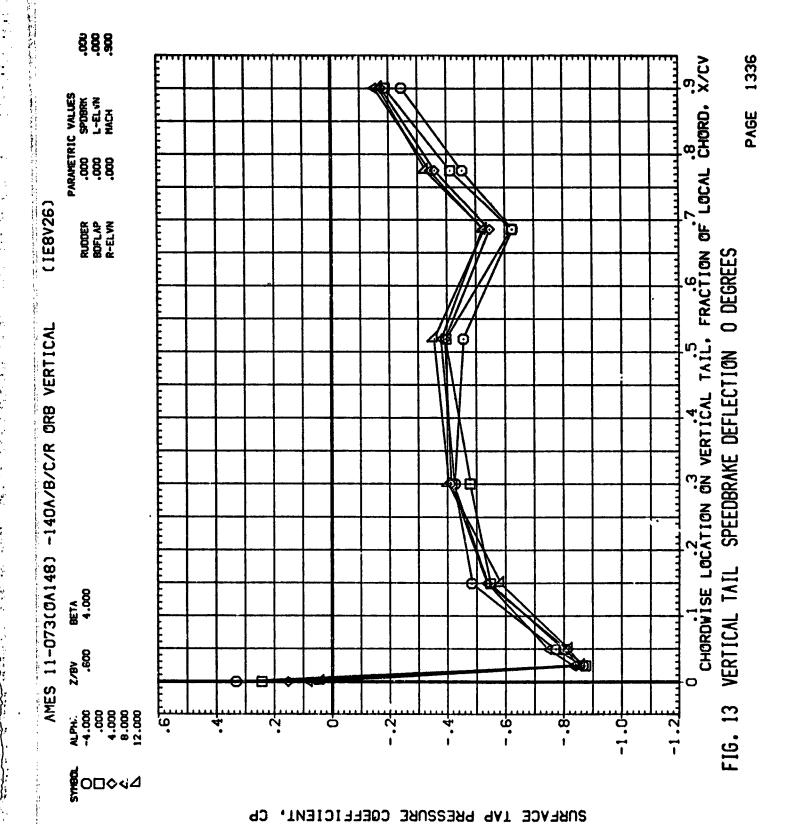
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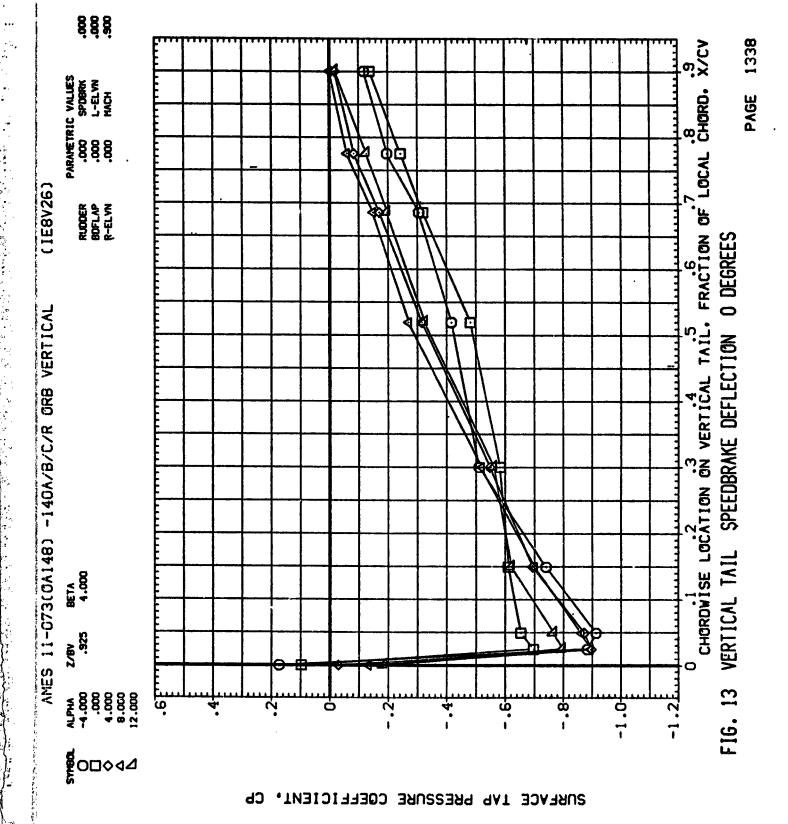
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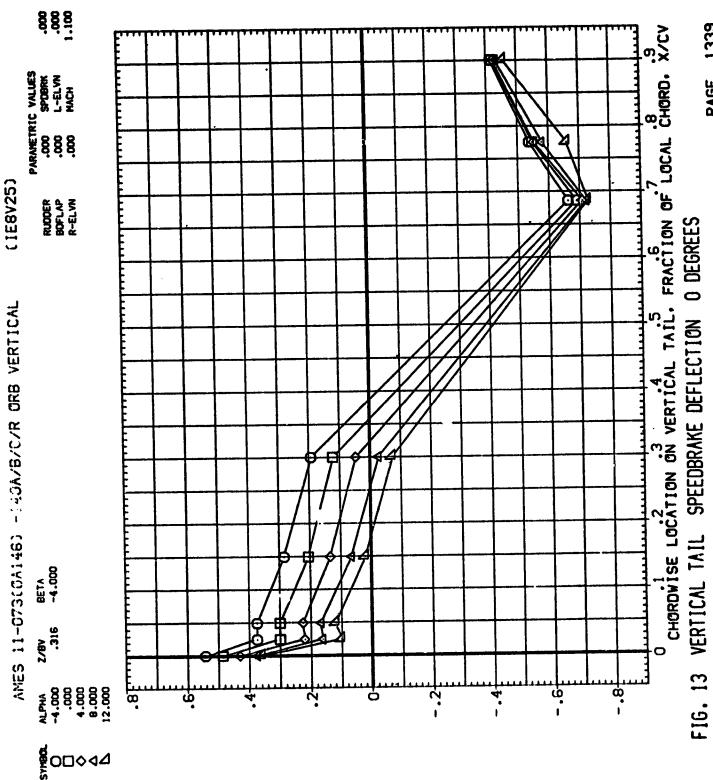


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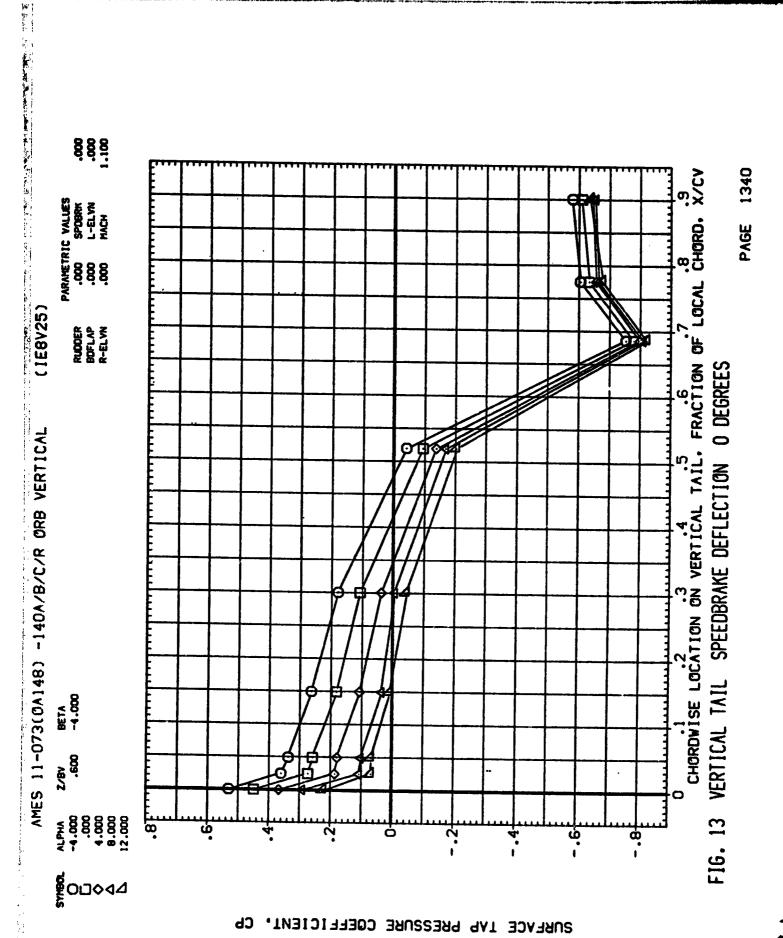


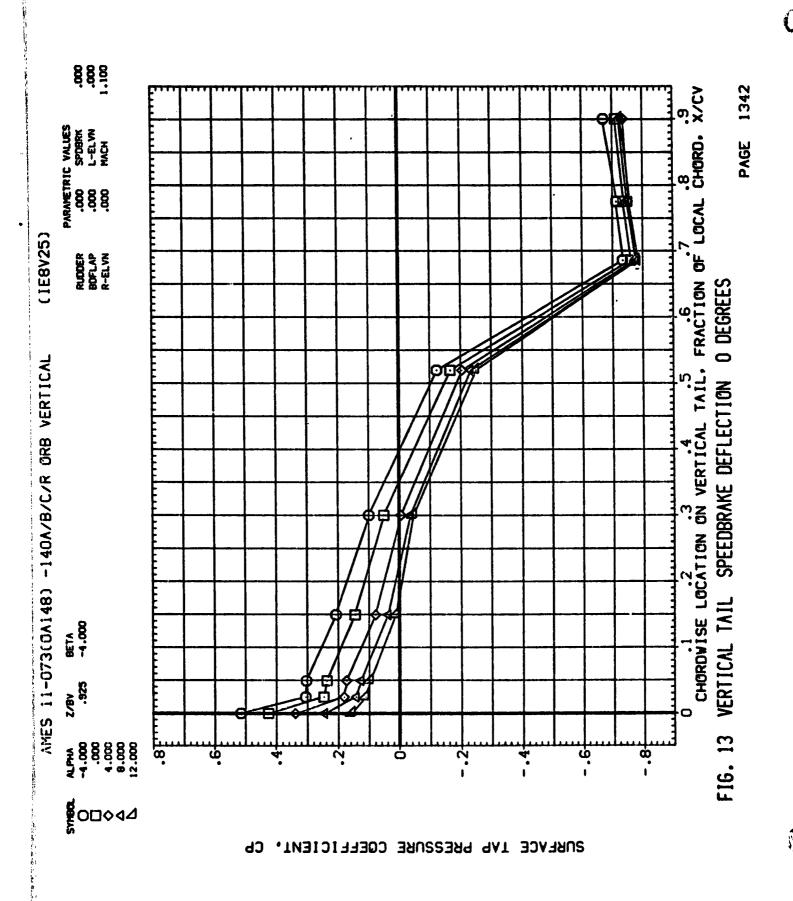


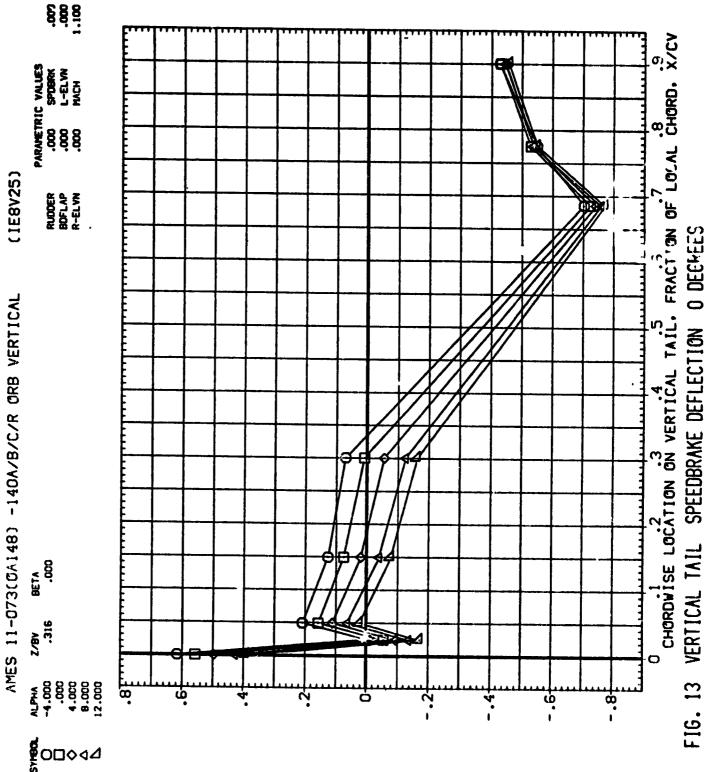


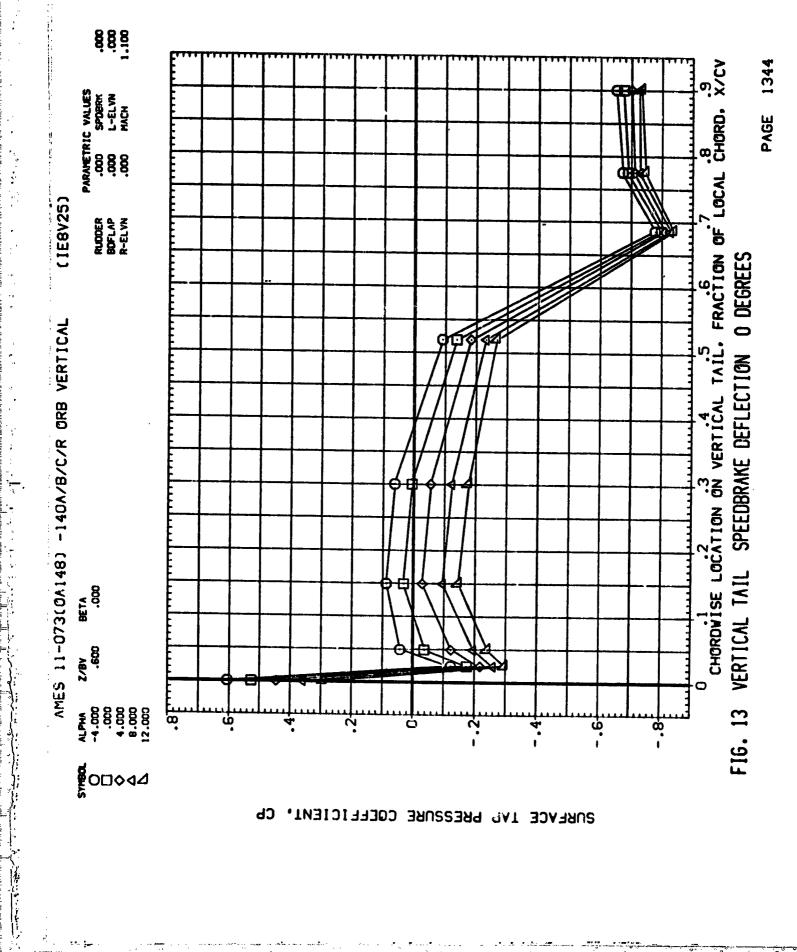
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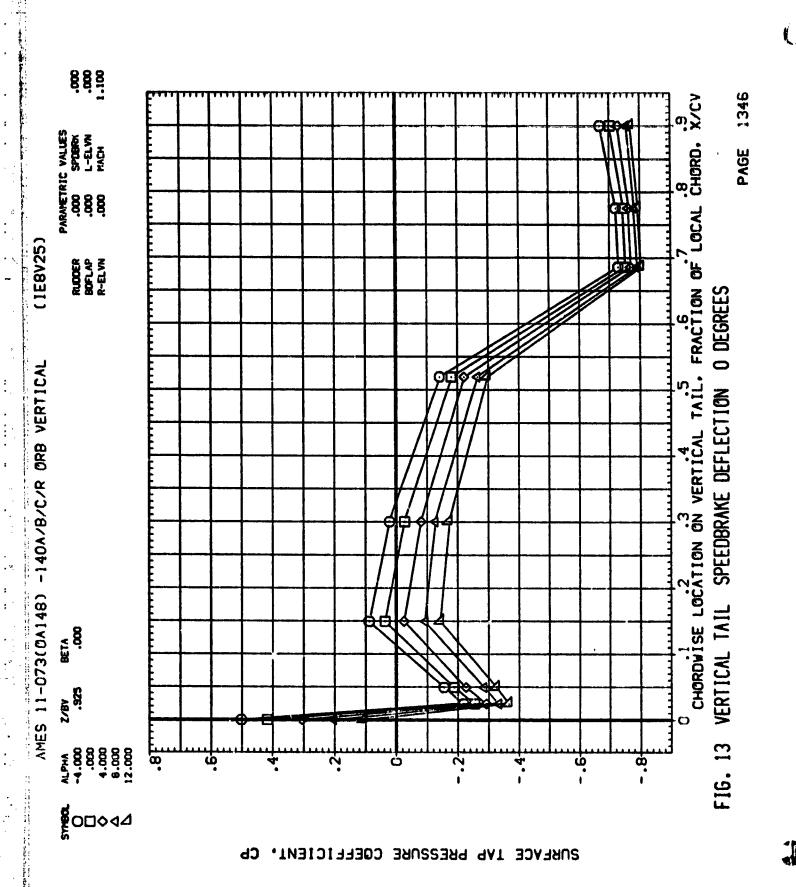


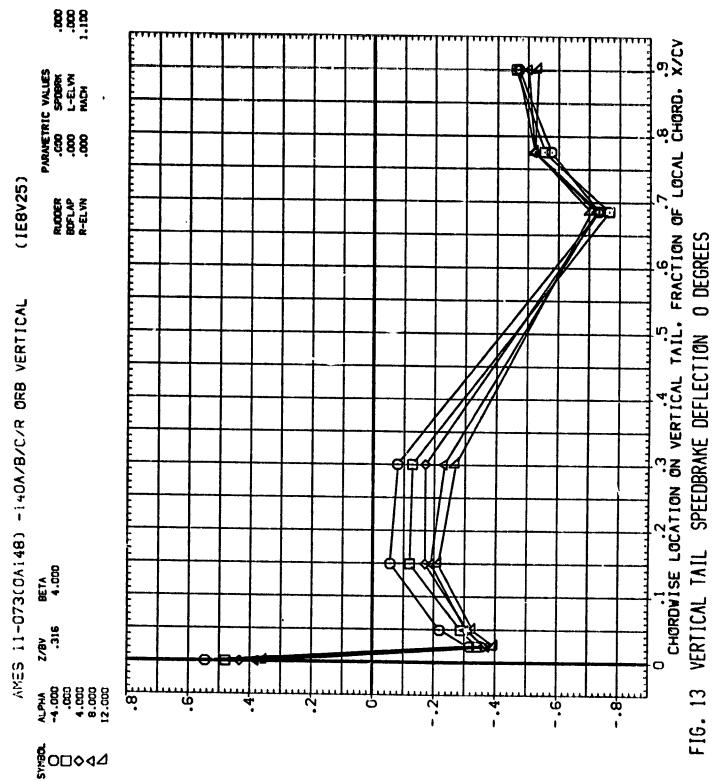
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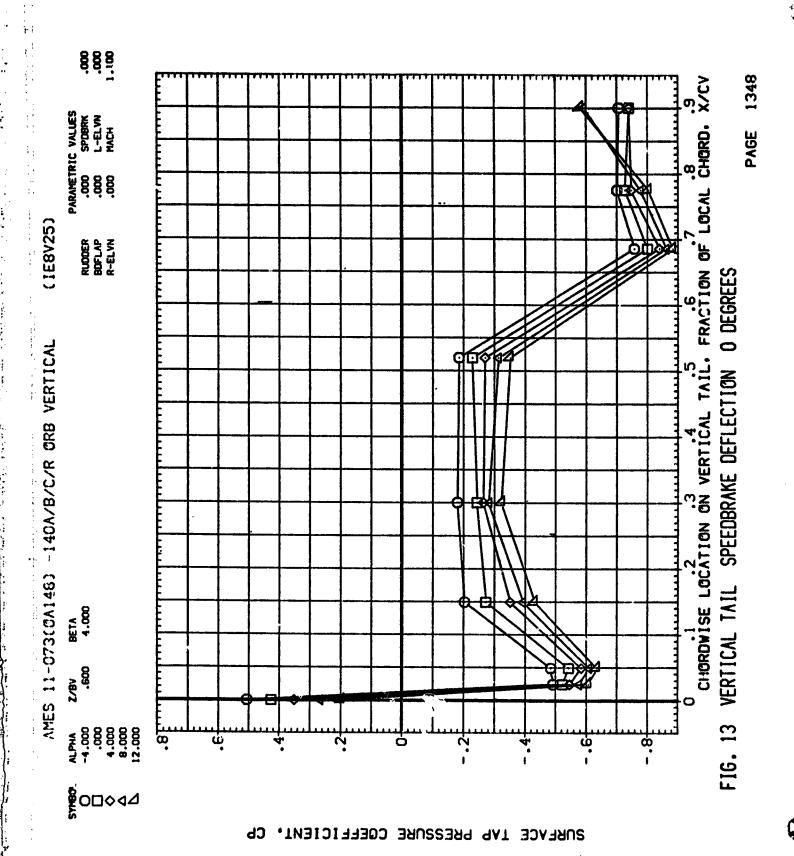
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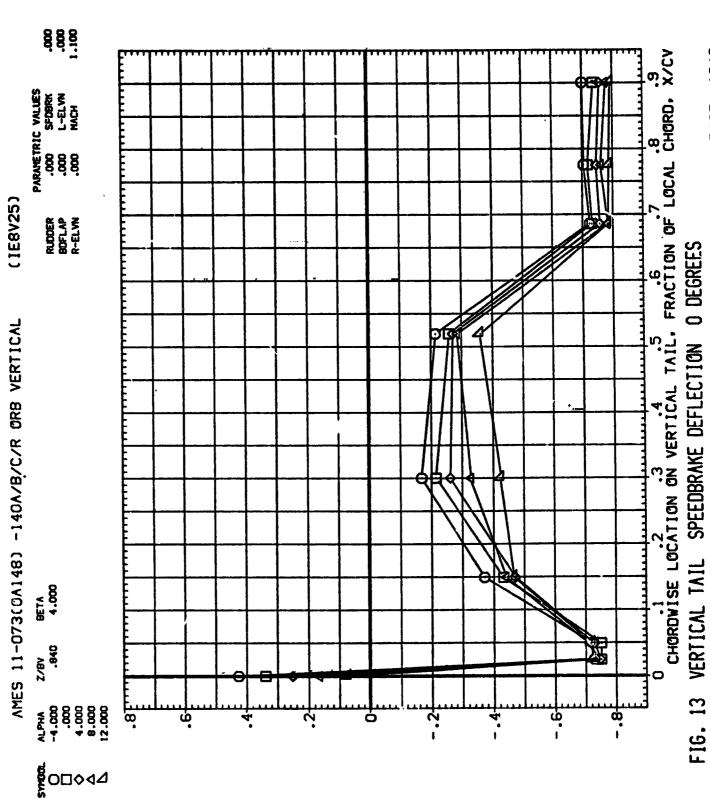




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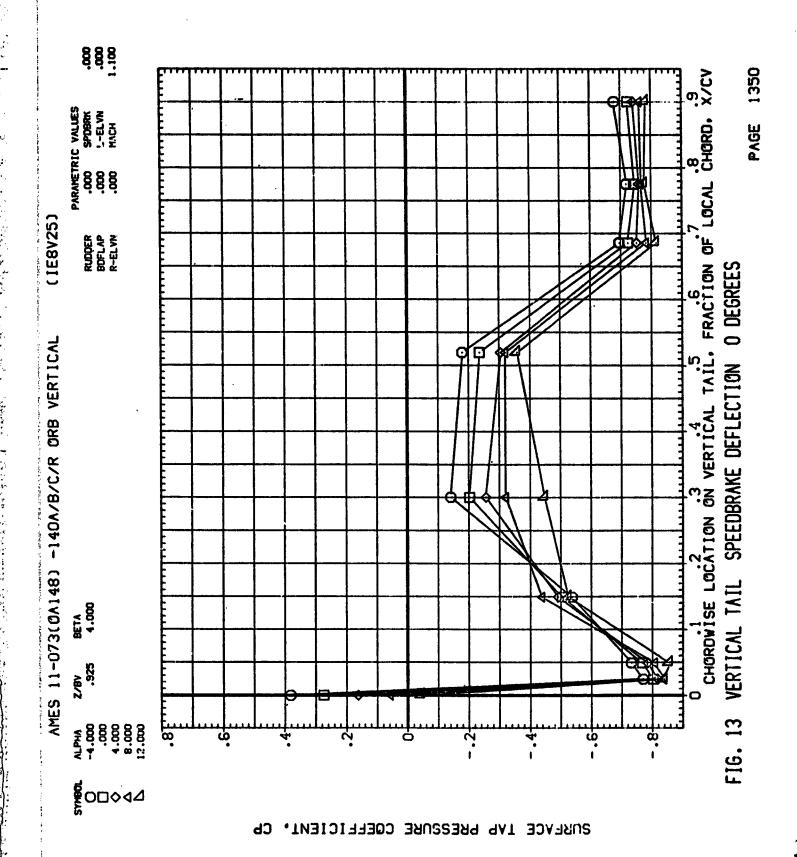


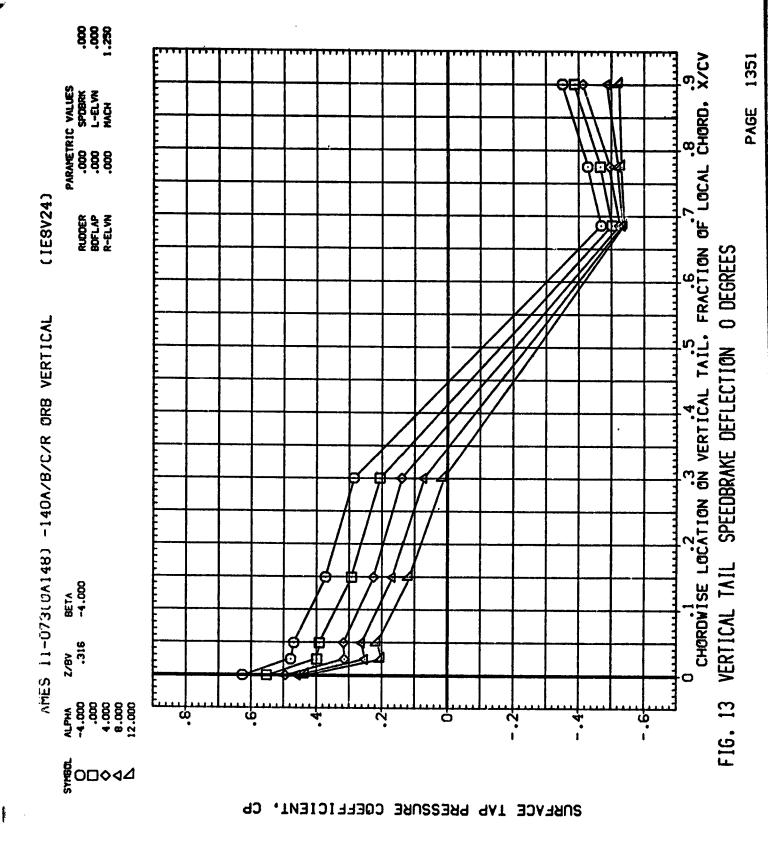


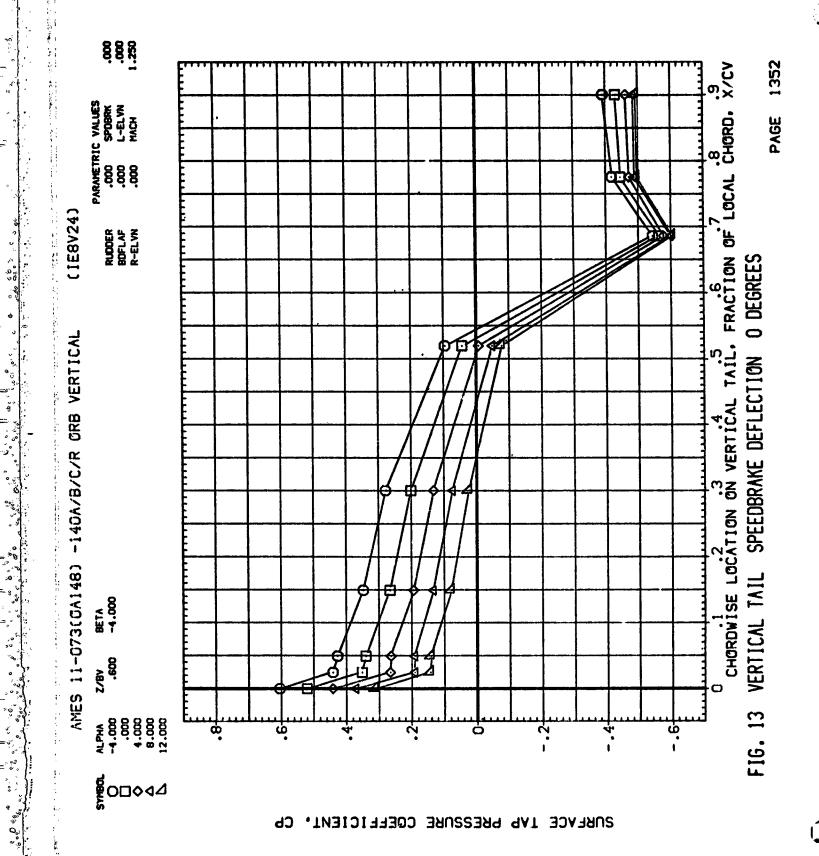
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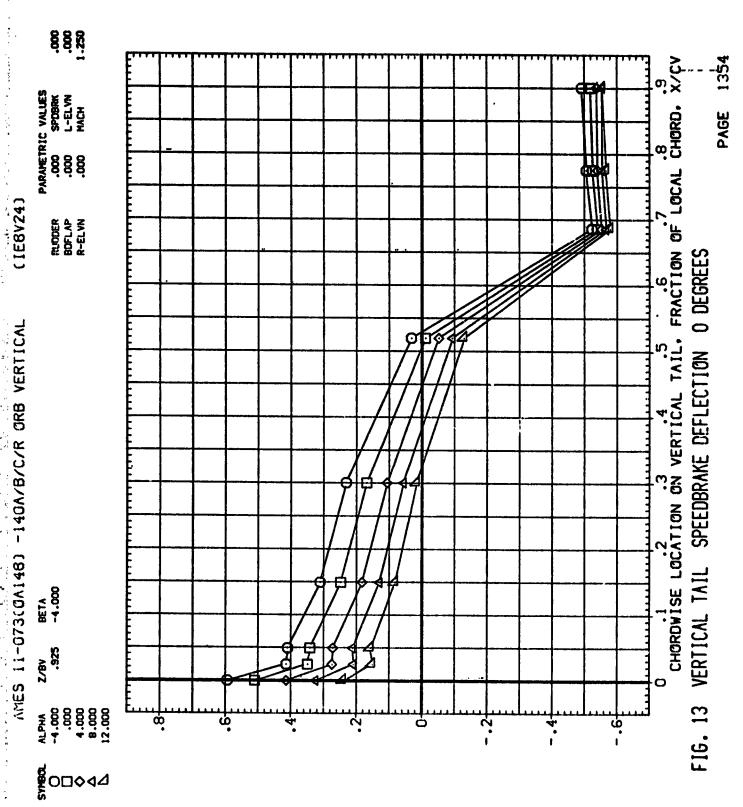
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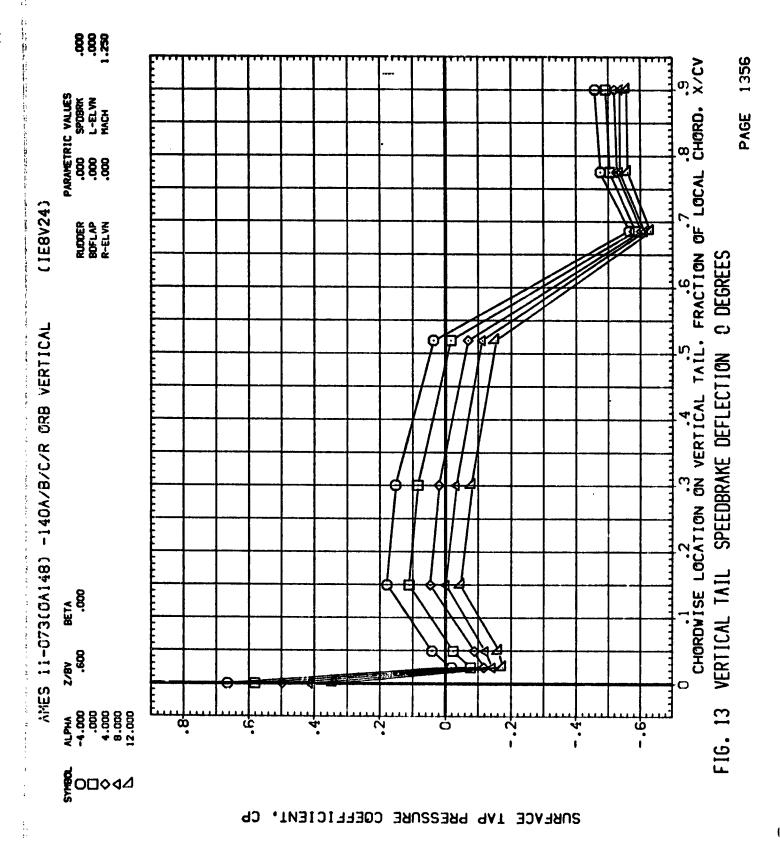




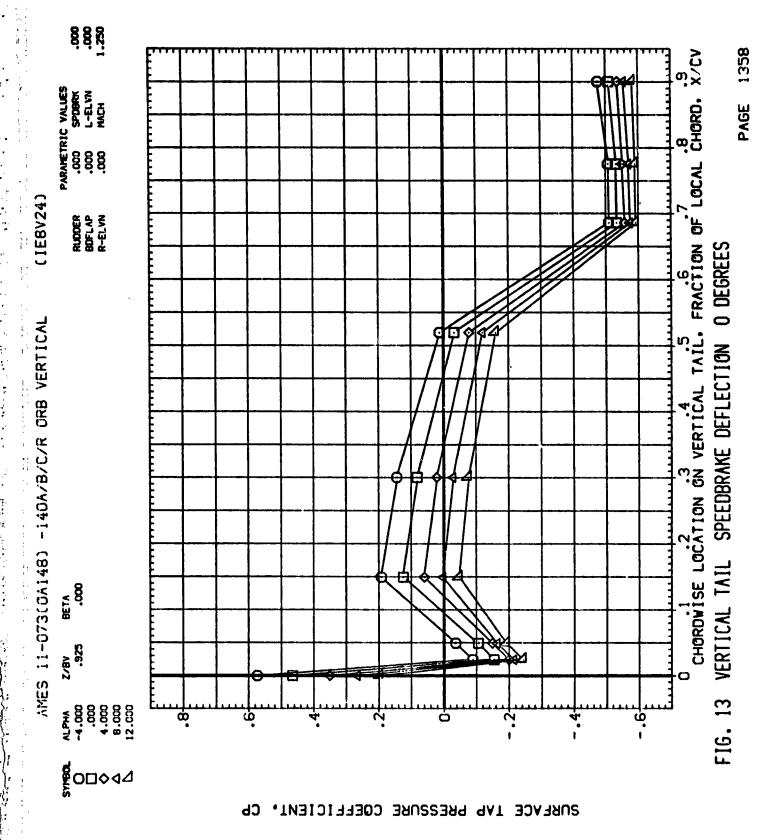
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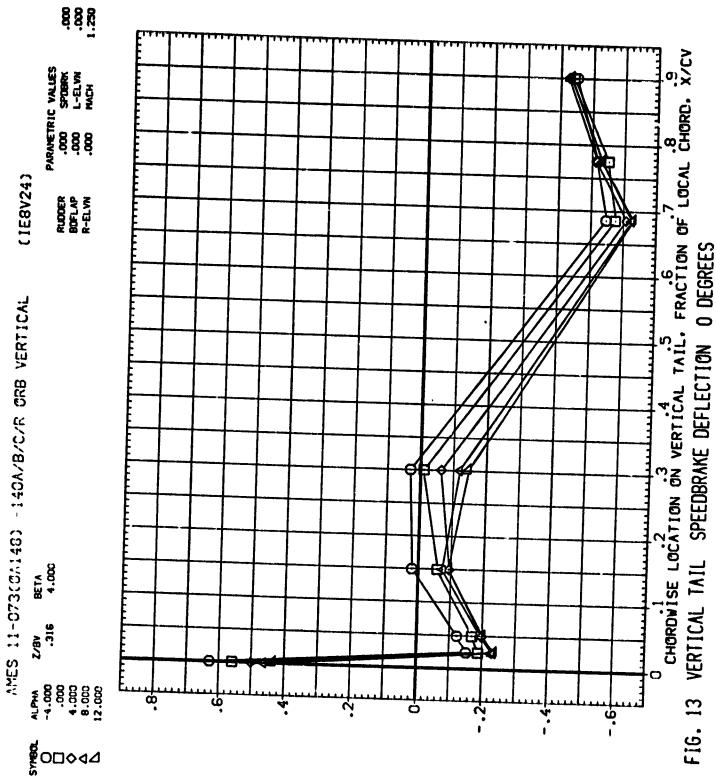


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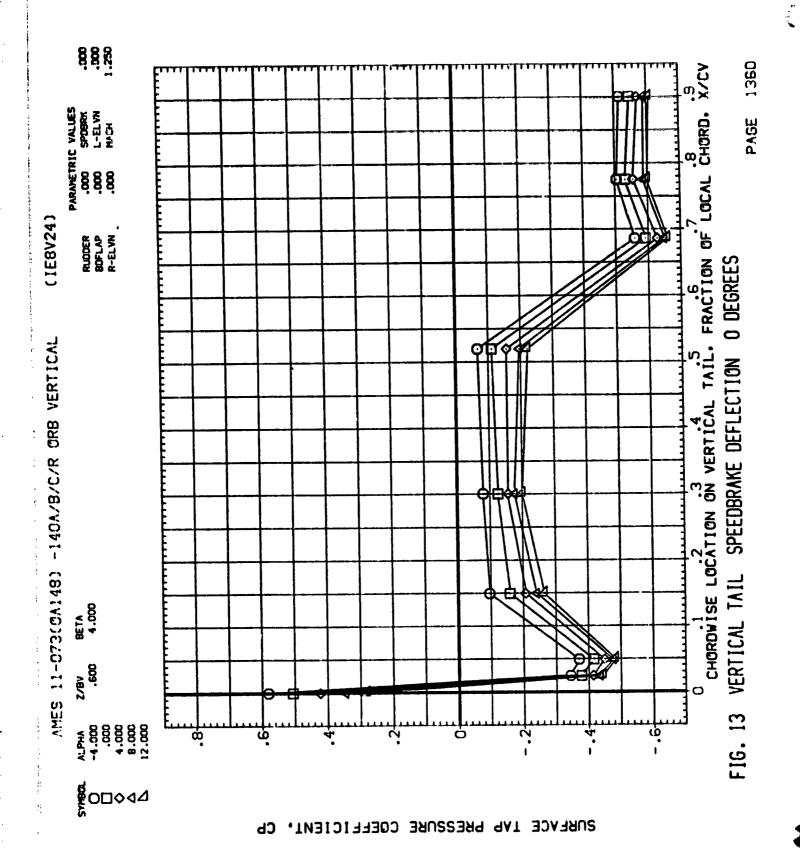


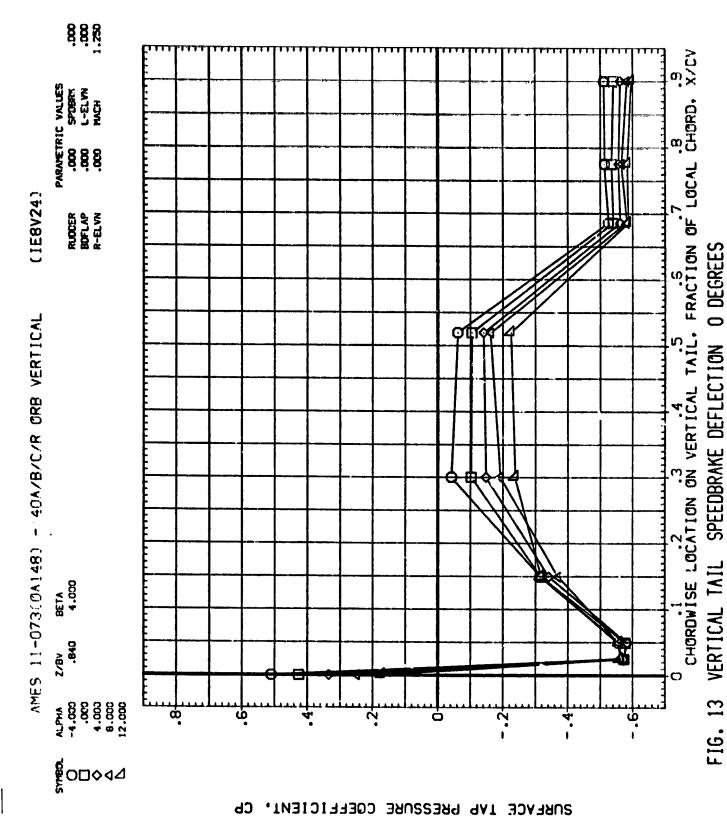
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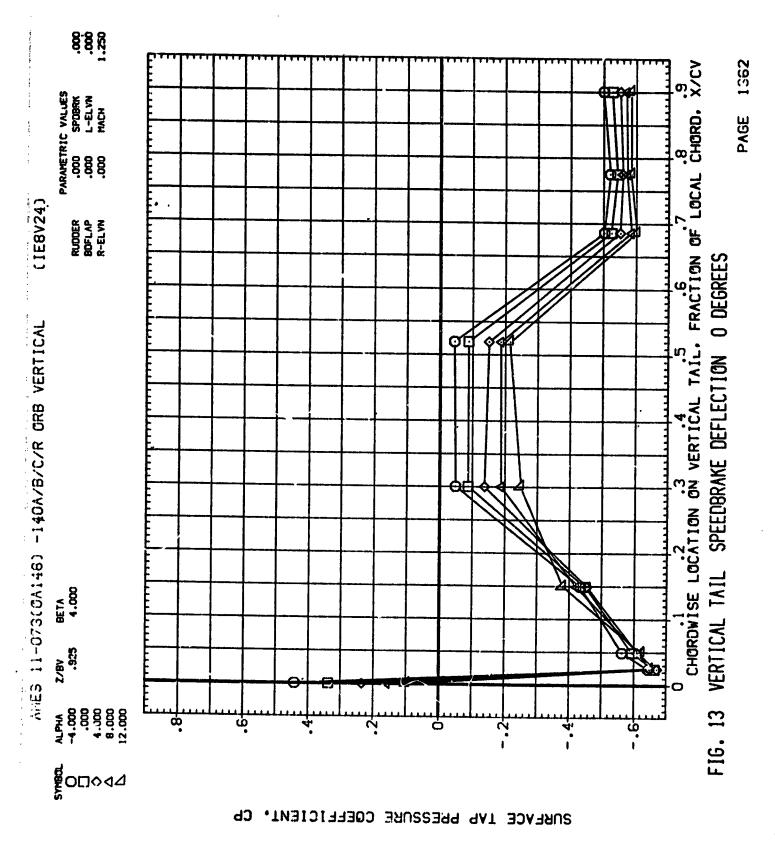


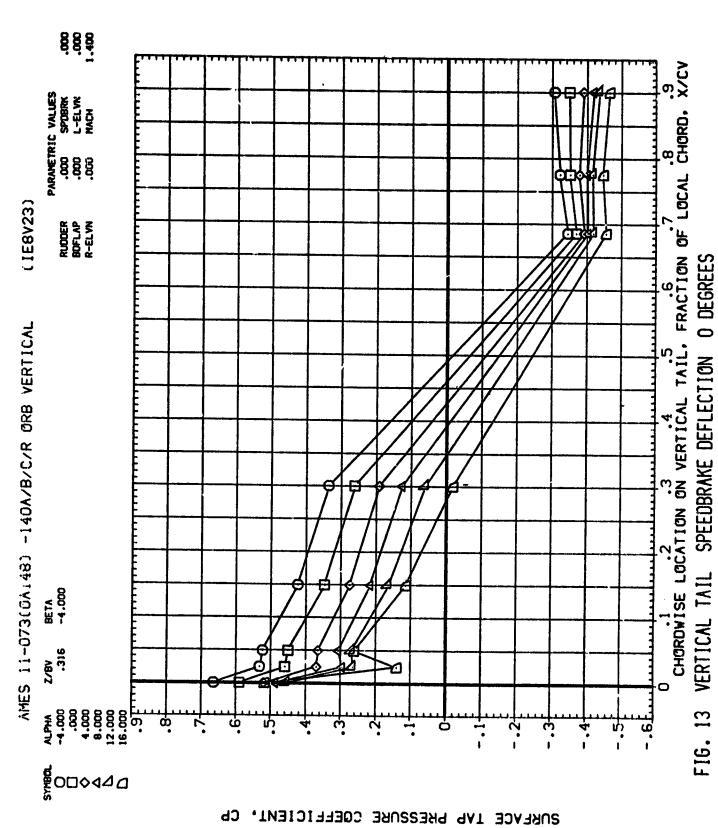


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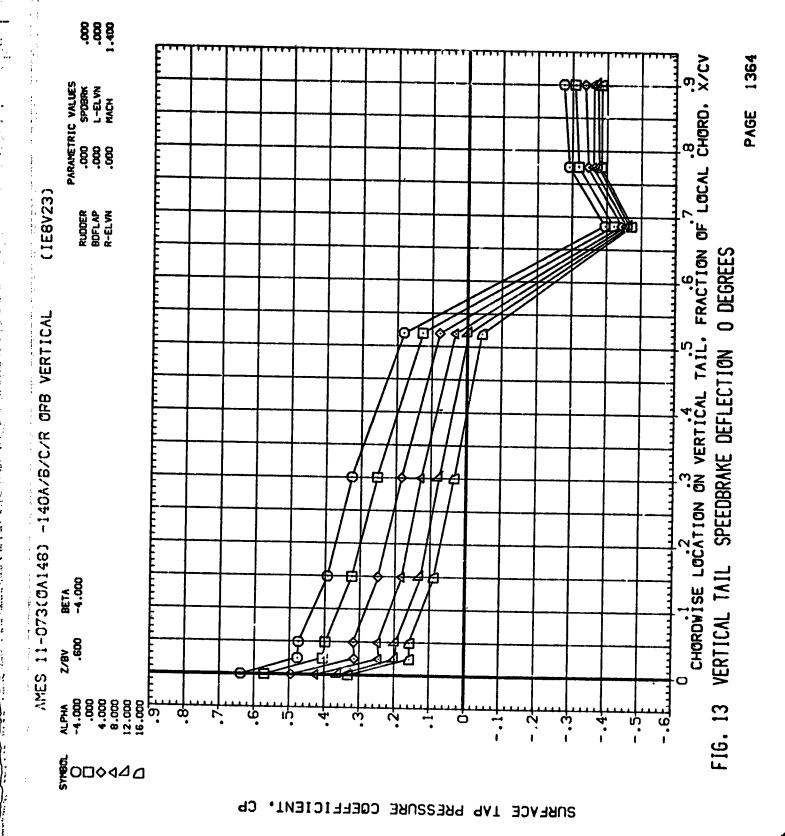




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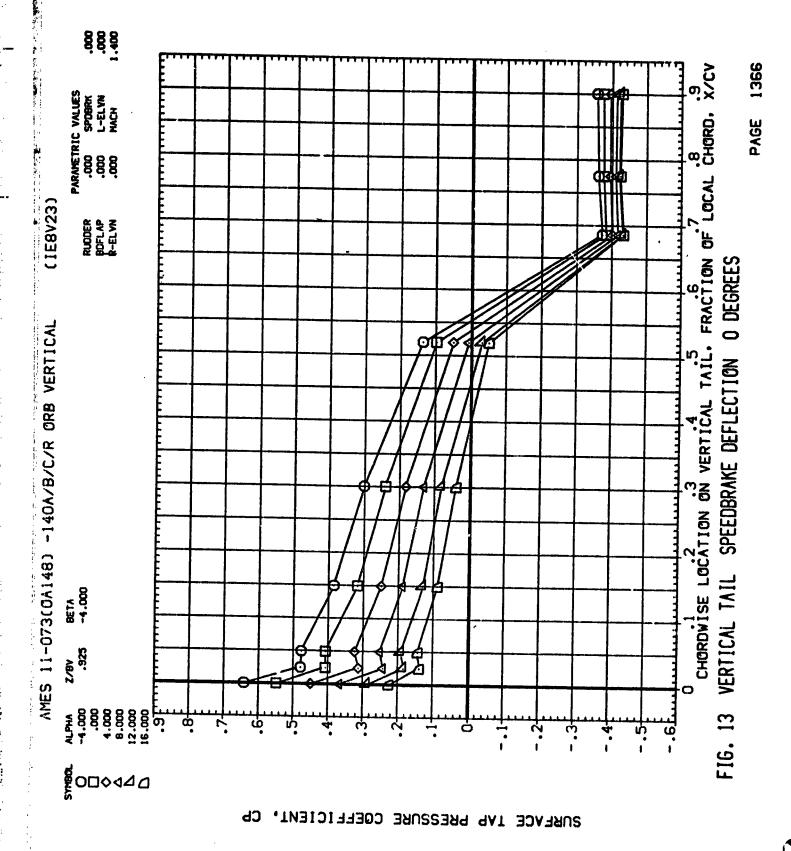
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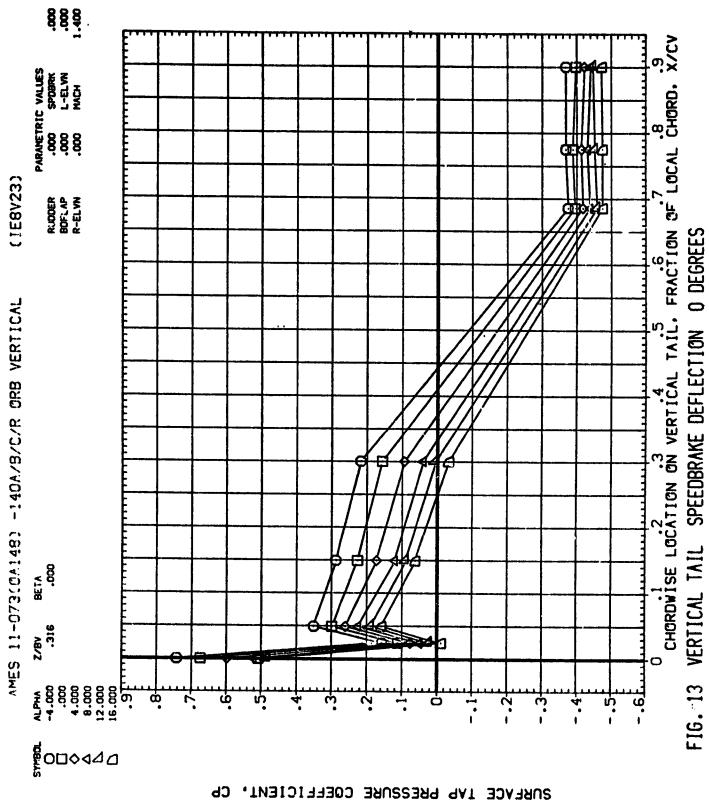




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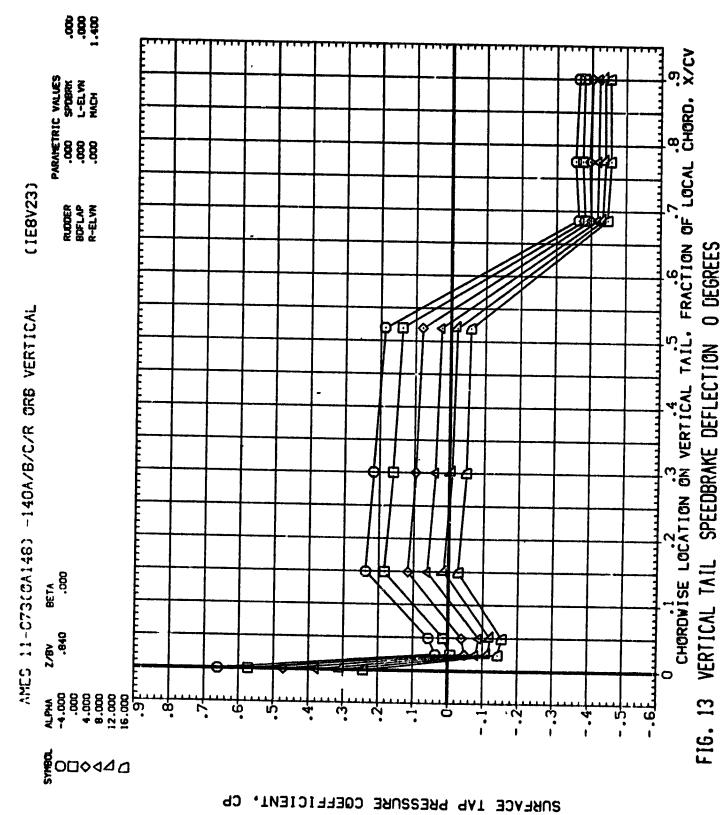
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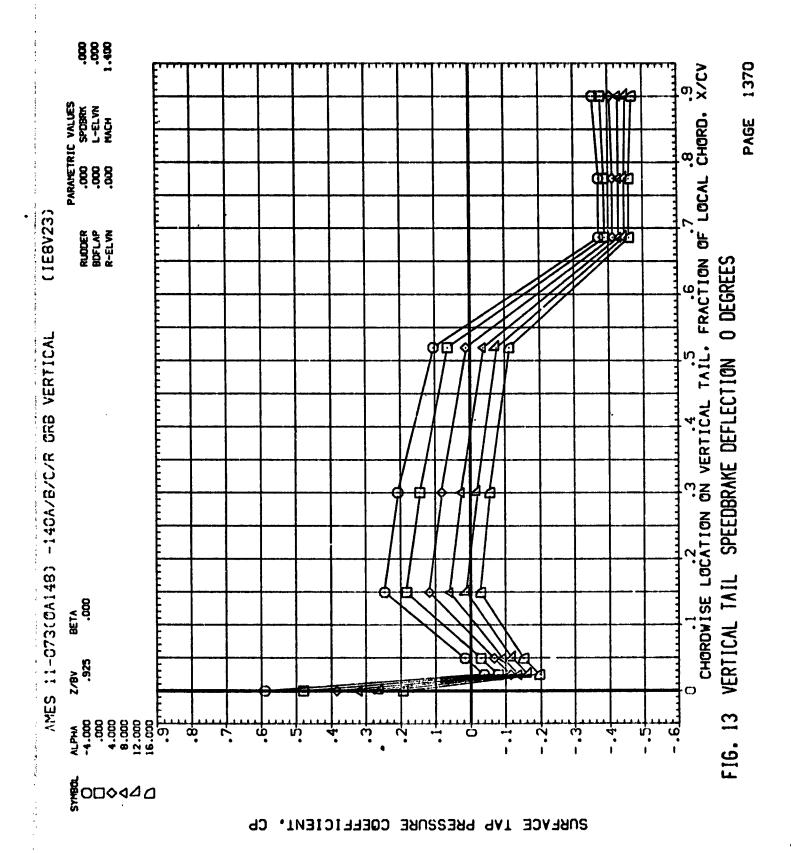


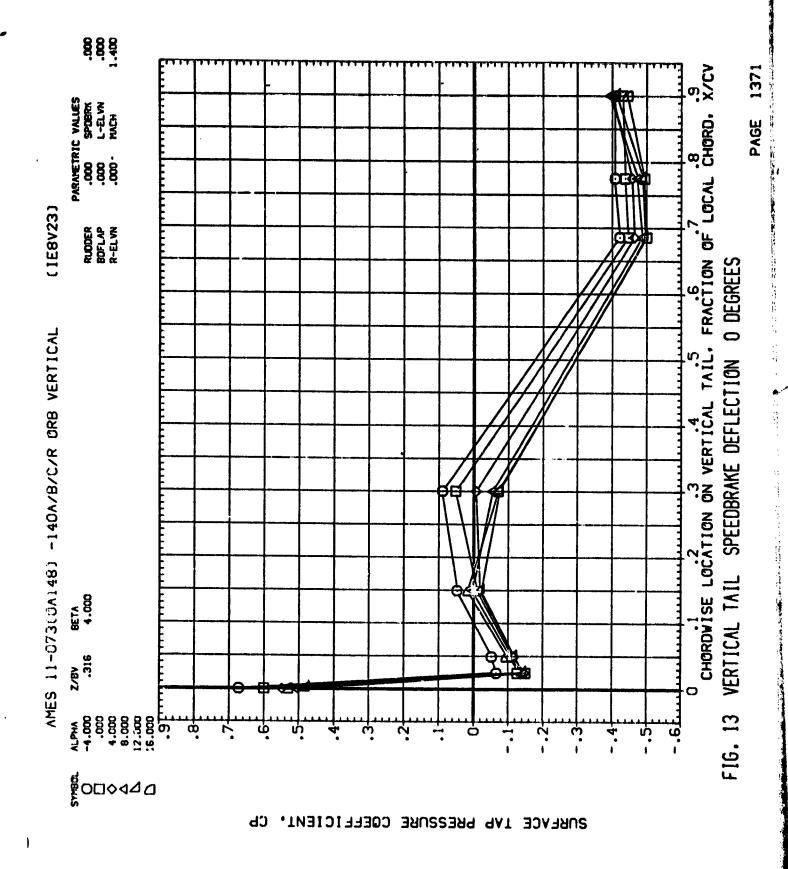
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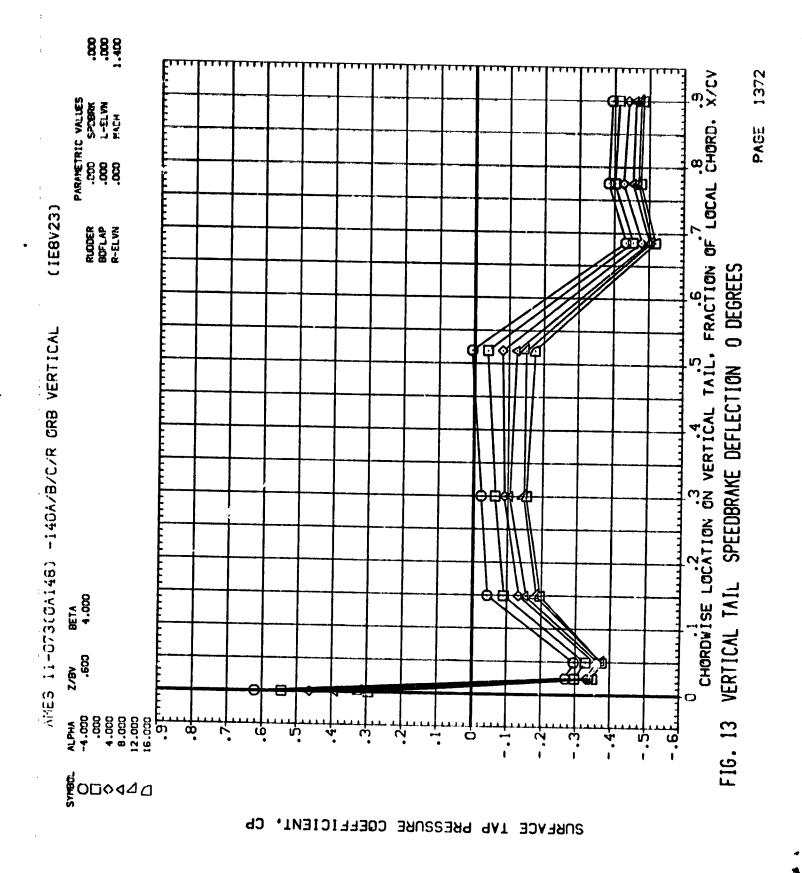
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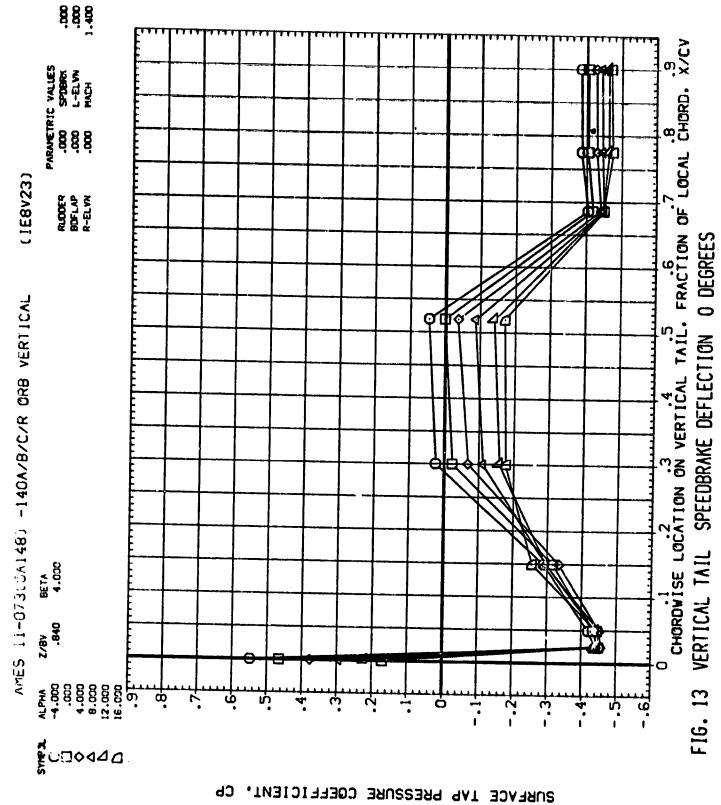


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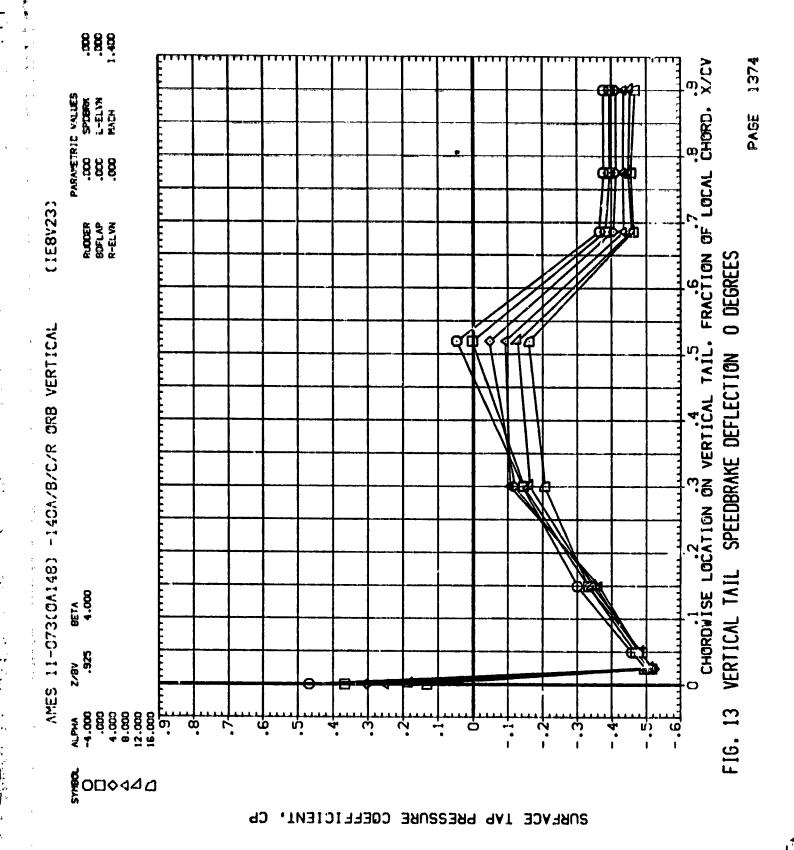


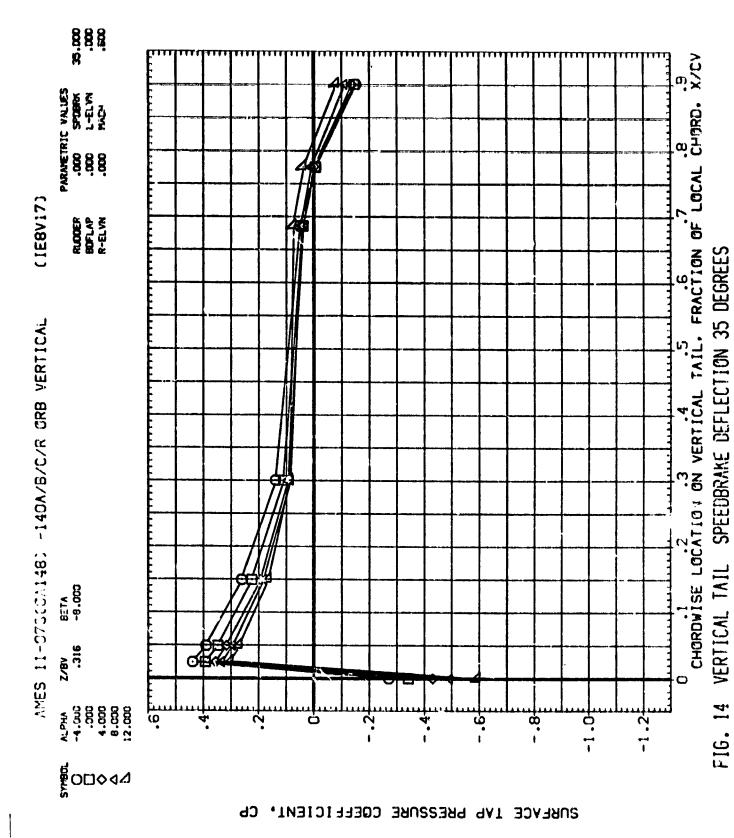




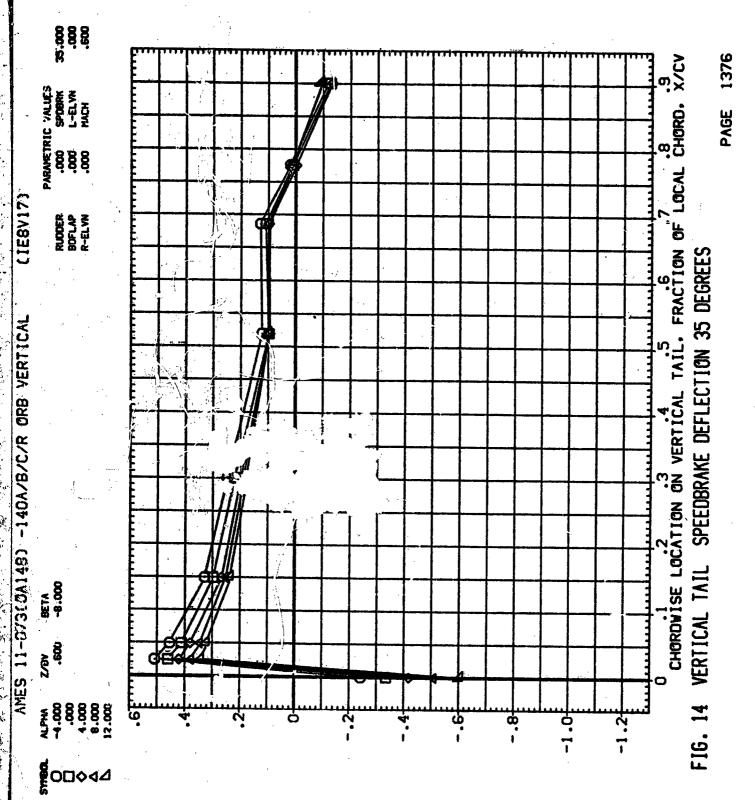


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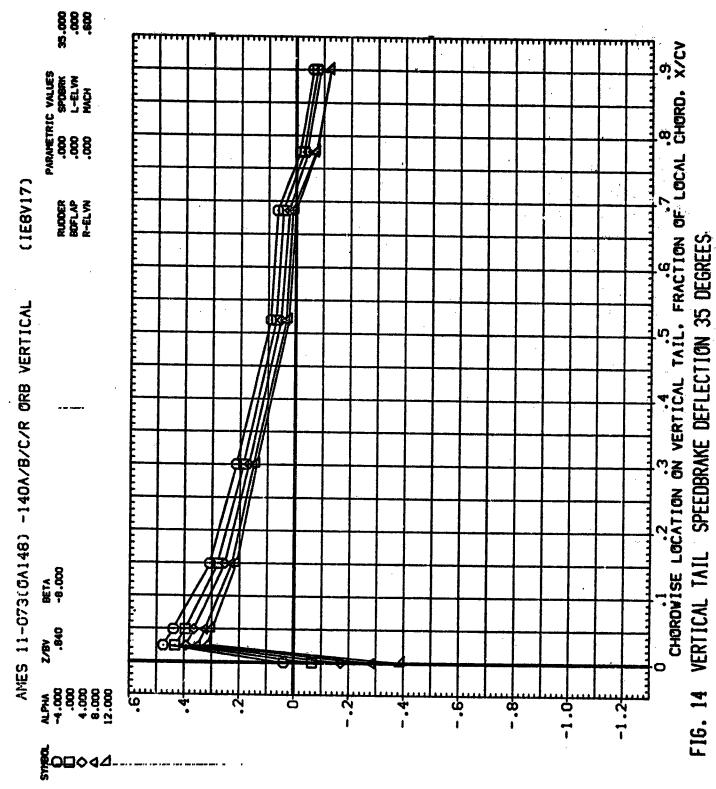






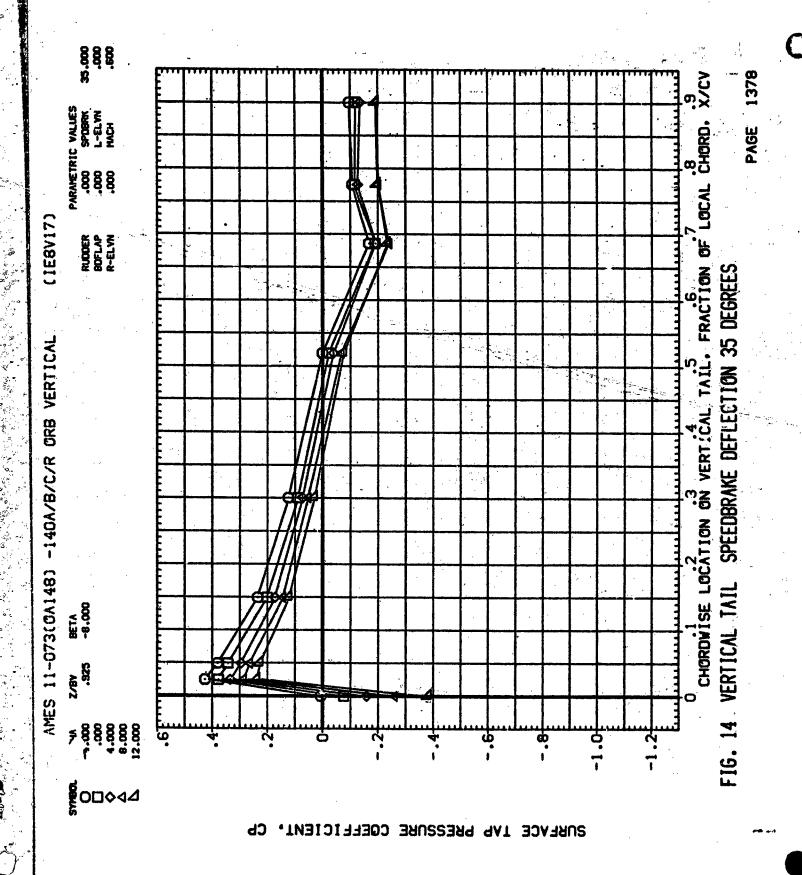
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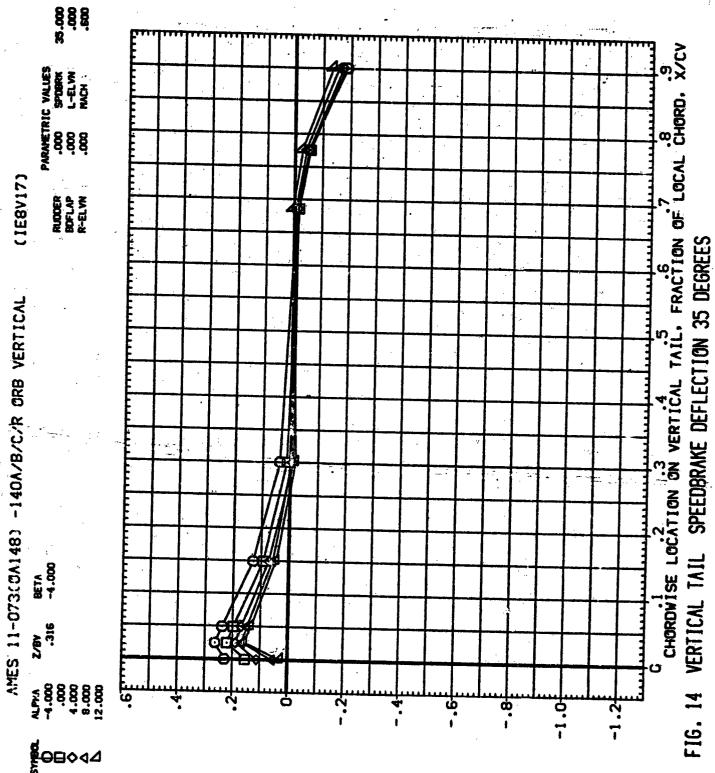
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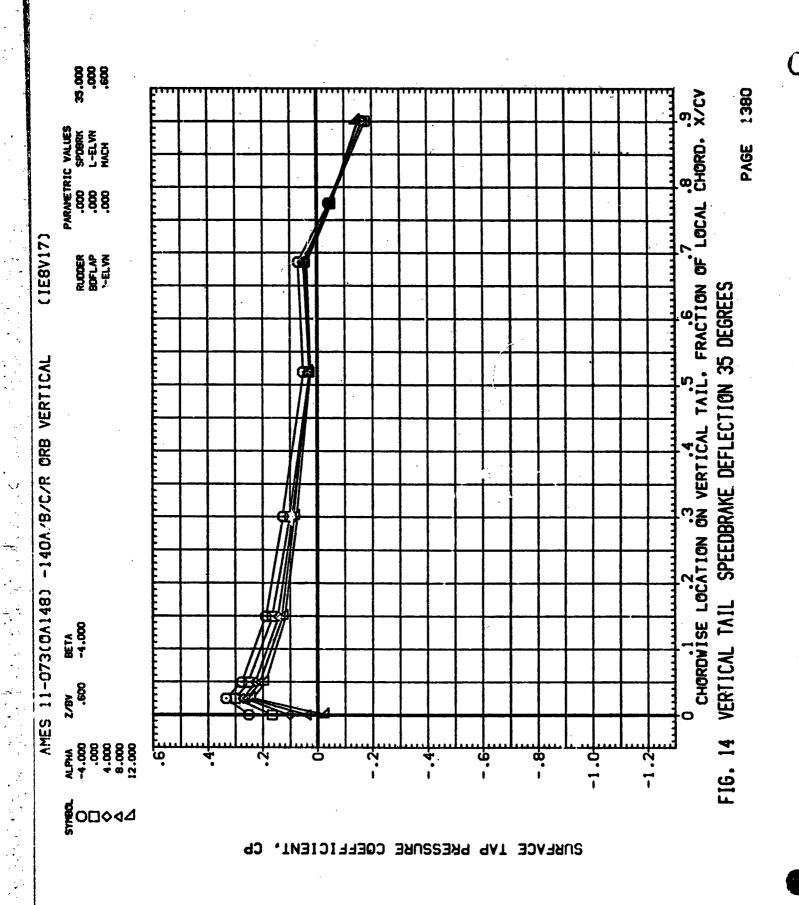
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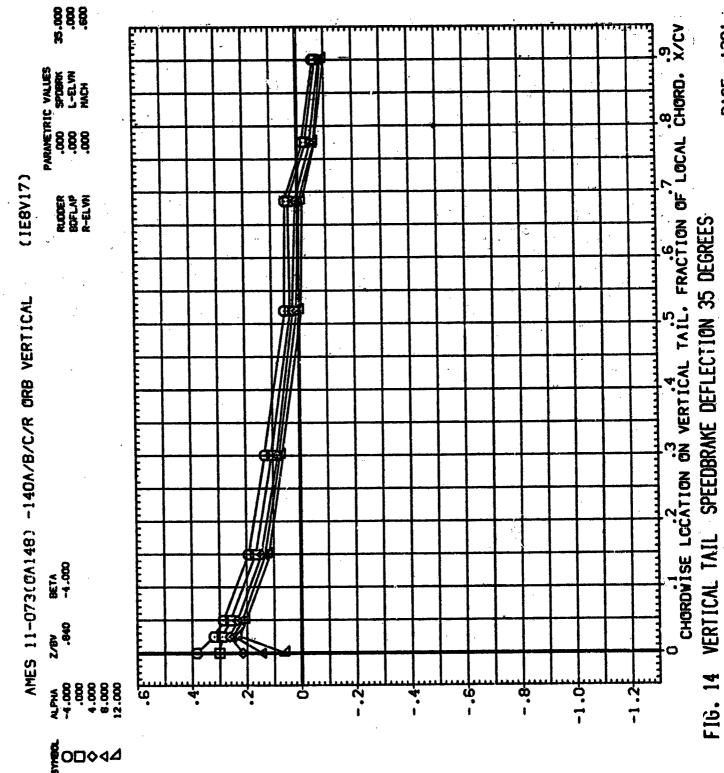




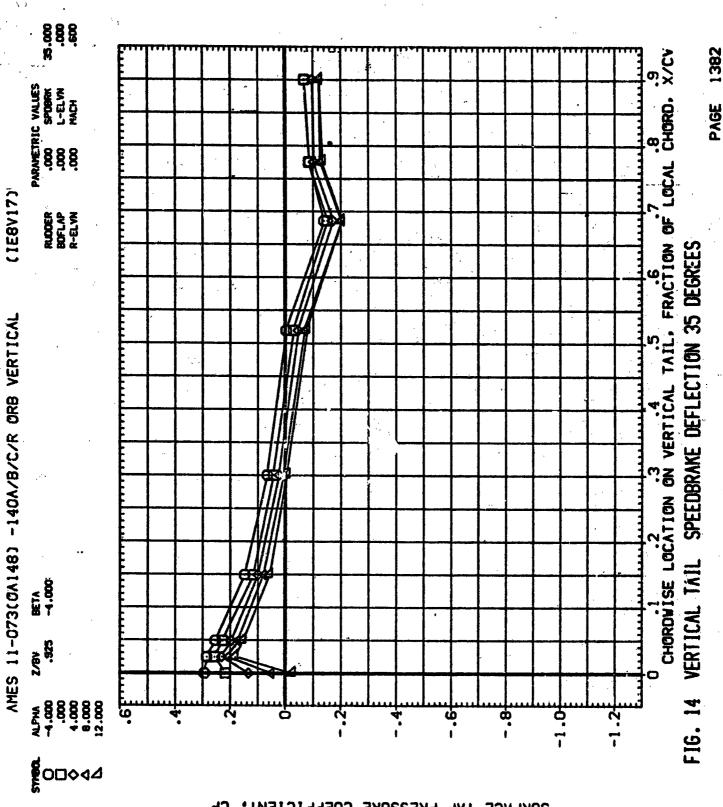
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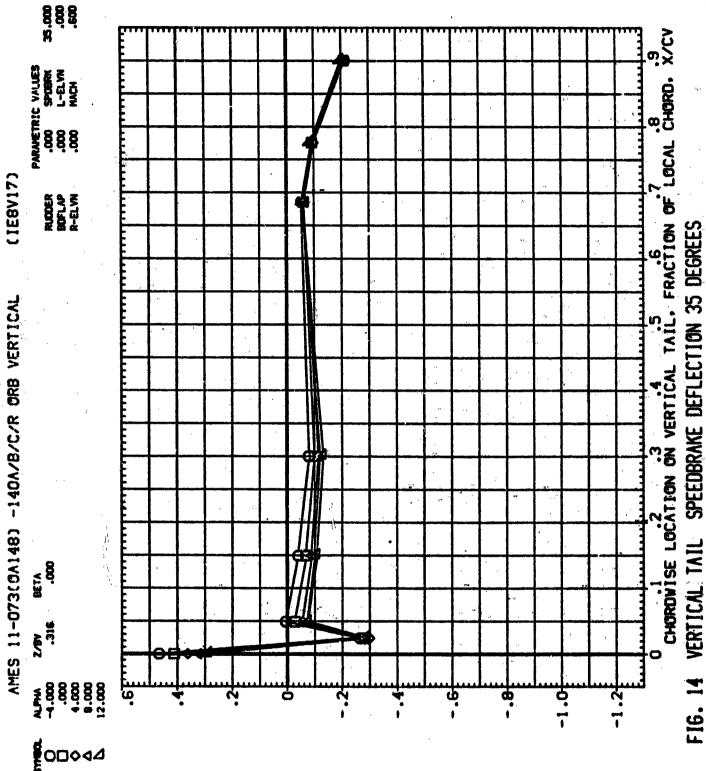




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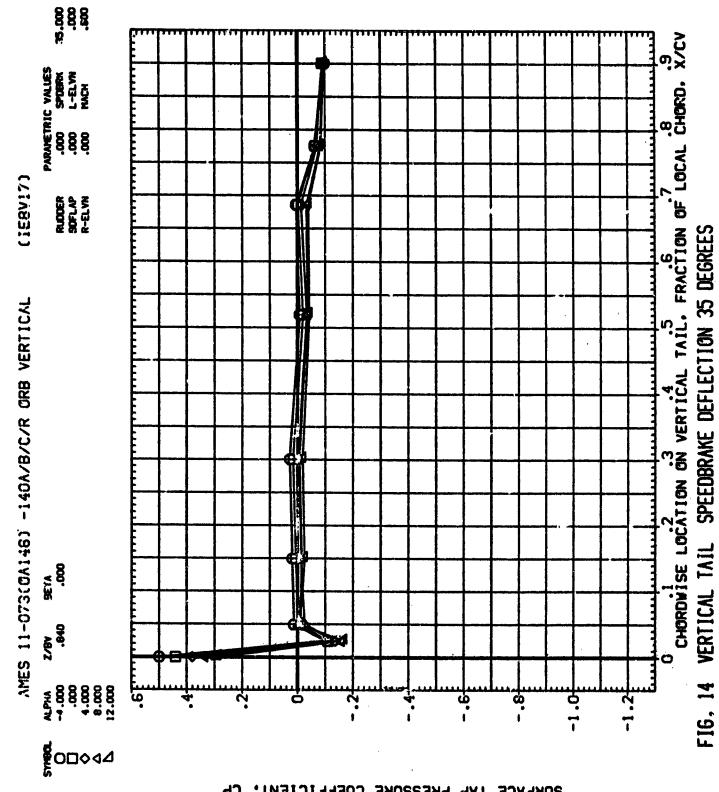


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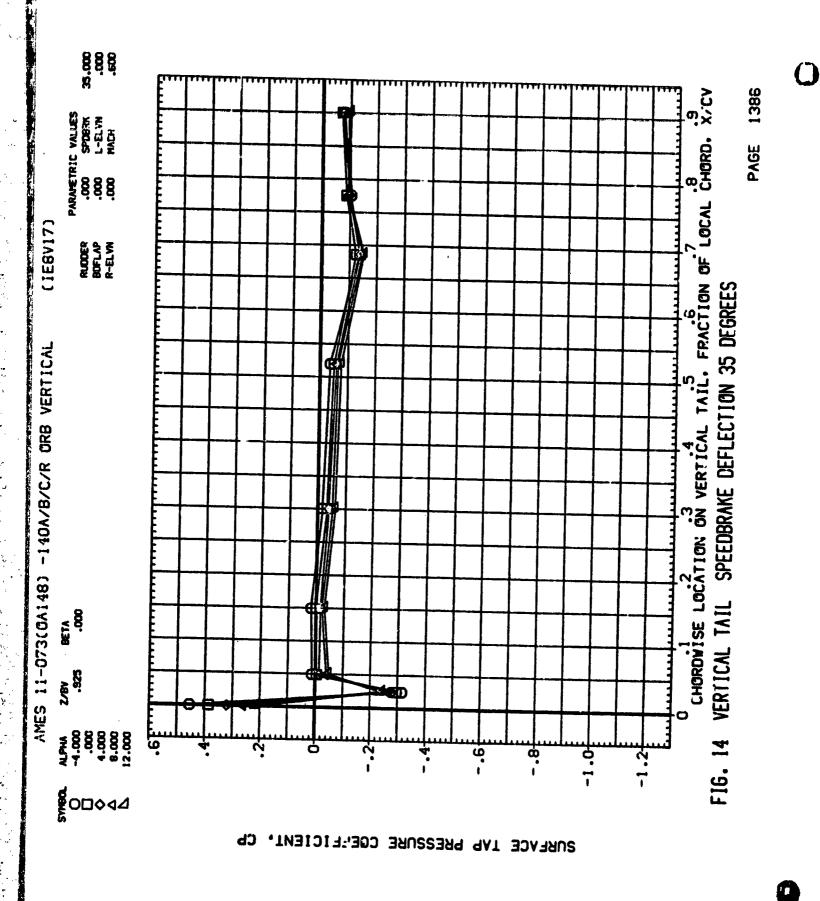


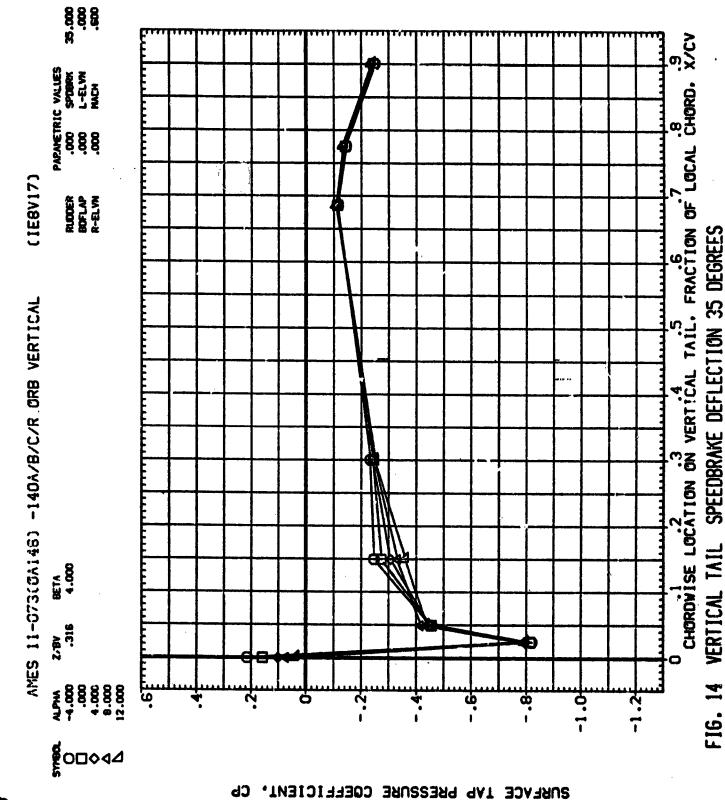
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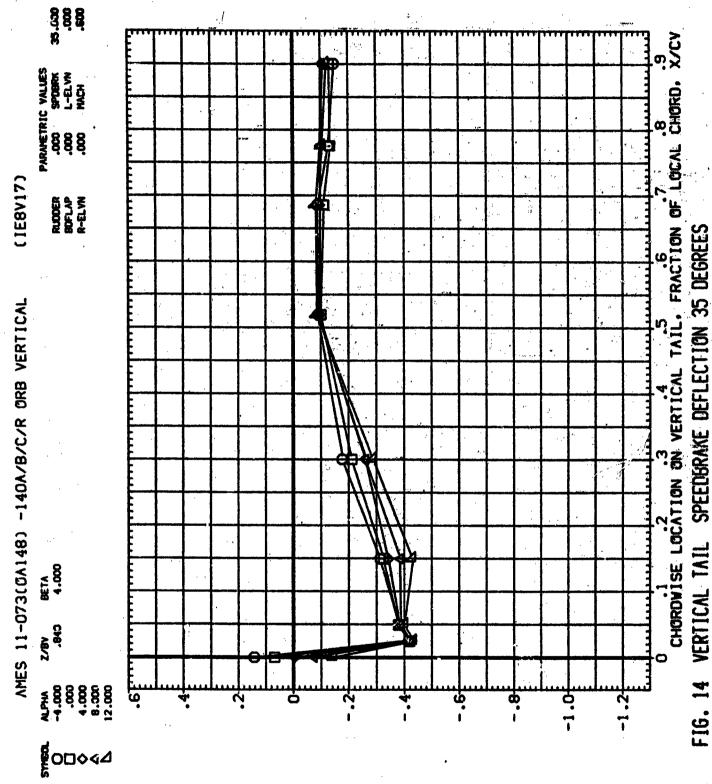


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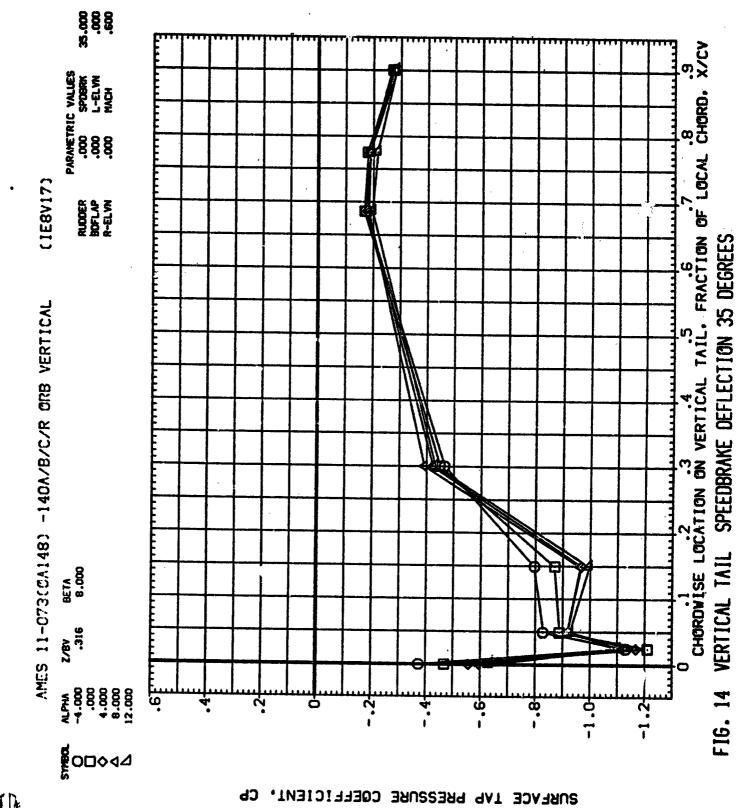




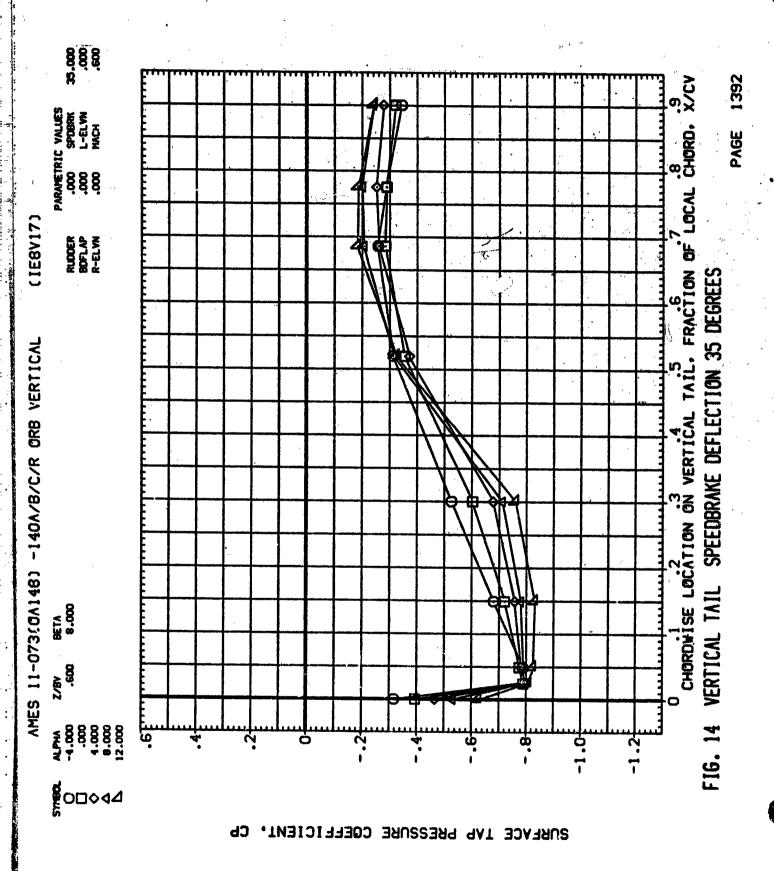
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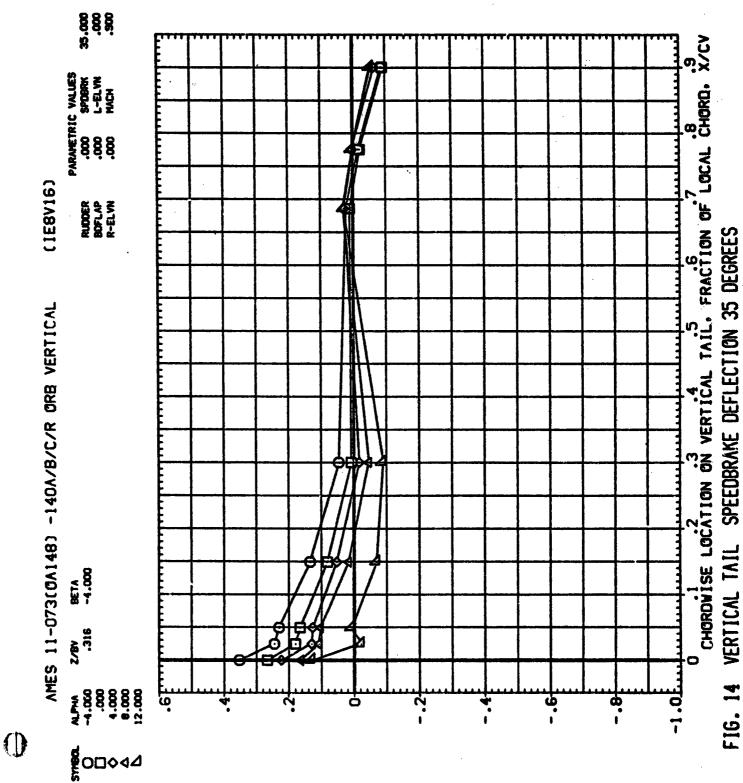
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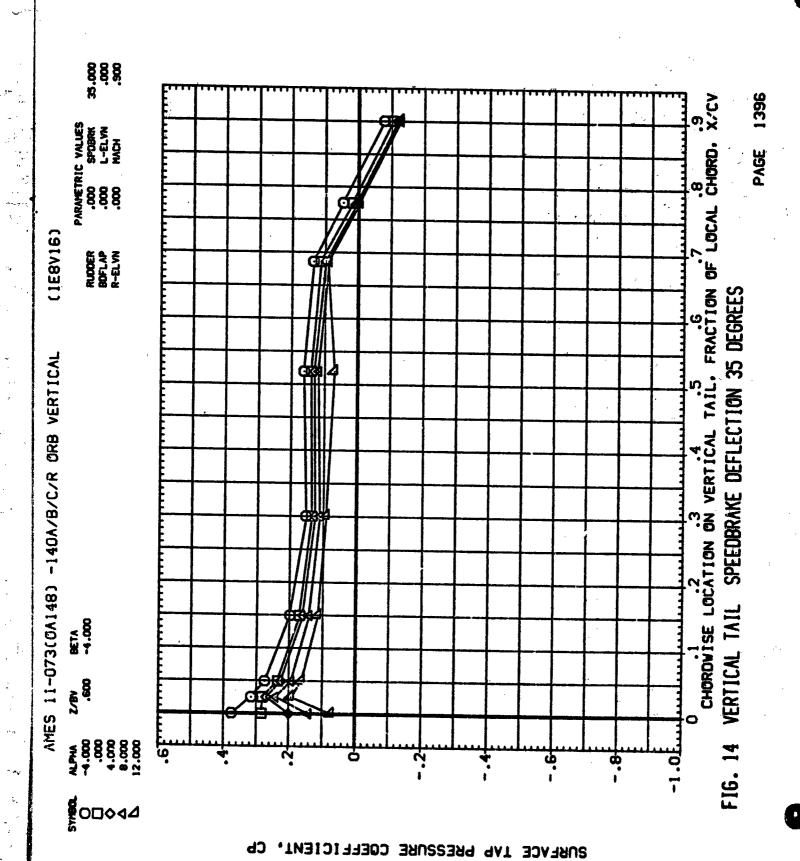
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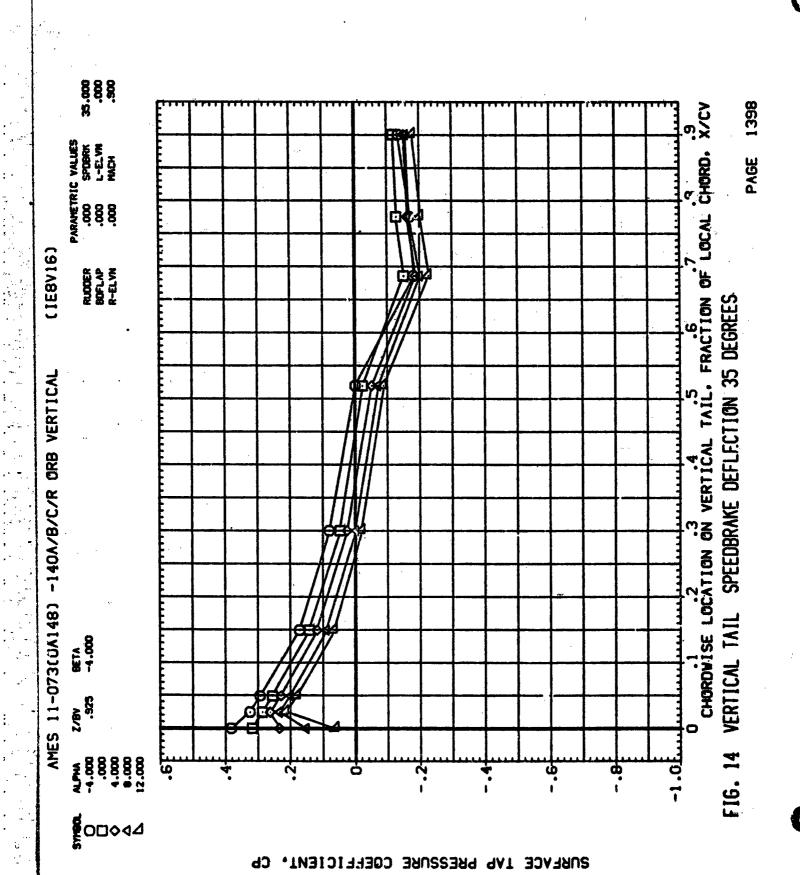
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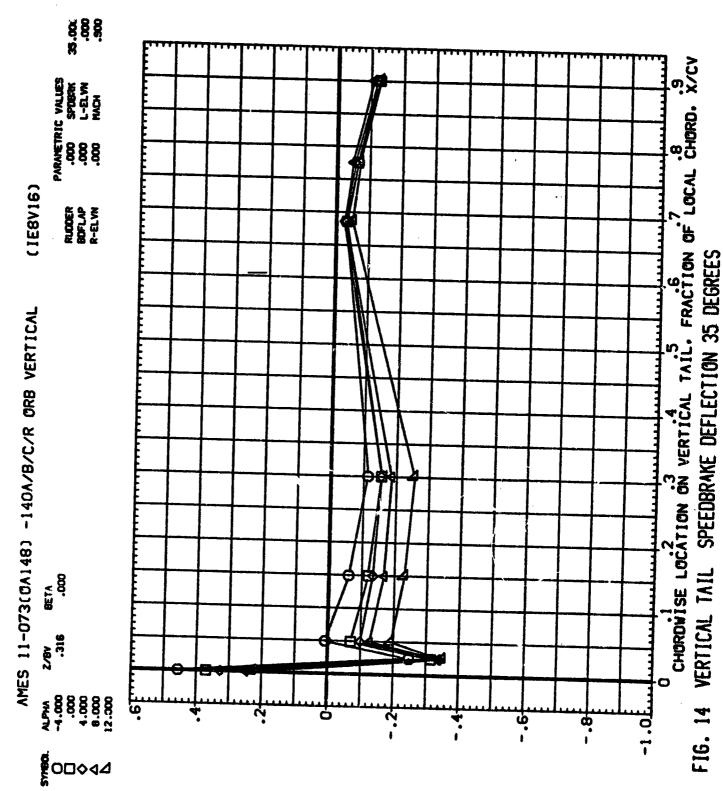
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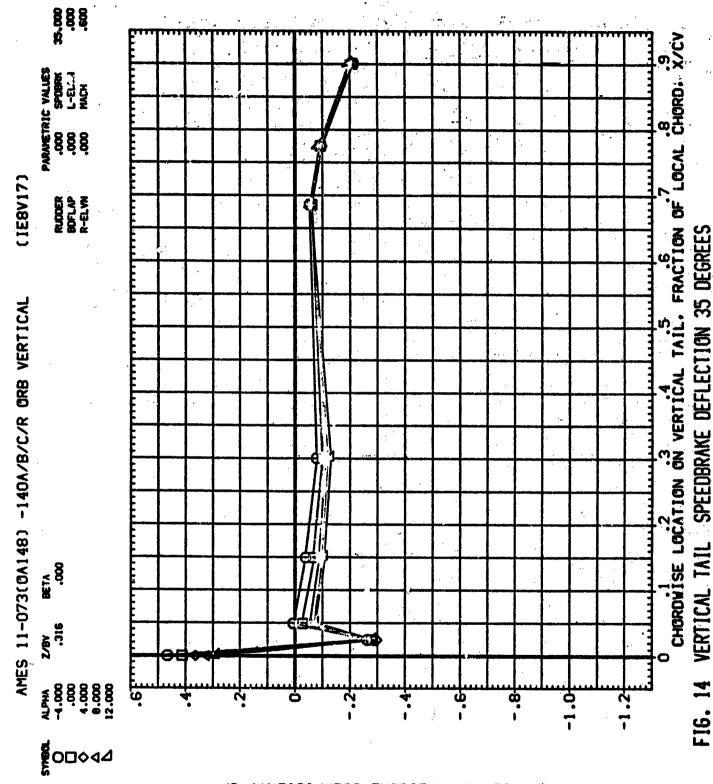
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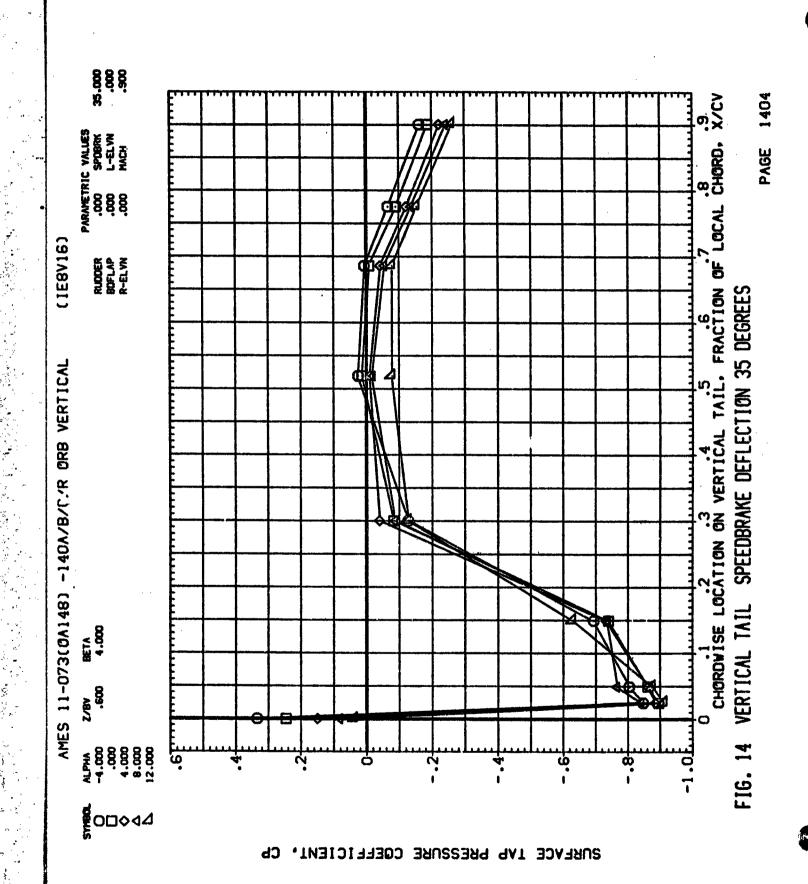
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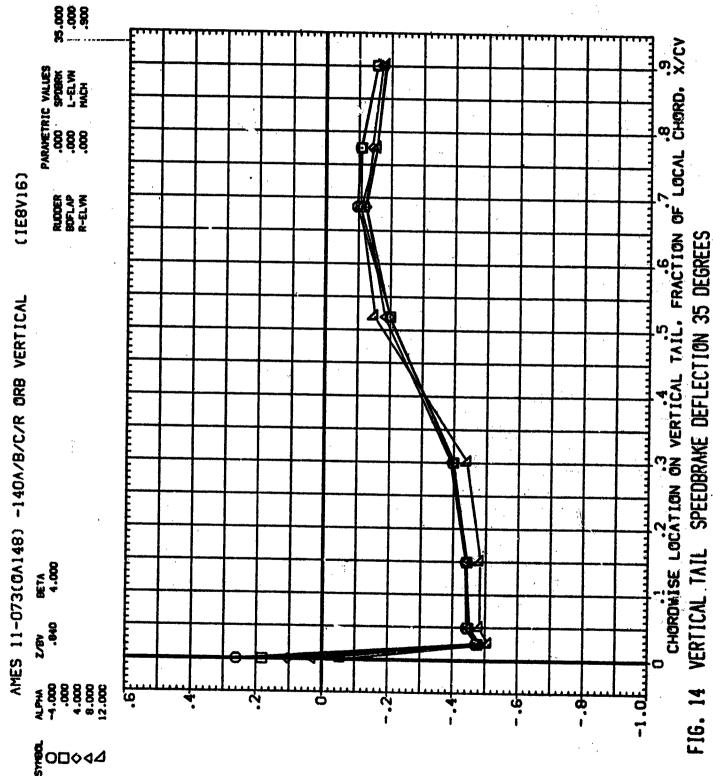
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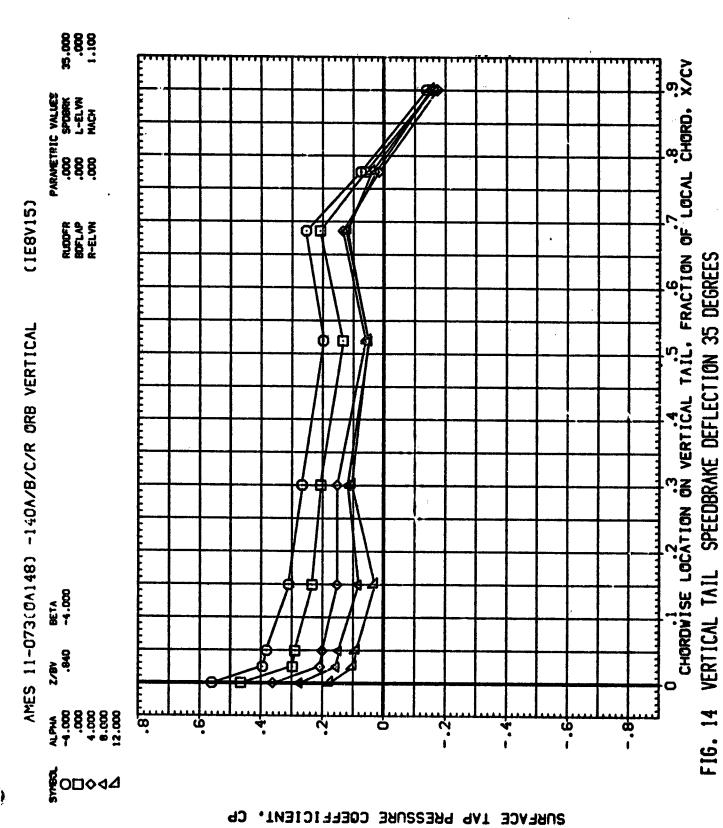
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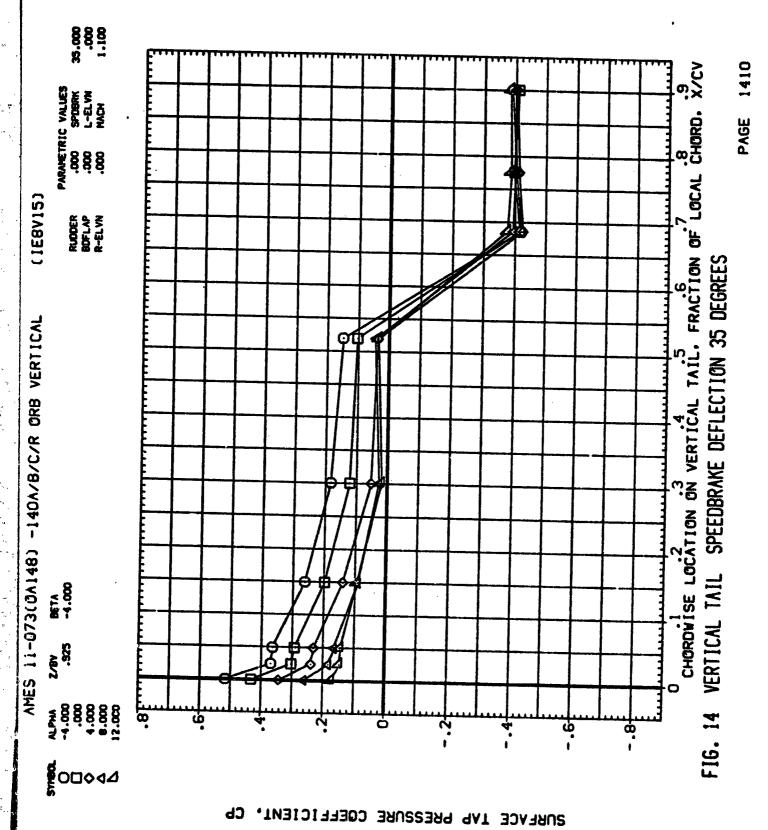


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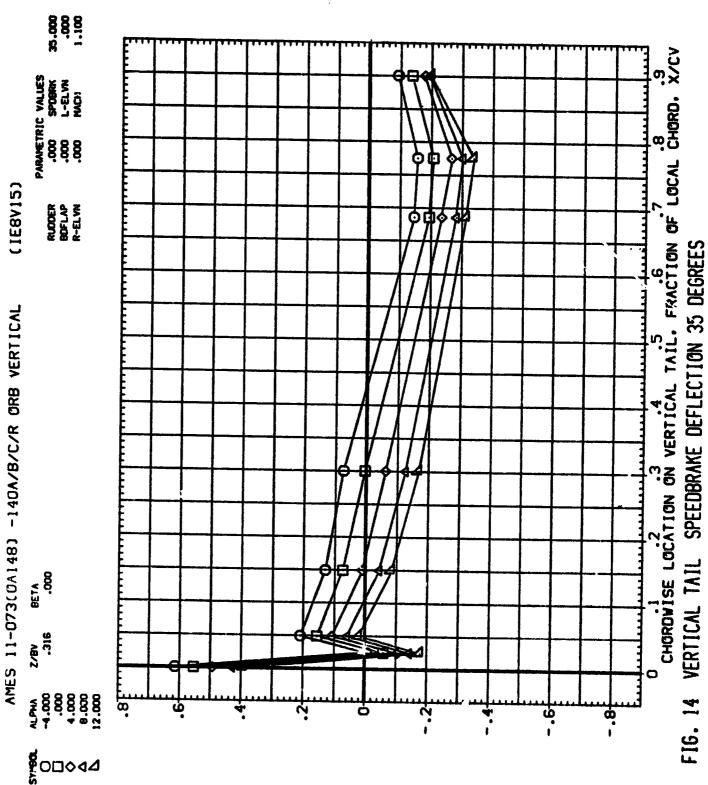


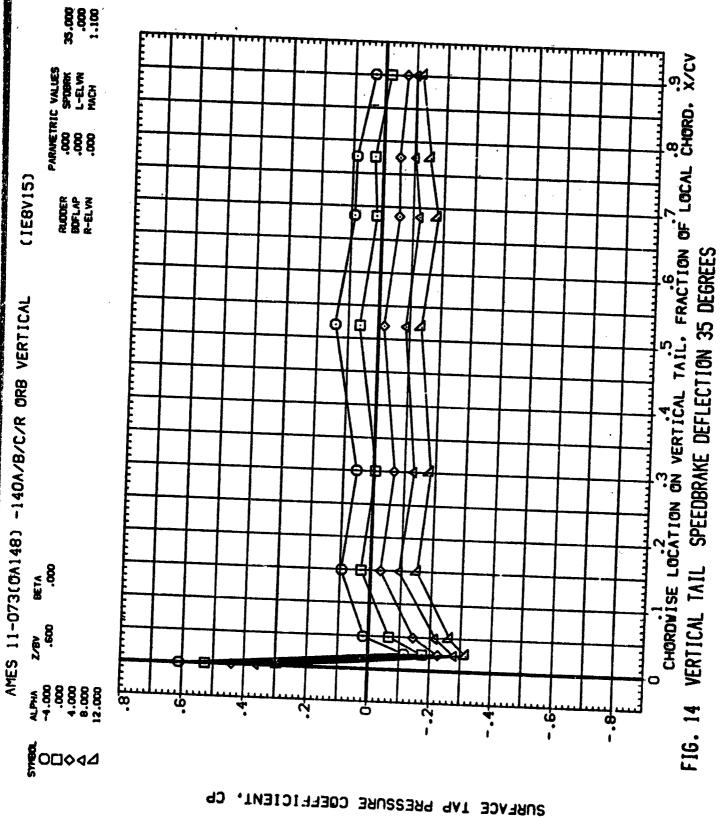
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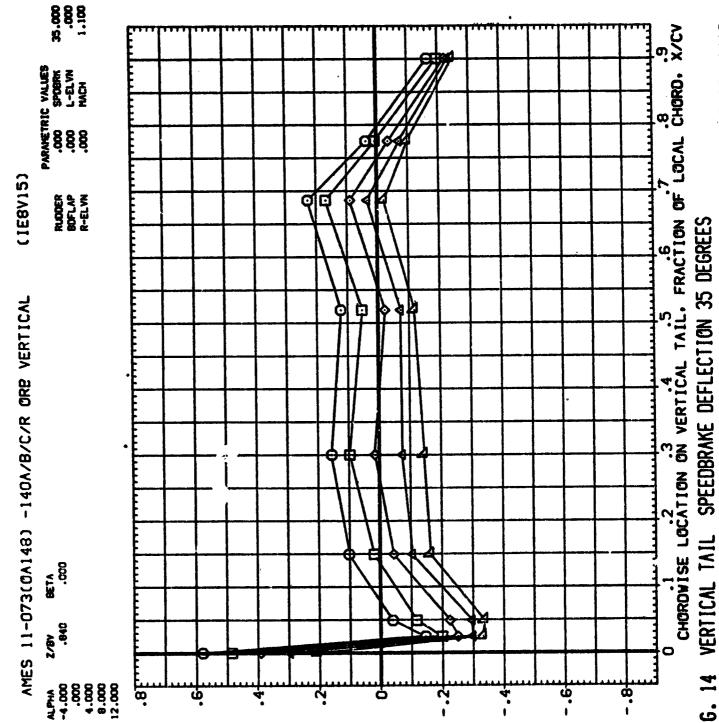


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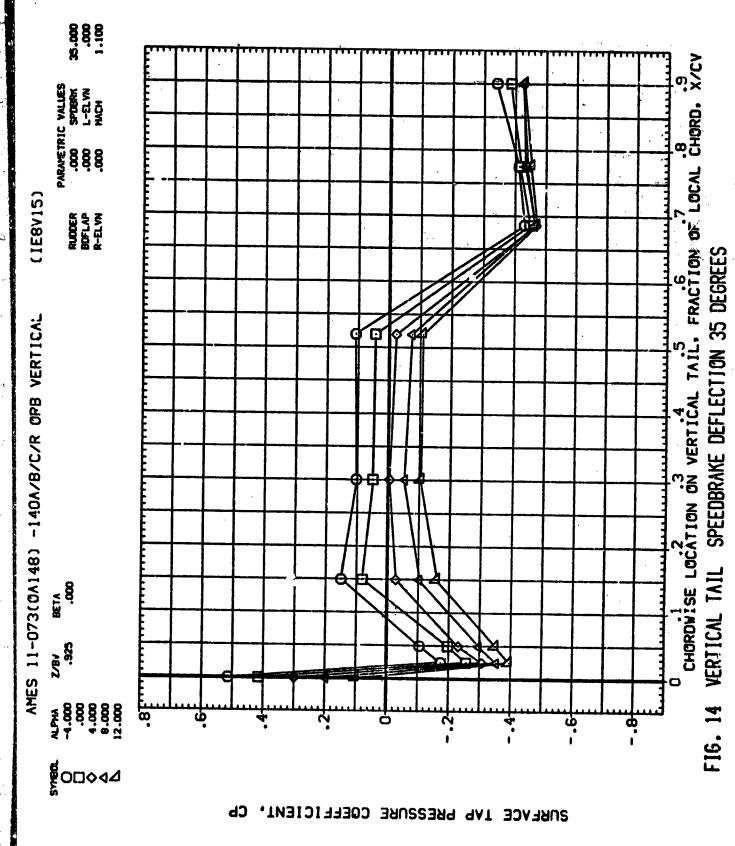


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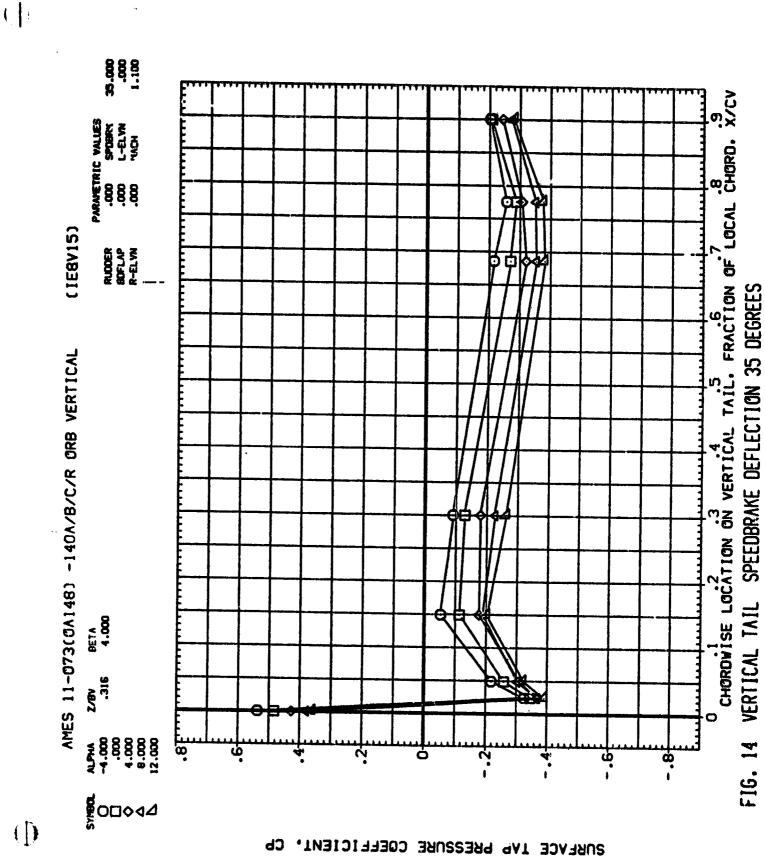


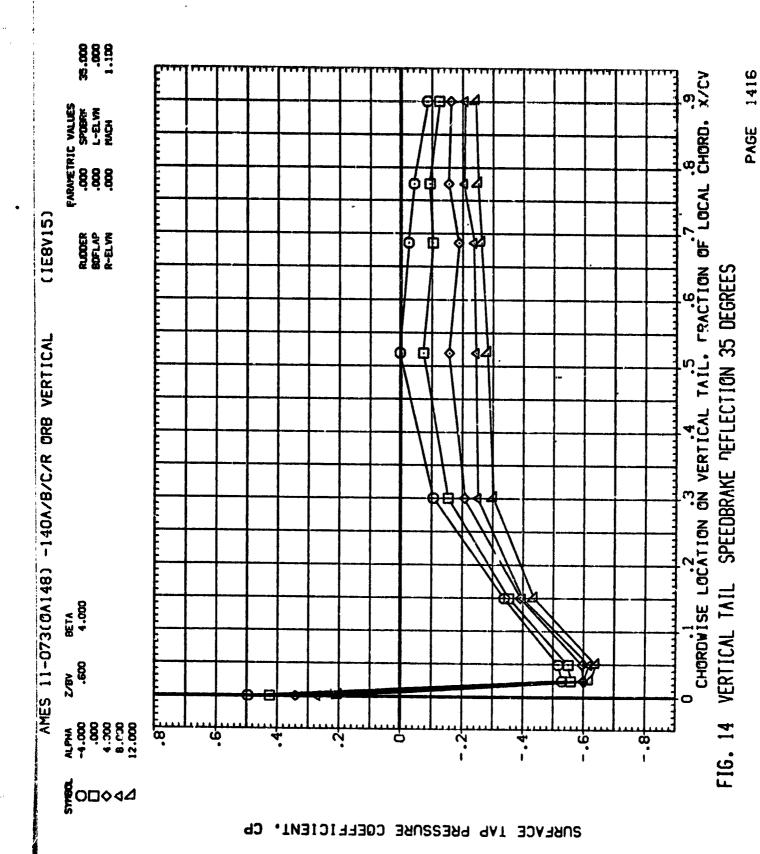
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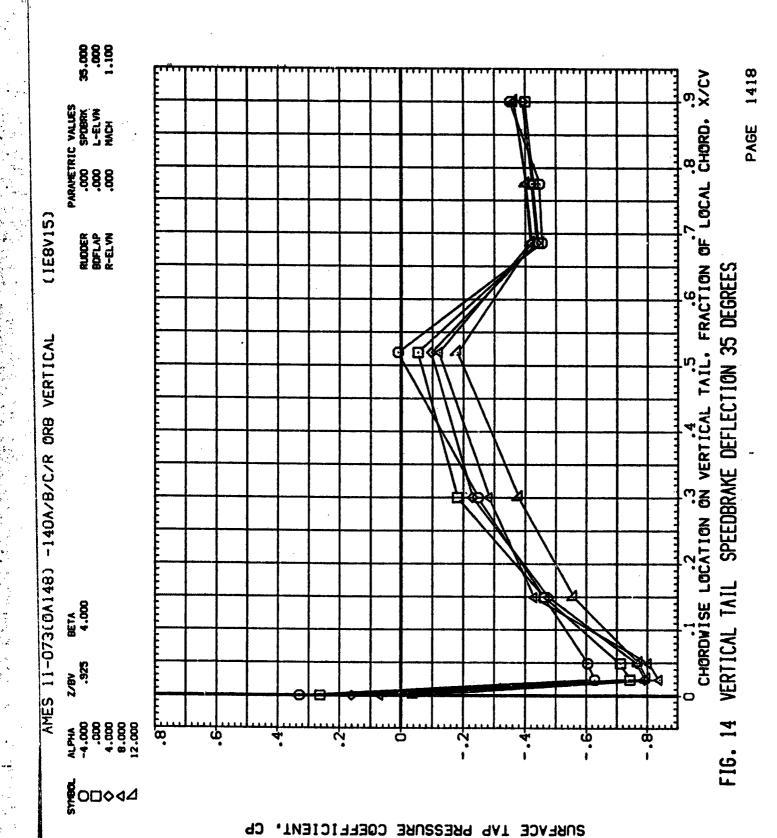
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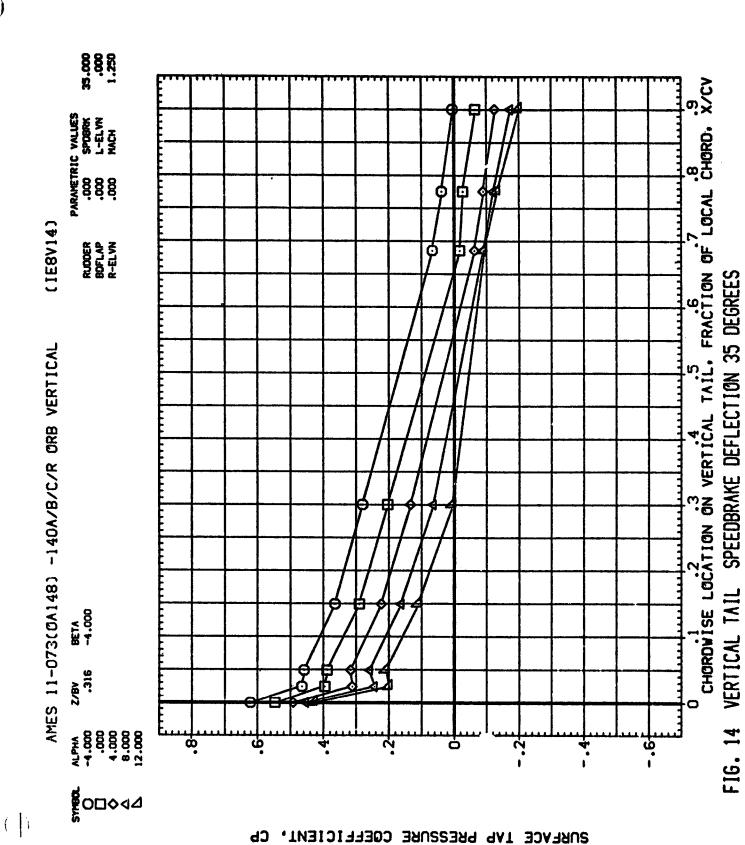


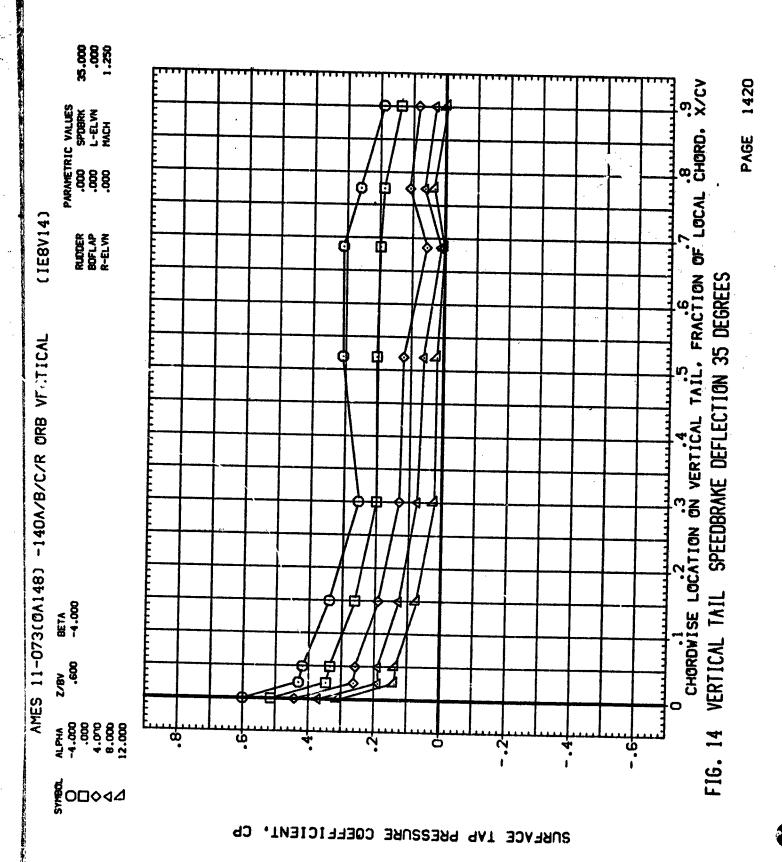


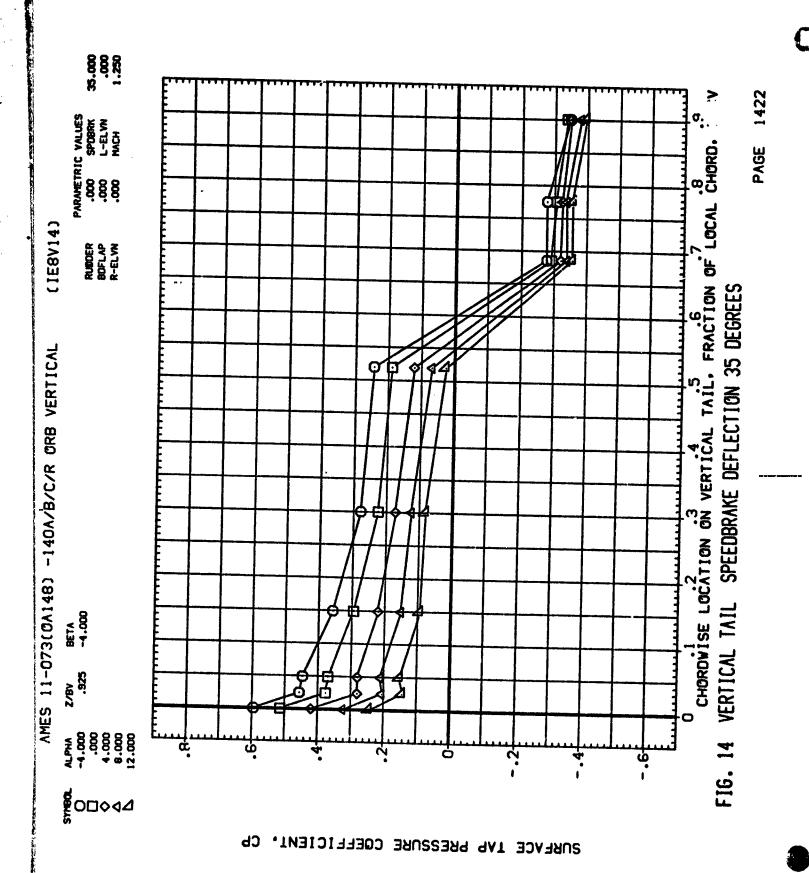
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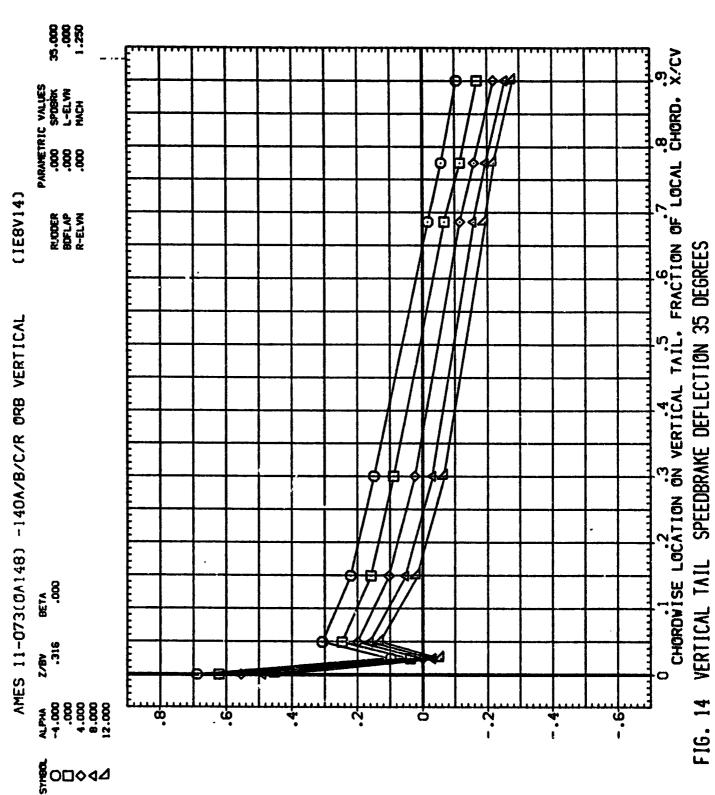
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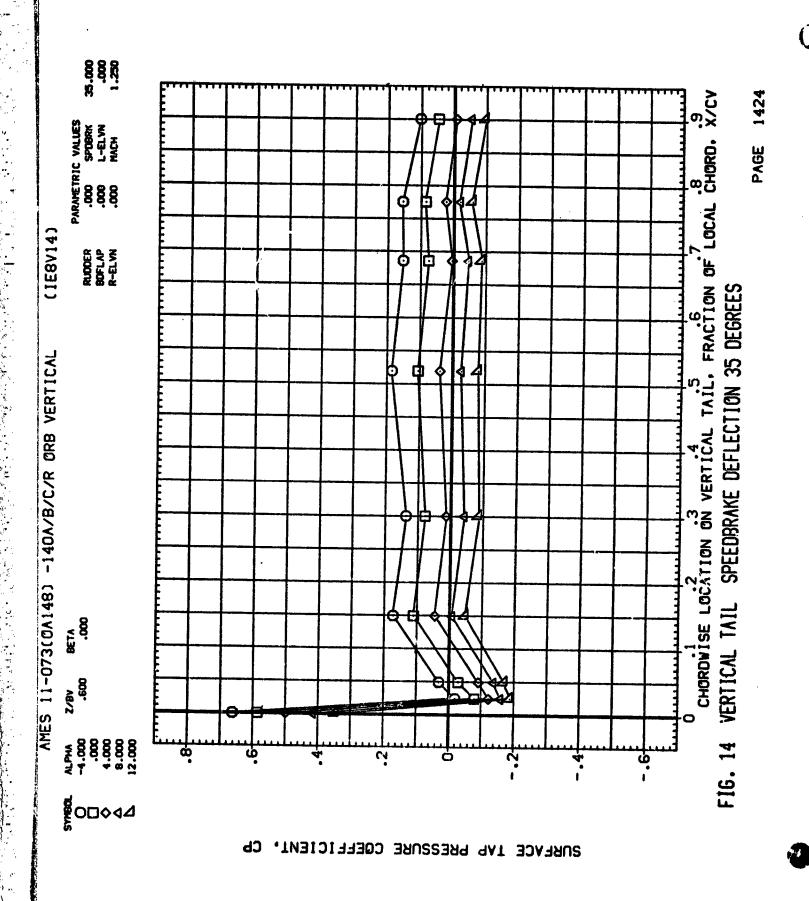


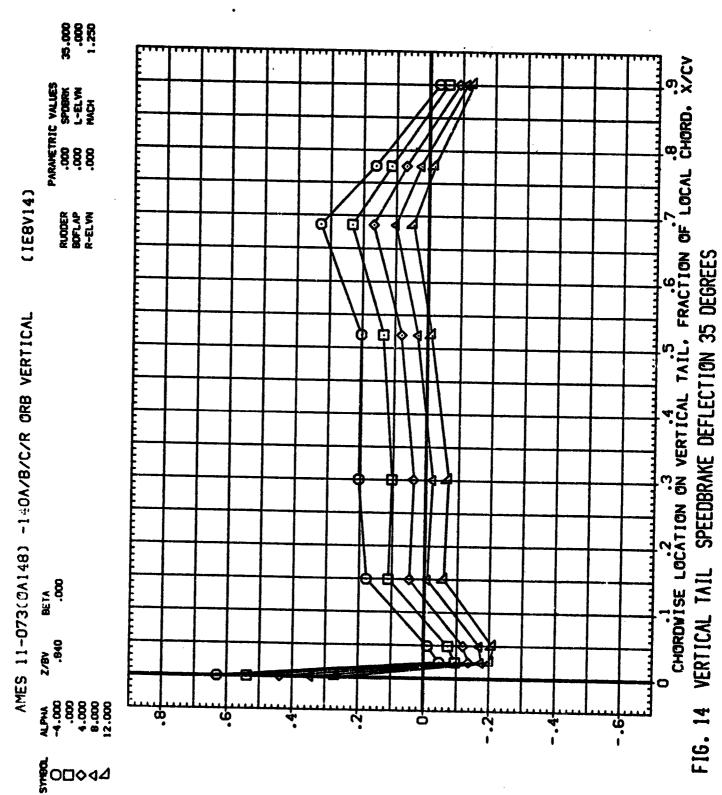




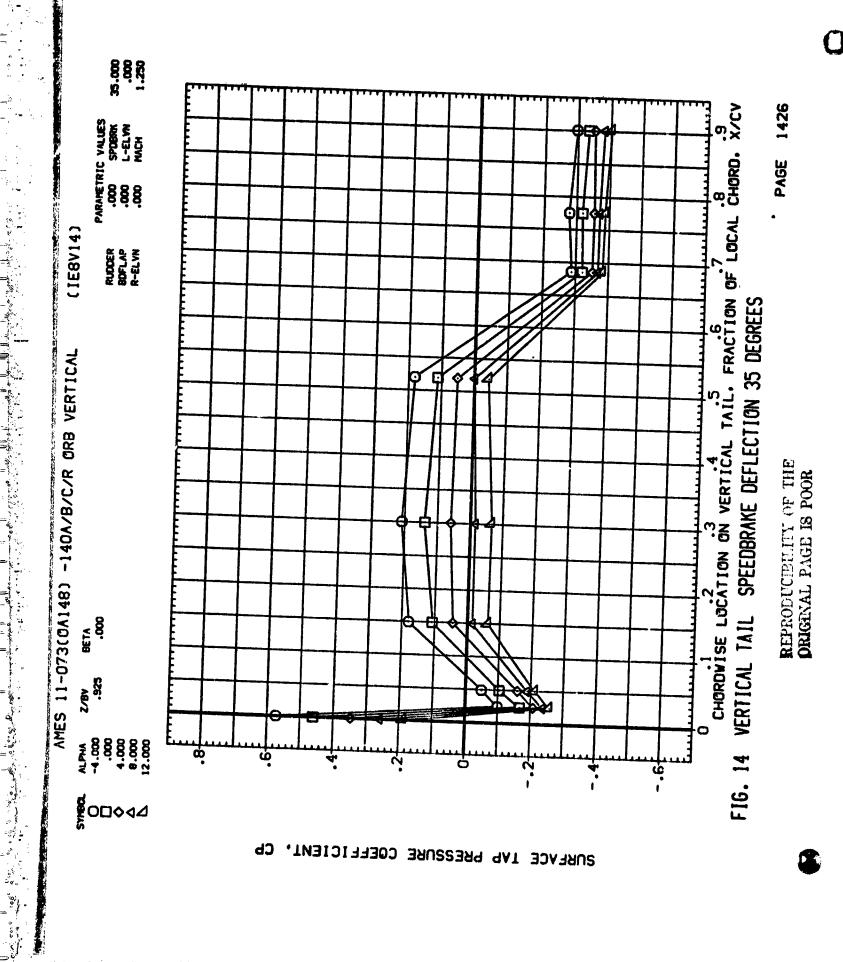


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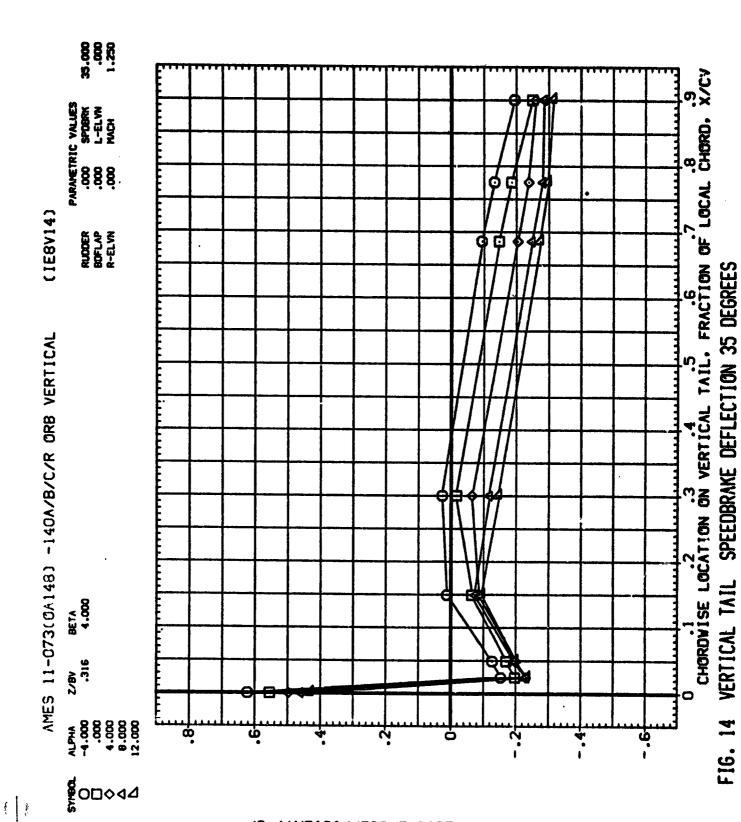




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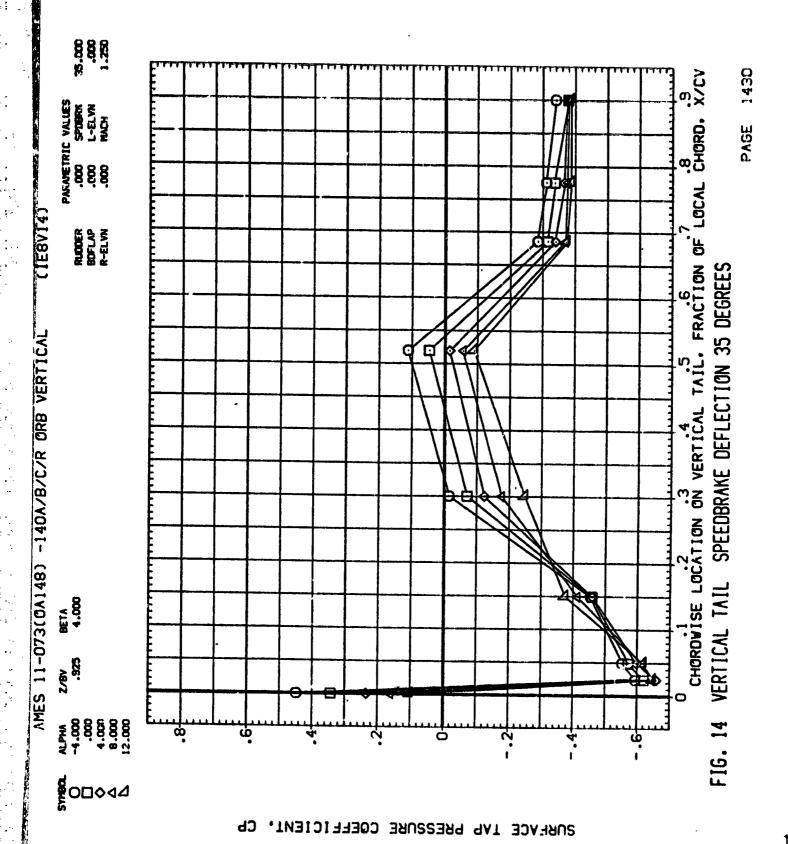


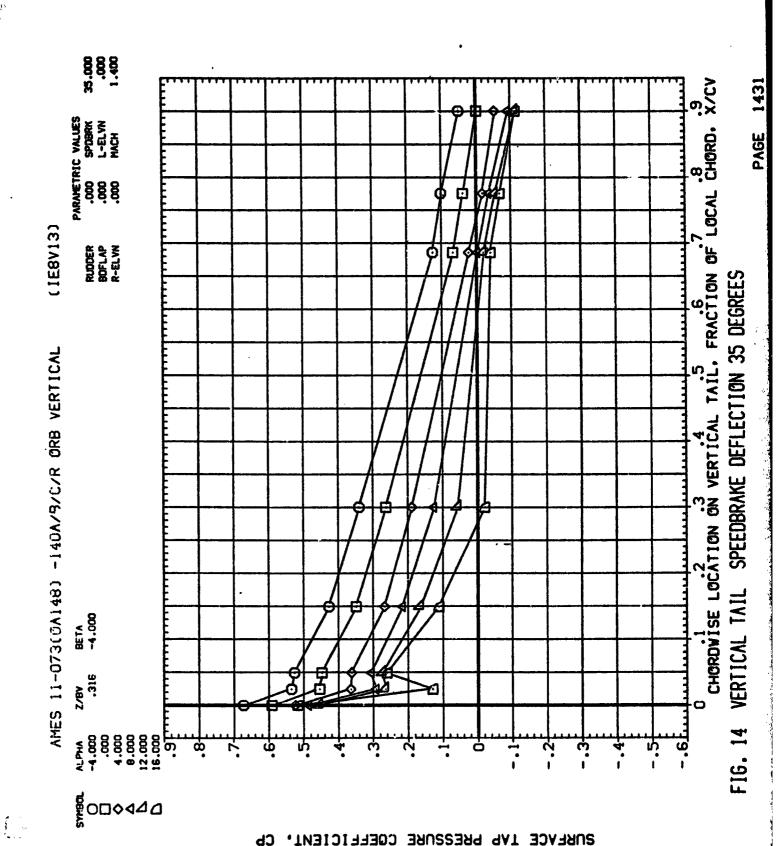
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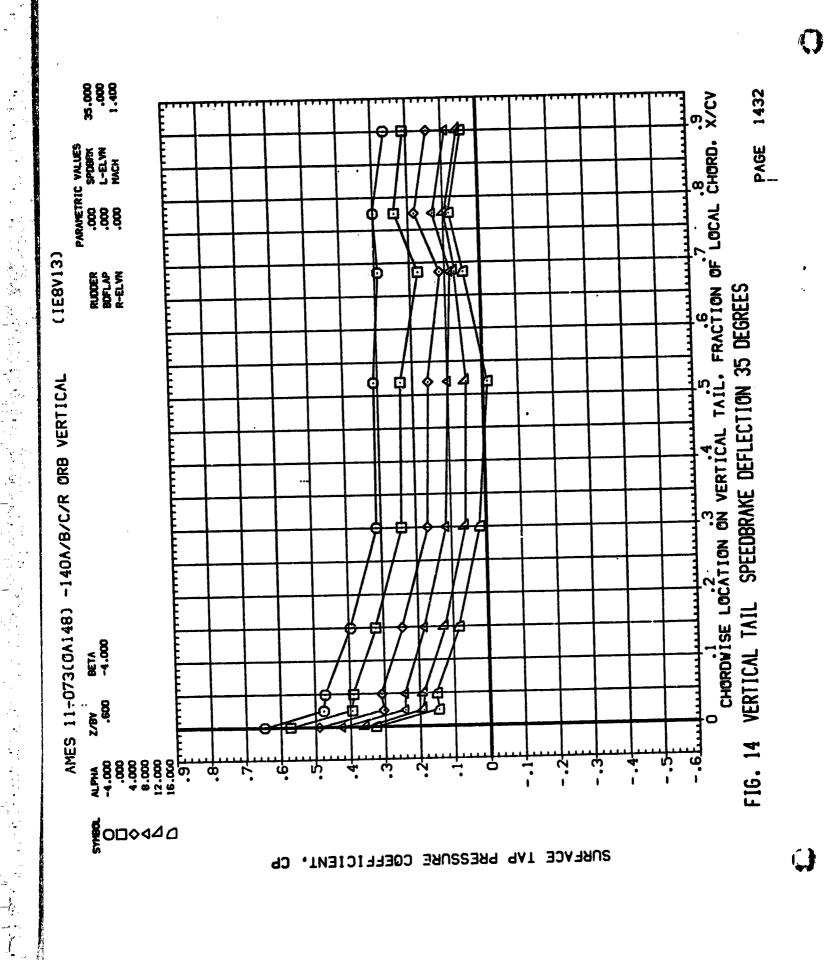
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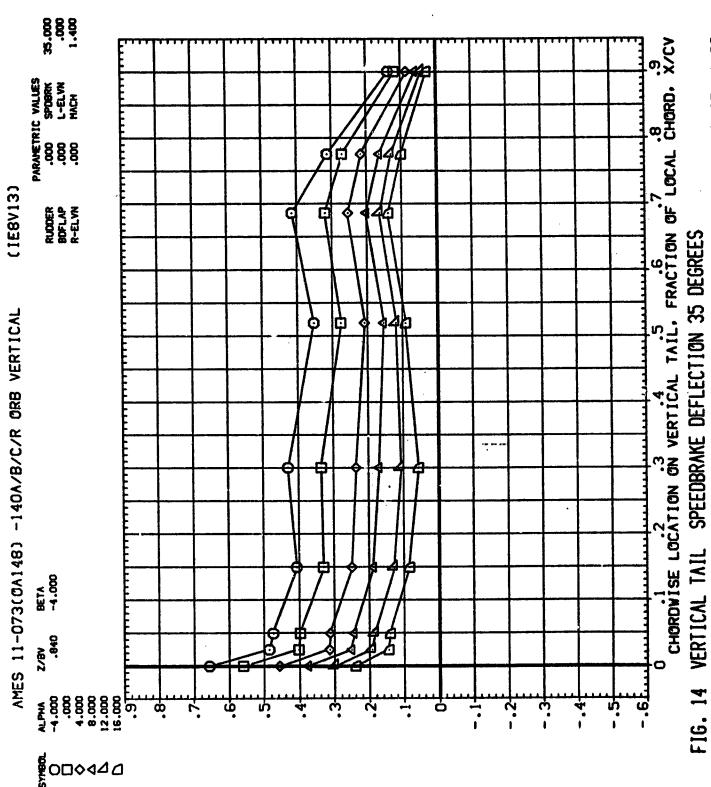
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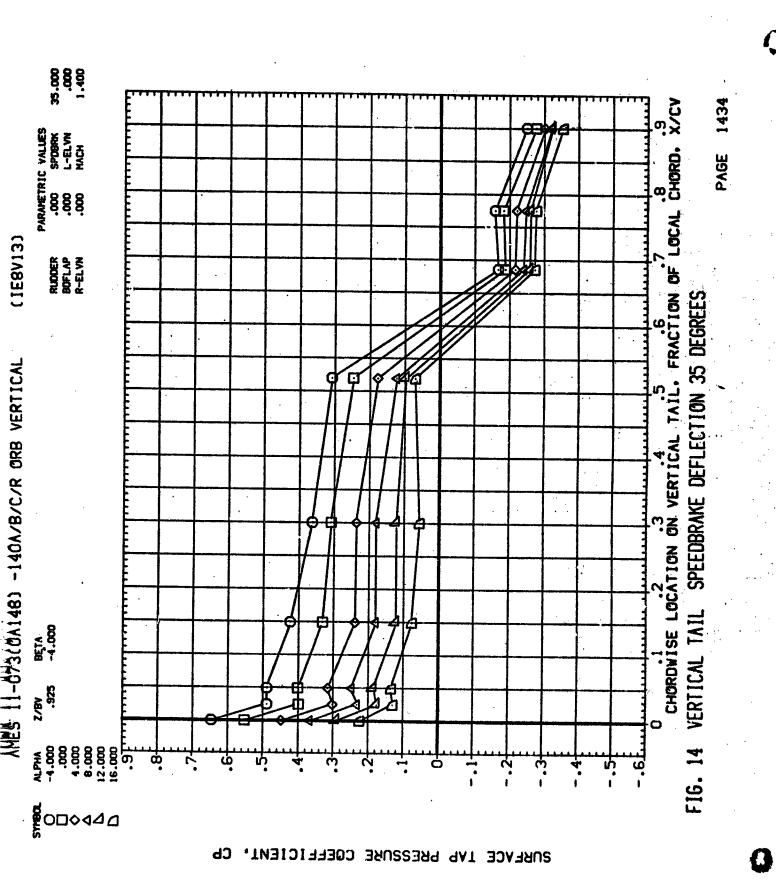
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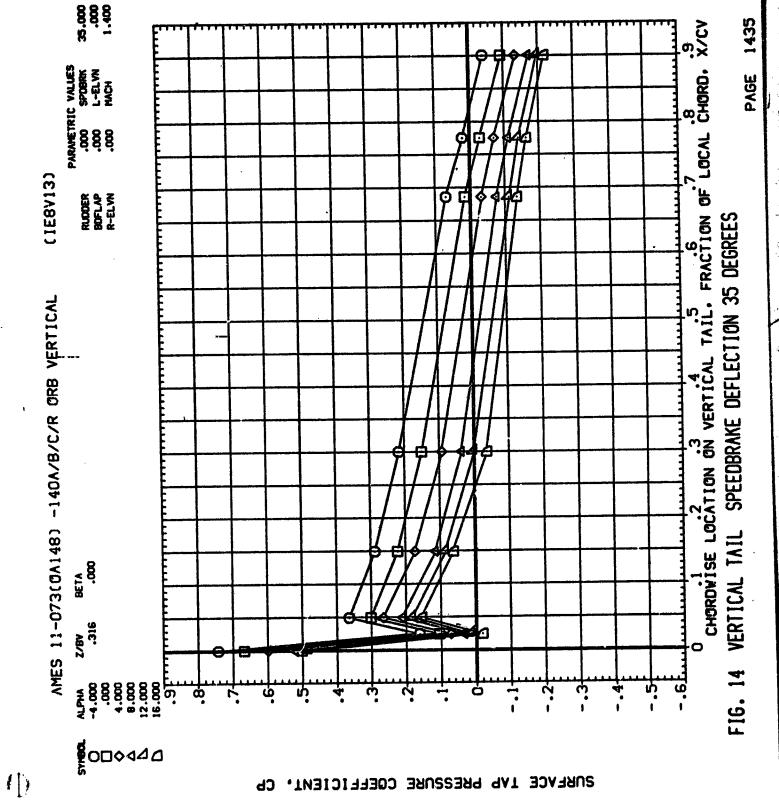




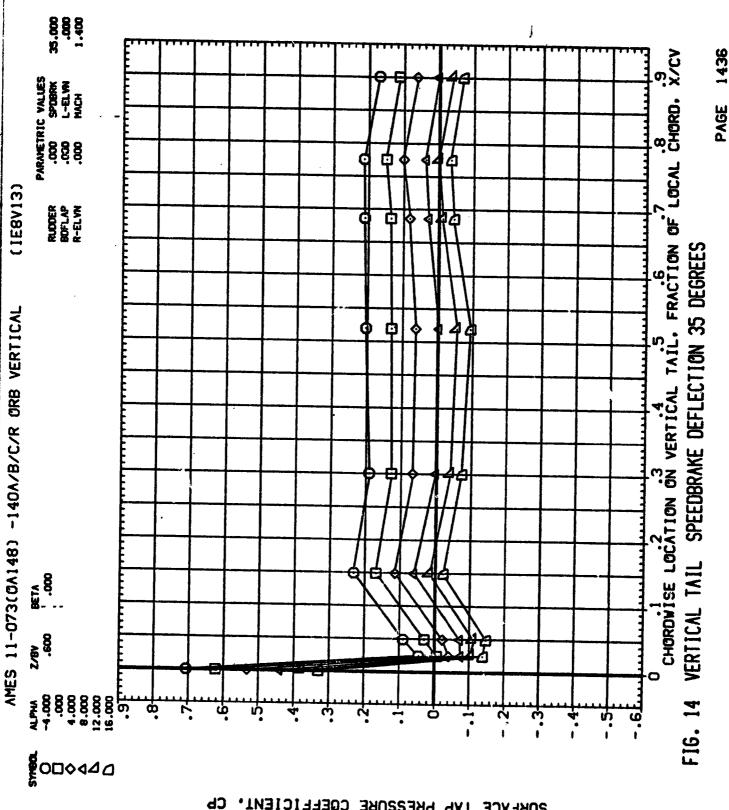
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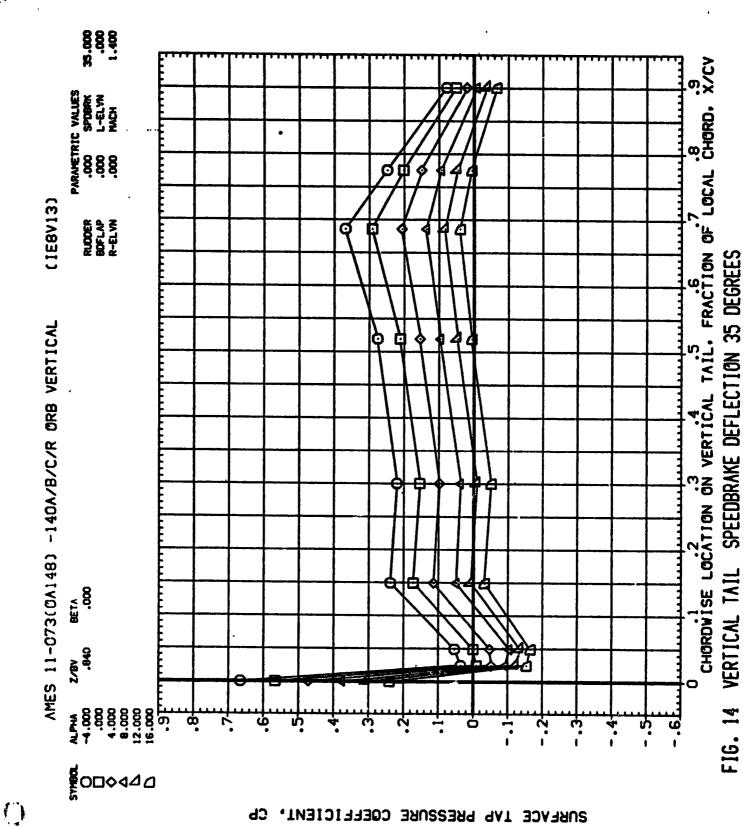


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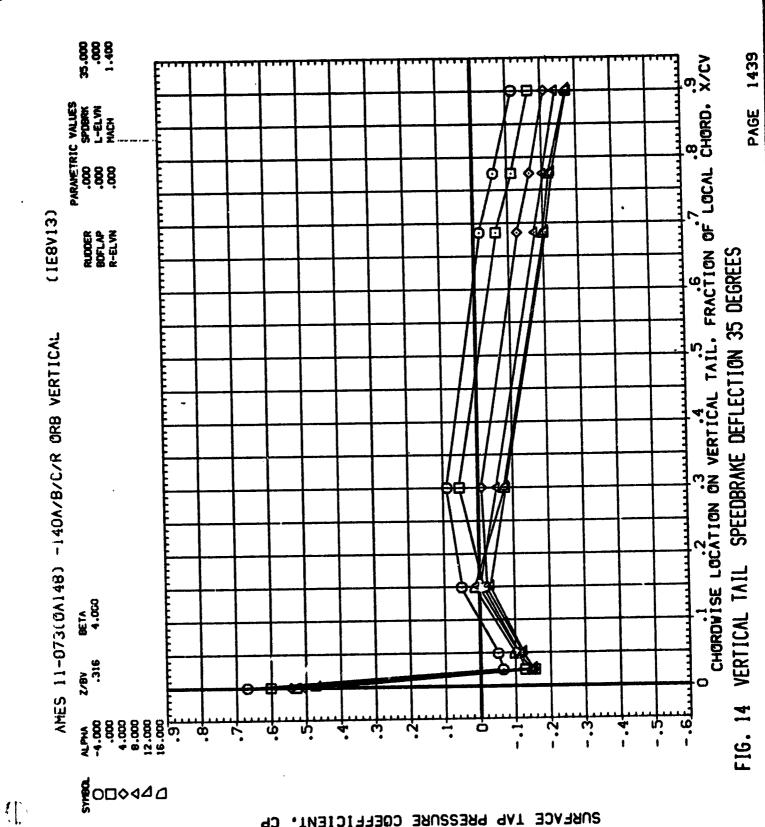


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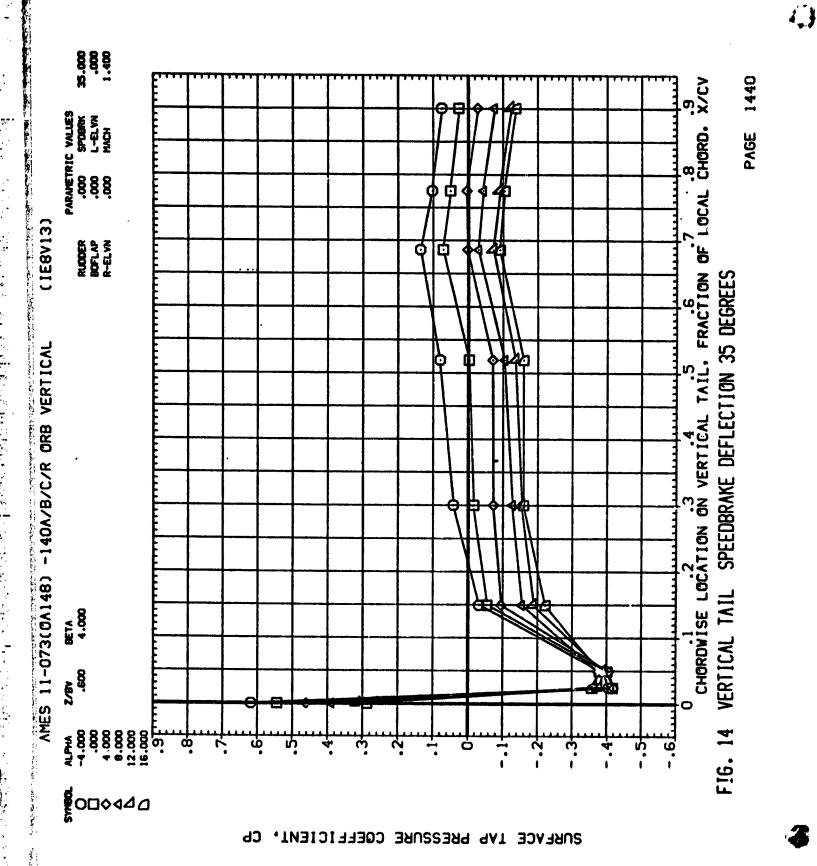
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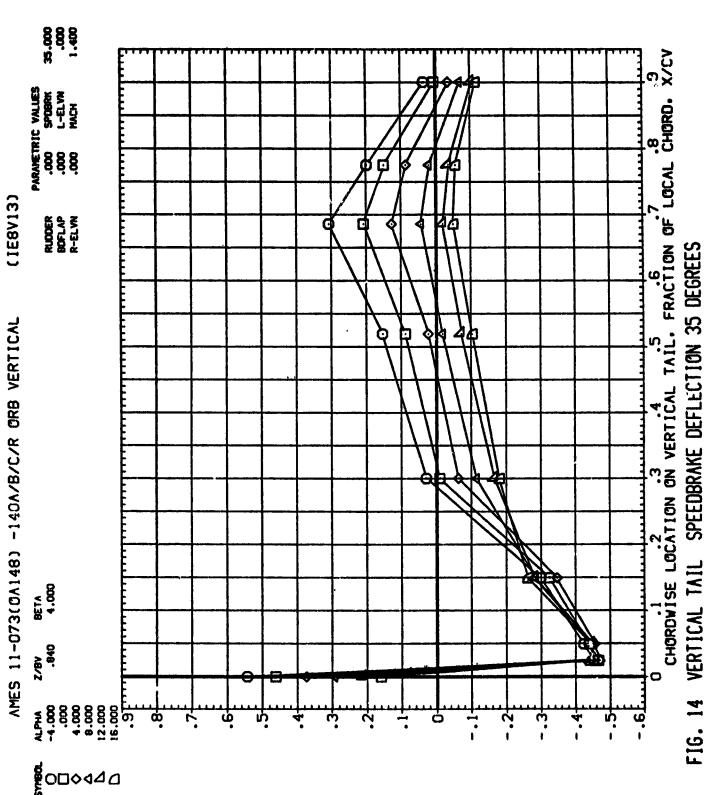


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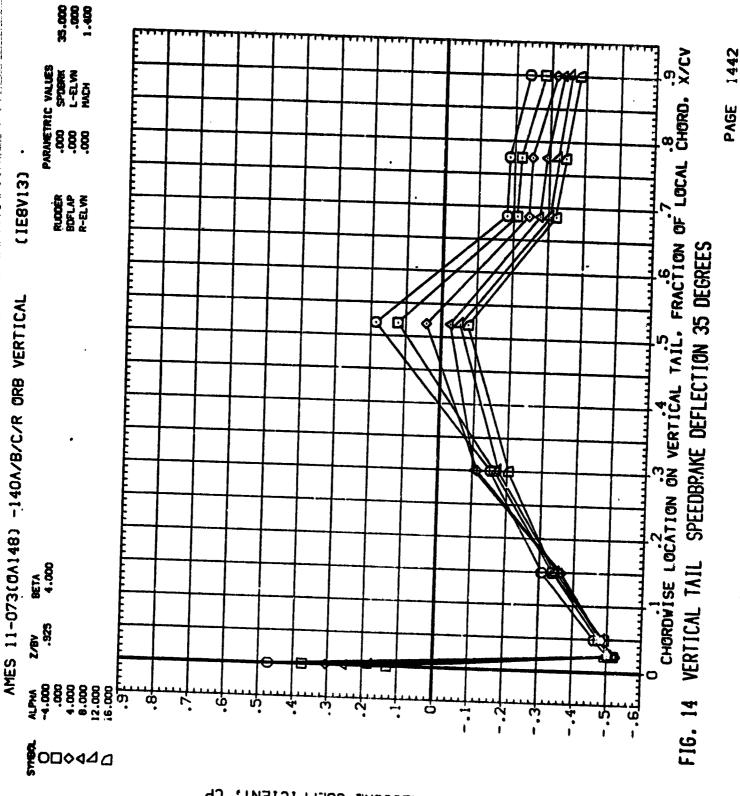


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